

# Lanes, Volumes, Timings

## 4: Norwood Avenue & EB 80 Off-Ramp/EB 80 On-Ramp

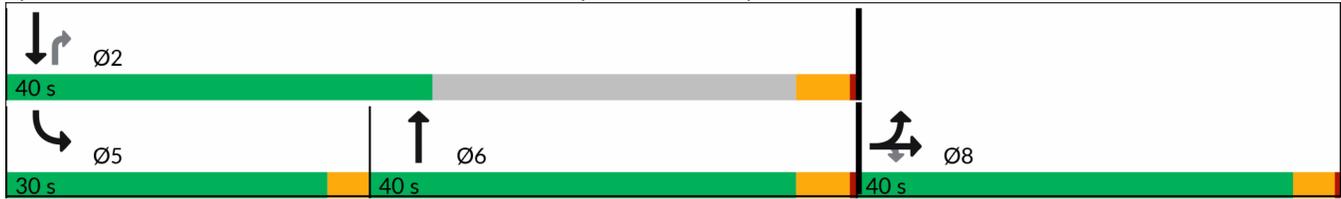
12/20/2024

Intersection Capacity Utilization 61.7%

ICU Level of Service B

Analysis Period (min) 15

Splits and Phases: 4: Norwood Avenue & EB 80 Off-Ramp/EB 80 On-Ramp



Queues

4: Norwood Avenue & EB 80 Off-Ramp/EB 80 On-Ramp

12/20/2024



| Lane Group              | EBL  | EBT  | EBR  | NBT  | NBR  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 238  | 240  | 369  | 670  | 246  | 264  | 534  |
| v/c Ratio               | 0.55 | 0.55 | 0.65 | 0.64 | 0.24 | 0.61 | 0.25 |
| Control Delay (s/veh)   | 28.3 | 28.3 | 15.8 | 24.7 | 1.7  | 31.3 | 7.0  |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 28.3 | 28.3 | 15.8 | 24.7 | 1.7  | 31.3 | 7.0  |
| Queue Length 50th (ft)  | 81   | 82   | 44   | 113  | 0    | 89   | 44   |
| Queue Length 95th (ft)  | 203  | 204  | 166  | 243  | 28   | 220  | 97   |
| Internal Link Dist (ft) |      | 679  |      | 657  |      |      | 446  |
| Turn Bay Length (ft)    |      |      | 50   |      | 220  | 180  |      |
| Base Capacity (vph)     | 1001 | 1007 | 1020 | 2082 | 1425 | 791  | 3256 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.24 | 0.24 | 0.36 | 0.32 | 0.17 | 0.33 | 0.16 |

Intersection Summary

HCM 6th Signalized Intersection Summary  
 4: Norwood Avenue & EB 80 Off-Ramp/EB 80 On-Ramp

12/20/2024

|   |  |  |  |  |  |  |  |  |  |  |  |  |
|---|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement  | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL  | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations   |  |  |  |   |   |   |  |  |  |  |  |  |
| Traffic Volume (veh/h)  | 466   | 12  | 369   | 0   | 0   | 0   | 0  | 670   | 246   | 264   | 534   | 0   |
| Future Volume (veh/h)   | 466   | 12  | 369   | 0   | 0   | 0   | 0  | 670   | 246   | 264   | 534   | 0   |
| Initial Q (Qb), veh   | 0   | 0   | 0   |   |   |   |  | 0   | 0   | 0   | 0   | 0   |
| Ped-Bike Adj(A_pbT)   | 1.00  |   | 1.00  |   |   |   |  | 1.00  | 1.00  | 1.00  |   | 1.00  |
| Parking Bus, Adj  | 1.00  | 1.00  | 1.00  |   |   |   |  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach   |   | No  |   |   |   |   |  | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln  | 1856  | 1856  | 1856  |   |   |   | 0  | 1870  | 1870  | 1885  | 1885  | 0   |
| Adj Flow Rate, veh/h  | 475   | 0   | 0   |   |   |   | 0  | 670   | 0   | 264   | 534   | 0   |
| Peak Hour Factor  | 1.00  | 1.00  | 1.00  |   |   |   | 1.00   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %  | 3   | 3   | 3   |   |   |   | 0  | 2   | 2   | 1   | 1   | 0   |
| Cap, veh/h  | 765   | 0   |   |   |   |   | 0  | 1064  |   | 342   | 2054  | 0   |
| Arrive On Green   | 0.22  | 0.00  | 0.00  |   |   |   | 0.00   | 0.30  | 0.00  | 0.19  | 0.57  | 0.00  |
| Sat Flow, veh/h   | 3534  | 0   | 1572  |   |   |   | 0  | 3647  | 1585  | 1795  | 3676  | 0   |
| Grp Volume(v), veh/h  | 475   | 0   | 0   |   |   |   | 0  | 670   | 0   | 264   | 534   | 0   |
| Grp Sat Flow(s),veh/h/ln  | 1767  | 0   | 1572  |   |   |   | 0  | 1777  | 1585  | 1795  | 1791  | 0   |
| Q Serve(g_s), s   | 5.1   | 0.0   | 0.0   |   |   |   | 0.0  | 6.8   | 0.0   | 5.8   | 3.1   | 0.0   |
| Cycle Q Clear(g_c), s   | 5.1   | 0.0   | 0.0   |   |   |   | 0.0  | 6.8   | 0.0   | 5.8   | 3.1   | 0.0   |
| Prop In Lane  | 1.00  |   | 1.00  |   |   |   | 0.00   |   | 1.00  | 1.00  |   | 0.00  |
| Lane Grp Cap(c), veh/h  | 765   | 0   |   |   |   |   | 0  | 1064  |   | 342   | 2054  | 0   |
| V/C Ratio(X)  | 0.62  | 0.00  |   |   |   |   | 0.00   | 0.63  |   | 0.77  | 0.26  | 0.00  |
| Avail Cap(c_a), veh/h   | 3039  | 0   |   |   |   |   | 0  | 2987  |   | 1136  | 3011  | 0   |
| HCM Platoon Ratio   | 1.00  | 1.00  | 1.00  |   |   |   | 1.00   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)  | 1.00  | 0.00  | 0.00  |   |   |   | 0.00   | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  |
| Uniform Delay (d), s/veh  | 14.9  | 0.0   | 0.0   |   |   |   | 0.0  | 12.7  | 0.0   | 16.1  | 4.5   | 0.0   |
| Incr Delay (d2), s/veh  | 0.3   | 0.0   | 0.0   |   |   |   | 0.0  | 0.5   | 0.0   | 2.8   | 0.0   | 0.0   |
| Initial Q Delay(d3), s/veh  | 0.0   | 0.0   | 0.0   |   |   |   | 0.0  | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln  | 1.7   | 0.0   | 0.0   |   |   |   | 0.0  | 2.1   | 0.0   | 2.3   | 0.7   | 0.0   |
| Unsig. Movement Delay, s/veh  |   |   |   |   |   |   |  |   |   |   |   |   |
| LnGrp Delay(d), s/veh   | 15.2  | 0.0   | 0.0   |   |   |   | 0.0  | 13.1  | 0.0   | 18.9  | 4.5   | 0.0   |
| LnGrp LOS   | B   |   |   |   |   |   |  | B   |   | B   | A   |   |
| Approach Vol, veh/h   |   | 475   |   |   |   |   |  | 670   |   |   | 798   |   |
| Approach Delay, s/veh   |   | 15.2  |   |   |   |   |  | 13.1  |   |   | 9.3   |   |
| Approach LOS  |   | B   |   |   |   |   |  | B   |   |   | A   |   |
| Timer - Assigned Phs  |   | 2   |   |   | 5   | 6   |  | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s  |   | 28.8  |   |   | 11.5  | 17.3  |  | 13.1  |   |   |   |   |
| Change Period (Y+Rc), s   |   | 4.8   |   |   | 3.5   | 4.8   |  | 4.0   |   |   |   |   |
| Max Green Setting (Gmax), s   |   | 35.2  |   |   | 26.5  | 35.2  |  | 36.0  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s  |   | 5.1   |   |   | 7.8   | 8.8   |  | 7.1   |   |   |   |   |
| Green Ext Time (p_c), s   |   | 3.2   |   |   | 0.5   | 3.7   |  | 0.9   |   |   |   |   |
| <b>Intersection Summary</b>   |   |   |   |   |   |   |  |   |   |   |   |   |
| HCM 6th Ctrl Delay, s/veh   |   |   | 12.0  |   |   |   |  |   |   |   |   |   |
| HCM 6th LOS   |   |   | B   |   |   |   |  |   |   |   |   |   |
| <b>Notes</b>  |   |   |   |   |   |   |  |   |   |   |   |   |
| User approved volume balancing among the lanes for turning movement.  |   |   |   |   |   |   |  |   |   |   |   |   |
| Unsignalized Delay for [NBR, EBR] is excluded from calculations of the approach delay and intersection delay. |   |   |   |   |   |   |  |   |   |   |   |   |

# HCM 7th Signalized Intersection Summary

## 4: Norwood Avenue & EB 80 Off-Ramp/EB 80 On-Ramp

12/20/2024



| Movement                     | EBL  | EBT  | EBR  | WBL | WBT  | WBR  | NBL  | NBT  | NBR  | SBL  | SBT  | SBR  |
|------------------------------|------|------|------|-----|------|------|------|------|------|------|------|------|
| Lane Configurations          | ↖    | ↗    | ↘    |     |      |      |      | ↑↑   | ↗    | ↘    | ↑↑   |      |
| Traffic Volume (veh/h)       | 466  | 12   | 369  | 0   | 0    | 0    | 0    | 670  | 246  | 264  | 534  | 0    |
| Future Volume (veh/h)        | 466  | 12   | 369  | 0   | 0    | 0    | 0    | 670  | 246  | 264  | 534  | 0    |
| Initial Q (Qb), veh          | 0    | 0    | 0    |     |      |      | 0    | 0    | 0    | 0    | 0    | 0    |
| Lane Width Adj.              | 1.00 | 1.00 | 1.00 |     |      |      | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped-Bike Adj(A_pbT)          | 1.00 |      | 1.00 |     |      |      | 1.00 |      | 1.00 | 1.00 |      | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00 | 1.00 |     |      |      | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach        |      | No   |      |     |      |      |      | No   |      |      | No   |      |
| Adj Sat Flow, veh/h/ln       | 1856 | 1856 | 1856 |     |      |      | 0    | 1870 | 1870 | 1885 | 1885 | 0    |
| Adj Flow Rate, veh/h         | 475  | 0    | 0    |     |      |      | 0    | 670  | 0    | 264  | 534  | 0    |
| Peak Hour Factor             | 1.00 | 1.00 | 1.00 |     |      |      | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, %         | 3    | 3    | 3    |     |      |      | 0    | 2    | 2    | 1    | 1    | 0    |
| Cap, veh/h                   | 765  | 0    |      |     |      |      | 0    | 1064 |      | 342  | 2054 | 0    |
| Arrive On Green              | 0.22 | 0.00 | 0.00 |     |      |      | 0.00 | 0.30 | 0.00 | 0.19 | 0.57 | 0.00 |
| Sat Flow, veh/h              | 3534 | 0    | 1572 |     |      |      | 0    | 3647 | 1585 | 1795 | 3676 | 0    |
| Grp Volume(v), veh/h         | 475  | 0    | 0    |     |      |      | 0    | 670  | 0    | 264  | 534  | 0    |
| Grp Sat Flow(s),veh/h/ln     | 1767 | 0    | 1572 |     |      |      | 0    | 1777 | 1585 | 1795 | 1791 | 0    |
| Q Serve(g_s), s              | 5.1  | 0.0  | 0.0  |     |      |      | 0.0  | 6.8  | 0.0  | 5.8  | 3.1  | 0.0  |
| Cycle Q Clear(g_c), s        | 5.1  | 0.0  | 0.0  |     |      |      | 0.0  | 6.8  | 0.0  | 5.8  | 3.1  | 0.0  |
| Prop In Lane                 | 1.00 |      | 1.00 |     |      |      | 0.00 |      | 1.00 | 1.00 |      | 0.00 |
| Lane Grp Cap(c), veh/h       | 765  | 0    |      |     |      |      | 0    | 1064 |      | 342  | 2054 | 0    |
| V/C Ratio(X)                 | 0.62 | 0.00 |      |     |      |      | 0.00 | 0.63 |      | 0.77 | 0.26 | 0.00 |
| Avail Cap(c_a), veh/h        | 3039 | 0    |      |     |      |      | 0    | 2987 |      | 1136 | 3011 | 0    |
| HCM Platoon Ratio            | 1.00 | 1.00 | 1.00 |     |      |      | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00 | 0.00 |     |      |      | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh     | 14.9 | 0.0  | 0.0  |     |      |      | 0.0  | 12.7 | 0.0  | 16.1 | 4.5  | 0.0  |
| Incr Delay (d2), s/veh       | 0.3  | 0.0  | 0.0  |     |      |      | 0.0  | 0.5  | 0.0  | 2.8  | 0.0  | 0.0  |
| Initial Q Delay(d3), s/veh   | 0.0  | 0.0  | 0.0  |     |      |      | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 1.7  | 0.0  | 0.0  |     |      |      | 0.0  | 2.1  | 0.0  | 2.3  | 0.7  | 0.0  |
| Unsig. Movement Delay, s/veh |      |      |      |     |      |      |      |      |      |      |      |      |
| LnGrp Delay(d), s/veh        | 15.2 | 0.0  | 0.0  |     |      |      | 0.0  | 13.1 | 0.0  | 18.9 | 4.5  | 0.0  |
| LnGrp LOS                    | B    |      |      |     |      |      |      | B    |      | B    | A    |      |
| Approach Vol, veh/h          |      | 475  |      |     |      |      |      | 670  |      |      | 798  |      |
| Approach Delay, s/veh        |      | 15.2 |      |     |      |      |      | 13.1 |      |      | 9.3  |      |
| Approach LOS                 |      | B    |      |     |      |      |      | B    |      |      | A    |      |
| Timer - Assigned Phs         |      | 2    |      |     | 5    | 6    |      | 8    |      |      |      |      |
| Phs Duration (G+Y+Rc), s     |      | 28.8 |      |     | 11.5 | 17.3 |      | 13.1 |      |      |      |      |
| Change Period (Y+Rc), s      |      | 4.8  |      |     | 3.5  | 4.8  |      | 4.0  |      |      |      |      |
| Max Green Setting (Gmax), s  |      | 35.2 |      |     | 26.5 | 35.2 |      | 36.0 |      |      |      |      |
| Max Q Clear Time (g_c+I1), s |      | 5.1  |      |     | 7.8  | 8.8  |      | 7.1  |      |      |      |      |
| Green Ext Time (p_c), s      |      | 3.2  |      |     | 0.5  | 3.7  |      | 0.9  |      |      |      |      |

### Intersection Summary

|                              |      |
|------------------------------|------|
| HCM 7th Control Delay, s/veh | 12.0 |
| HCM 7th LOS                  | B    |

### Notes

User approved volume balancing among the lanes for turning movement.  
 Unsignalized Delay for [NBR, EBR] is excluded from calculations of the approach delay and intersection delay.

Lanes, Volumes, Timings  
5: Norwood Avenue & Harris Avenue

12/20/2024

|                            |  |  |  |  |  |  |  |  |  |  |  |  |
|----------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Lane Group                 | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations        |   |  |  |   |  |  |  |  |  |  |  |  |
| Traffic Volume (vph)       | 230   | 14  | 39  | 17  | 6   | 93  | 17  | 602   | 14  | 56  | 736   | 105   |
| Future Volume (vph)        | 230   | 14  | 39  | 17  | 6   | 93  | 17  | 602   | 14  | 56  | 736   | 105   |
| Ideal Flow (vphpl)         | 1900  | 1900  | 1900  | 1900  | 1900  | 1900  | 1900  | 1900  | 1900  | 1900  | 1900  | 1900  |
| Storage Length (ft)        | 0   |   | 140   | 100   |   | 0   | 85  |   | 0   | 110   |   | 0   |
| Storage Lanes              | 0   |   | 1   | 1   |   | 1   | 1   |   | 0   | 1   |   | 0   |
| Taper Length (ft)          | 25  |   |   | 35  |   |   | 40  |   |   | 30  |   |   |
| Lane Util. Factor          | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 0.95  | 0.95  | 1.00  | 0.95  | 0.95  |
| Ped Bike Factor            |   |   | 0.97  |   | 0.99  | 0.98  | 0.98  | 0.99  |   | 0.99  | 0.99  |   |
| Frt                        |   |   | 0.850   |   |   | 0.850   |   | 0.997   |   |   |   | 0.981   |
| Flt Protected              |   | 0.955   |   |   | 0.964   |   | 0.950   |   |   | 0.950   |   |   |
| Satd. Flow (prot)          | 0   | 1762  | 1568  | 0   | 1778  | 1568  | 1787  | 3559  | 0   | 1752  | 3415  | 0   |
| Flt Permitted              |   | 0.955   |   |   | 0.964   |   | 0.950   |   |   | 0.950   |   |   |
| Satd. Flow (perm)          | 0   | 1762  | 1533  | 0   | 1769  | 1546  | 1768  | 3559  | 0   | 1737  | 3415  | 0   |
| Right Turn on Red          |   |   | Yes   |   |   | Yes   |   |   | Yes   |   |   | Yes   |
| Satd. Flow (RTOR)          |   |   | 39  |   |   | 93  |   | 1   |   |   |   | 9   |
| Link Speed (mph)           |   | 30  |   |   | 30  |   |   | 40  |   |   |   | 30  |
| Link Distance (ft)         |   | 735   |   |   | 595   |   |   | 331   |   |   |   | 737   |
| Travel Time (s)            |   | 16.7  |   |   | 13.5  |   |   | 5.6   |   |   |   | 16.8  |
| Confl. Peds. (#/hr)        |   |   | 5   | 5   |   |   | 9   |   | 4   | 4   |   | 9   |
| Confl. Bikes (#/hr)        |   |   | 2   |   |   | 2   |   |   | 7   |   |   | 1   |
| Peak Hour Factor           | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Heavy Vehicles (%)         | 3%  | 3%  | 3%  | 3%  | 3%  | 3%  | 1%  | 1%  | 1%  | 3%  | 3%  | 3%  |
| Adj. Flow (vph)            | 230   | 14  | 39  | 17  | 6   | 93  | 17  | 602   | 14  | 56  | 736   | 105   |
| Shared Lane Traffic (%)    |   |   |   |   |   |   |   |   |   |   |   |   |
| Lane Group Flow (vph)      | 0   | 244   | 39  | 0   | 23  | 93  | 17  | 616   | 0   | 56  | 841   | 0   |
| Enter Blocked Intersection | No  | No  | No  | No  | No  | No  |
| Lane Alignment             | Left  | Left  | Right   | Left  | Left  | Right   | Left  | Left  | Right   | Left  | Left  | Right   |
| Median Width(ft)           |   | 0   |   |   | 0   |   |   | 12  |   |   |   | 12  |
| Link Offset(ft)            |   | 0   |   |   | 0   |   |   | 0   |   |   |   | 0   |
| Crosswalk Width(ft)        |   | 16  |   |   | 16  |   |   | 16  |   |   |   | 16  |
| Two way Left Turn Lane     |   |   |   |   |   |   |   |   |   |   |   |   |
| Headway Factor             | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Turning Speed (mph)        | 15  |   | 9   | 15  |   | 9   | 15  |   | 9   | 15  |   | 9   |
| Number of Detectors        | 1   | 2   | 1   | 1   | 2   | 1   | 1   | 2   |   | 1   | 2   |   |
| Detector Template          | Left  | Thru  | Right   | Left  | Thru  | Right   | Left  | Thru  |   | Left  | Thru  |   |
| Leading Detector (ft)      | 20  | 100   | 20  | 20  | 100   | 20  | 20  | 100   |   | 20  | 100   |   |
| Trailing Detector (ft)     | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |   | 0   | 0   |   |
| Detector 1 Position(ft)    | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |   | 0   | 0   |   |
| Detector 1 Size(ft)        | 20  | 6   | 20  | 20  | 6   | 20  | 20  | 6   |   | 20  | 6   |   |
| Detector 1 Type            | Cl+Ex   | Cl+Ex   |   | Cl+Ex   | Cl+Ex   |   |
| Detector 1 Channel         |   |   |   |   |   |   |   |   |   |   |   |   |
| Detector 1 Extend (s)      | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |   | 0.0   | 0.0   |   |
| Detector 1 Queue (s)       | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |   | 0.0   | 0.0   |   |
| Detector 1 Delay (s)       | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |   | 0.0   | 0.0   |   |
| Detector 2 Position(ft)    |   | 94  |   |   | 94  |   |   | 94  |   |   |   | 94  |
| Detector 2 Size(ft)        |   | 6   |   |   | 6   |   |   | 6   |   |   |   | 6   |
| Detector 2 Type            |   | Cl+Ex   |   |   | Cl+Ex   |   |   | Cl+Ex   |   |   |   | Cl+Ex   |
| Detector 2 Channel         |   |   |   |   |   |   |   |   |   |   |   |   |

Lanes, Volumes, Timings  
5: Norwood Avenue & Harris Avenue

12/20/2024



| Lane Group              | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR | SBL   | SBT   | SBR |
|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-----|-------|-------|-----|
| Detector 2 Extend (s)   |       | 0.0   |       |       | 0.0   |       |       | 0.0   |     |       | 0.0   |     |
| Turn Type               | Split | NA    | pm+ov | Split | NA    | Perm  | Prot  | NA    |     | Prot  | NA    |     |
| Protected Phases        | 6     | 6     | 3     | 2     | 2     |       | 3     | 8     |     | 7     | 4     |     |
| Permitted Phases        |       |       | 6     |       |       | 2     |       |       |     |       |       |     |
| Detector Phase          | 6     | 6     | 3     | 2     | 2     | 2     | 3     | 8     |     | 7     | 4     |     |
| Switch Phase            |       |       |       |       |       |       |       |       |     |       |       |     |
| Minimum Initial (s)     | 10.0  | 10.0  | 10.0  | 11.0  | 11.0  | 11.0  | 10.0  | 7.0   |     | 9.0   | 8.0   |     |
| Minimum Split (s)       | 28.6  | 28.6  | 13.5  | 14.8  | 14.8  | 14.8  | 13.5  | 19.6  |     | 12.5  | 25.6  |     |
| Total Split (s)         | 40.0  | 40.0  | 40.0  | 40.0  | 40.0  | 40.0  | 40.0  | 40.0  |     | 40.0  | 40.0  |     |
| Total Split (%)         | 25.0% | 25.0% | 25.0% | 25.0% | 25.0% | 25.0% | 25.0% | 25.0% |     | 25.0% | 25.0% |     |
| Maximum Green (s)       | 36.4  | 36.4  | 36.5  | 36.2  | 36.2  | 36.2  | 36.5  | 35.4  |     | 36.5  | 35.4  |     |
| Yellow Time (s)         | 3.5   | 3.5   | 3.5   | 3.5   | 3.5   | 3.5   | 3.5   | 4.3   |     | 3.5   | 4.3   |     |
| All-Red Time (s)        | 0.1   | 0.1   | 0.0   | 0.3   | 0.3   | 0.3   | 0.0   | 0.3   |     | 0.0   | 0.3   |     |
| Lost Time Adjust (s)    |       | 0.0   | 0.0   |       | 0.0   | 0.0   | 0.0   | 0.0   |     | 0.0   | 0.0   |     |
| Total Lost Time (s)     |       | 3.6   | 3.5   |       | 3.8   | 3.8   | 3.5   | 4.6   |     | 3.5   | 4.6   |     |
| Lead/Lag                |       |       | Lead  |       |       |       | Lead  | Lag   |     | Lead  | Lag   |     |
| Lead-Lag Optimize?      |       |       | Yes   |       |       |       | Yes   | Yes   |     | Yes   | Yes   |     |
| Vehicle Extension (s)   | 2.0   | 2.0   | 2.0   | 2.0   | 2.0   | 2.0   | 2.0   | 2.5   |     | 2.0   | 2.5   |     |
| Recall Mode             | None  |     | None  | None  |     |
| Walk Time (s)           | 7.0   | 7.0   |       |       |       |       |       | 7.0   |     |       | 7.0   |     |
| Flash Dont Walk (s)     | 18.0  | 18.0  |       |       |       |       |       | 8.0   |     |       | 14.0  |     |
| Pedestrian Calls (#/hr) | 2     | 2     |       |       |       |       |       | 2     |     |       | 2     |     |
| Act Effct Green (s)     |       | 16.7  | 27.2  |       | 11.5  | 11.5  | 10.5  | 37.5  |     | 9.7   | 37.0  |     |
| Actuated g/C Ratio      |       | 0.20  | 0.33  |       | 0.14  | 0.14  | 0.13  | 0.45  |     | 0.12  | 0.45  |     |
| v/c Ratio               |       | 0.69  | 0.07  |       | 0.09  | 0.31  | 0.07  | 0.38  |     | 0.27  | 0.55  |     |
| Control Delay (s/veh)   |       | 43.4  | 6.5   |       | 37.7  | 12.1  | 38.5  | 19.4  |     | 42.1  | 21.9  |     |
| Queue Delay             |       | 0.0   | 0.0   |       | 0.0   | 0.0   | 0.0   | 0.0   |     | 0.0   | 0.0   |     |
| Total Delay (s/veh)     |       | 43.4  | 6.5   |       | 37.7  | 12.1  | 38.5  | 19.4  |     | 42.1  | 21.9  |     |
| LOS                     |       | D     | A     |       | D     | B     | D     | B     |     | D     | C     |     |
| Approach Delay (s/veh)  |       | 38.4  |       |       | 17.2  |       |       | 19.9  |     |       | 23.2  |     |
| Approach LOS            |       | D     |       |       | B     |       |       | B     |     |       | C     |     |
| Queue Length 50th (ft)  |       | 130   | 0     |       | 12    | 0     | 9     | 124   |     | 29    | 188   |     |
| Queue Length 95th (ft)  |       | 208   | 20    |       | 37    | 46    | 30    | 204   |     | 71    | 292   |     |
| Internal Link Dist (ft) |       | 655   |       |       | 515   |       |       | 251   |     |       | 657   |     |
| Turn Bay Length (ft)    |       |       | 140   |       |       |       | 85    |       |     | 110   |       |     |
| Base Capacity (vph)     |       | 806   | 1043  |       | 809   | 754   | 820   | 1610  |     | 804   | 1526  |     |
| Starvation Cap Reductn  |       | 0     | 0     |       | 0     | 0     | 0     | 0     |     | 0     | 0     |     |
| Spillback Cap Reductn   |       | 0     | 0     |       | 0     | 0     | 0     | 0     |     | 0     | 0     |     |
| Storage Cap Reductn     |       | 0     | 0     |       | 0     | 0     | 0     | 0     |     | 0     | 0     |     |
| Reduced v/c Ratio       |       | 0.30  | 0.04  |       | 0.03  | 0.12  | 0.02  | 0.38  |     | 0.07  | 0.55  |     |

Intersection Summary

|                                    |                        |
|------------------------------------|------------------------|
| Area Type:                         | Other                  |
| Cycle Length:                      | 160                    |
| Actuated Cycle Length:             | 83.1                   |
| Natural Cycle:                     | 85                     |
| Control Type:                      | Actuated-Uncoordinated |
| Maximum v/c Ratio:                 | 0.69                   |
| Intersection Signal Delay (s/veh): | 24.0                   |
| Intersection LOS:                  | C                      |

Lanes, Volumes, Timings  
 5: Norwood Avenue & Harris Avenue

12/20/2024

Intersection Capacity Utilization 62.9% ICU Level of Service B  
 Analysis Period (min) 15

Splits and Phases: 5: Norwood Avenue & Harris Avenue

|  |  |  |  |
|--|--|--|--|
|  Ø2 |  Ø6<br>40 s |  Ø3         |  Ø4         |
|  |  |  Ø7<br>40 s |  Ø8<br>40 s |

Queues

5: Norwood Avenue & Harris Avenue

12/20/2024



| Lane Group              | EBT  | EBR  | WBT  | WBR  | NBL  | NBT  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 244  | 39   | 23   | 93   | 17   | 616  | 56   | 841  |
| v/c Ratio               | 0.69 | 0.07 | 0.09 | 0.31 | 0.07 | 0.38 | 0.27 | 0.55 |
| Control Delay (s/veh)   | 43.4 | 6.5  | 37.7 | 12.1 | 38.5 | 19.4 | 42.1 | 21.9 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 43.4 | 6.5  | 37.7 | 12.1 | 38.5 | 19.4 | 42.1 | 21.9 |
| Queue Length 50th (ft)  | 130  | 0    | 12   | 0    | 9    | 124  | 29   | 188  |
| Queue Length 95th (ft)  | 208  | 20   | 37   | 46   | 30   | 204  | 71   | 292  |
| Internal Link Dist (ft) | 655  |      | 515  |      |      | 251  |      | 657  |
| Turn Bay Length (ft)    |      | 140  |      |      | 85   |      | 110  |      |
| Base Capacity (vph)     | 806  | 1043 | 809  | 754  | 820  | 1610 | 804  | 1526 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.30 | 0.04 | 0.03 | 0.12 | 0.02 | 0.38 | 0.07 | 0.55 |

Intersection Summary

# HCM 6th Signalized Intersection Summary

## 5: Norwood Avenue & Harris Avenue

12/20/2024

|  |  |  |  |  |  |  |  |  |  |  |  |  |
|--|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |   |  |  |   |  |  |  |  |  |  |  |  |
| Traffic Volume (veh/h)   | 230   | 14  | 39  | 17  | 6   | 93  | 17  | 602   | 14  | 56  | 736   | 105   |
| Future Volume (veh/h)  | 230   | 14  | 39  | 17  | 6   | 93  | 17  | 602   | 14  | 56  | 736   | 105   |
| Initial Q (Qb), veh  | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 0.98  | 1.00  |   | 0.96  | 1.00  |   | 0.95  | 1.00  |   | 0.97  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   | No  |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1856  | 1856  | 1856  | 1856  | 1856  | 1856  | 1885  | 1885  | 1885  | 1856  | 1856  | 1856  |
| Adj Flow Rate, veh/h   | 230   | 14  | 39  | 17  | 6   | 93  | 17  | 602   | 14  | 56  | 736   | 105   |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 3   | 3   | 3   | 3   | 3   | 3   | 1   | 1   | 1   | 3   | 3   | 3   |
| Cap, veh/h   | 319   | 19  | 359   | 216   | 76  | 247   | 74  | 995   | 23  | 165   | 1017  | 145   |
| Arrive On Green  | 0.19  | 0.19  | 0.19  | 0.16  | 0.16  | 0.16  | 0.04  | 0.28  | 0.28  | 0.09  | 0.33  | 0.33  |
| Sat Flow, veh/h  | 1670  | 102   | 1538  | 1323  | 467   | 1515  | 1795  | 3573  | 83  | 1767  | 3081  | 439   |
| Grp Volume(v), veh/h   | 244   | 0   | 39  | 23  | 0   | 93  | 17  | 301   | 315   | 56  | 421   | 420   |
| Grp Sat Flow(s),veh/h/ln   | 1772  | 0   | 1538  | 1789  | 0   | 1515  | 1795  | 1791  | 1866  | 1767  | 1763  | 1758  |
| Q Serve(g_s), s  | 7.3   | 0.0   | 1.1   | 0.6   | 0.0   | 3.1   | 0.5   | 8.2   | 8.3   | 1.7   | 11.9  | 11.9  |
| Cycle Q Clear(g_c), s  | 7.3   | 0.0   | 1.1   | 0.6   | 0.0   | 3.1   | 0.5   | 8.2   | 8.3   | 1.7   | 11.9  | 11.9  |
| Prop In Lane   | 0.94  |   | 1.00  | 0.74  |   | 1.00  | 1.00  |   | 0.04  | 1.00  |   | 0.25  |
| Lane Grp Cap(c), veh/h   | 338   | 0   | 359   | 292   | 0   | 247   | 74  | 499   | 519   | 165   | 582   | 580   |
| V/C Ratio(X)   | 0.72  | 0.00  | 0.11  | 0.08  | 0.00  | 0.38  | 0.23  | 0.60  | 0.61  | 0.34  | 0.72  | 0.72  |
| Avail Cap(c_a), veh/h  | 1142  | 0   | 1057  | 1147  | 0   | 971   | 1161  | 1123  | 1170  | 1142  | 1105  | 1102  |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Uniform Delay (d), s/veh   | 21.4  | 0.0   | 17.1  | 20.0  | 0.0   | 21.1  | 26.2  | 17.7  | 17.7  | 24.0  | 16.6  | 16.7  |
| Incr Delay (d2), s/veh   | 1.1   | 0.0   | 0.0   | 0.0   | 0.0   | 0.4   | 0.6   | 0.9   | 0.8   | 0.5   | 1.3   | 1.3   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 2.9   | 0.0   | 0.4   | 0.2   | 0.0   | 1.0   | 0.2   | 3.0   | 3.1   | 0.7   | 4.4   | 4.4   |
| Unsig. Movement Delay, s/veh   |   |   |   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 22.5  | 0.0   | 17.1  | 20.1  | 0.0   | 21.4  | 26.8  | 18.6  | 18.5  | 24.4  | 17.9  | 17.9  |
| LnGrp LOS  | C   |   | B   | C   |   | C   | C   | B   | B   | C   | B   | B   |
| Approach Vol, veh/h  |   | 283   |   |   | 116   |   |   | 633   |   |   | 897   |   |
| Approach Delay, s/veh  |   | 21.8  |   |   | 21.1  |   |   | 18.8  |   |   | 18.3  |   |
| Approach LOS   |   | C   |   |   | C   |   |   | B   |   |   | B   |   |
| Timer - Assigned Phs   |   | 2   | 3   | 4   |   | 6   | 7   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s   |   | 13.0  | 5.8   | 23.2  |   | 14.4  | 8.8   | 20.3  |   |   |   |   |
| Change Period (Y+Rc), s  |   | 3.8   | 3.5   | * 4.6   |   | 3.6   | 3.5   | * 4.6   |   |   |   |   |
| Max Green Setting (Gmax), s  |   | 36.2  | 36.5  | * 35  |   | 36.4  | 36.5  | * 35  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s   |   | 5.1   | 2.5   | 13.9  |   | 9.3   | 3.7   | 10.3  |   |   |   |   |
| Green Ext Time (p_c), s  |   | 0.2   | 0.0   | 4.6   |   | 1.0   | 0.1   | 2.8   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 6th Ctrl Delay, s/veh  |   |   | 19.2  |   |   |   |   |   |   |   |   |   |
| HCM 6th LOS  |   |   | B   |   |   |   |   |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| * HCM 6th computational engine requires equal clearance times for the phases crossing the barrier. |   |   |   |   |   |   |   |   |   |   |   |   |

# HCM 7th Signalized Intersection Summary

## 5: Norwood Avenue & Harris Avenue

12/20/2024

|  |  |  |  |  |  |  |  |  |  |  |  |  |
|--|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |   |  |  |   |  |  |  |  |  |  |  |  |
| Traffic Volume (veh/h)   | 230   | 14  | 39  | 17  | 6   | 93  | 17  | 602   | 14  | 56  | 736   | 105   |
| Future Volume (veh/h)  | 230   | 14  | 39  | 17  | 6   | 93  | 17  | 602   | 14  | 56  | 736   | 105   |
| Initial Q (Qb), veh  | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 0.98  | 1.00  |   | 0.96  | 1.00  |   | 0.95  | 1.00  |   | 0.97  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   | No  |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1856  | 1856  | 1856  | 1856  | 1856  | 1856  | 1885  | 1885  | 1885  | 1856  | 1856  | 1856  |
| Adj Flow Rate, veh/h   | 230   | 14  | 39  | 17  | 6   | 93  | 17  | 602   | 14  | 56  | 736   | 105   |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 3   | 3   | 3   | 3   | 3   | 3   | 1   | 1   | 1   | 3   | 3   | 3   |
| Cap, veh/h   | 319   | 19  | 359   | 216   | 76  | 247   | 74  | 995   | 23  | 165   | 1017  | 145   |
| Arrive On Green  | 0.19  | 0.19  | 0.19  | 0.16  | 0.16  | 0.16  | 0.04  | 0.28  | 0.28  | 0.09  | 0.33  | 0.33  |
| Sat Flow, veh/h  | 1670  | 102   | 1538  | 1323  | 467   | 1515  | 1795  | 3573  | 83  | 1767  | 3081  | 439   |
| Grp Volume(v), veh/h   | 244   | 0   | 39  | 23  | 0   | 93  | 17  | 301   | 315   | 56  | 421   | 420   |
| Grp Sat Flow(s),veh/h/ln   | 1772  | 0   | 1538  | 1789  | 0   | 1515  | 1795  | 1791  | 1866  | 1767  | 1763  | 1758  |
| Q Serve(g_s), s  | 7.3   | 0.0   | 1.1   | 0.6   | 0.0   | 3.1   | 0.5   | 8.2   | 8.3   | 1.7   | 11.9  | 11.9  |
| Cycle Q Clear(g_c), s  | 7.3   | 0.0   | 1.1   | 0.6   | 0.0   | 3.1   | 0.5   | 8.2   | 8.3   | 1.7   | 11.9  | 11.9  |
| Prop In Lane   | 0.94  |   | 1.00  | 0.74  |   | 1.00  | 1.00  |   | 0.04  | 1.00  |   | 0.25  |
| Lane Grp Cap(c), veh/h   | 338   | 0   | 359   | 292   | 0   | 247   | 74  | 499   | 519   | 165   | 582   | 580   |
| V/C Ratio(X)   | 0.72  | 0.00  | 0.11  | 0.08  | 0.00  | 0.38  | 0.23  | 0.60  | 0.61  | 0.34  | 0.72  | 0.72  |
| Avail Cap(c_a), veh/h  | 1142  | 0   | 1057  | 1147  | 0   | 971   | 1161  | 1123  | 1170  | 1142  | 1105  | 1102  |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Uniform Delay (d), s/veh   | 21.4  | 0.0   | 17.1  | 20.0  | 0.0   | 21.1  | 26.2  | 17.7  | 17.7  | 24.0  | 16.6  | 16.7  |
| Incr Delay (d2), s/veh   | 1.1   | 0.0   | 0.0   | 0.0   | 0.0   | 0.4   | 0.6   | 0.9   | 0.8   | 0.5   | 1.3   | 1.3   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 2.9   | 0.0   | 0.4   | 0.2   | 0.0   | 1.0   | 0.2   | 3.0   | 3.1   | 0.7   | 4.4   | 4.4   |
| Unsig. Movement Delay, s/veh   |   |   |   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 22.5  | 0.0   | 17.1  | 20.1  | 0.0   | 21.4  | 26.8  | 18.6  | 18.5  | 24.4  | 17.9  | 17.9  |
| LnGrp LOS  | C   |   | B   | C   |   | C   | C   | B   | B   | C   | B   | B   |
| Approach Vol, veh/h  |   | 283   |   |   | 116   |   |   | 633   |   |   | 897   |   |
| Approach Delay, s/veh  |   | 21.8  |   |   | 21.1  |   |   | 18.8  |   |   | 18.3  |   |
| Approach LOS   |   | C   |   |   | C   |   |   | B   |   |   | B   |   |
| Timer - Assigned Phs   |   | 2   | 3   | 4   |   | 6   | 7   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s   |   | 13.0  | 5.8   | 23.2  |   | 14.4  | 8.8   | 20.3  |   |   |   |   |
| Change Period (Y+Rc), s  |   | 3.8   | 3.5   | * 4.6   |   | 3.6   | 3.5   | * 4.6   |   |   |   |   |
| Max Green Setting (Gmax), s  |   | 36.2  | 36.5  | * 35  |   | 36.4  | 36.5  | * 35  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s   |   | 5.1   | 2.5   | 13.9  |   | 9.3   | 3.7   | 10.3  |   |   |   |   |
| Green Ext Time (p_c), s  |   | 0.2   | 0.0   | 4.6   |   | 1.0   | 0.1   | 2.8   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   |   |   | 19.2  |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS  |   |   | B   |   |   |   |   |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| * HCM 7th computational engine requires equal clearance times for the phases crossing the barrier. |   |   |   |   |   |   |   |   |   |   |   |   |

Lanes, Volumes, Timings  
6: Norwood Avenue & Silver Eagle Road

12/20/2024



| Lane Group                 | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations        |       |       |       |       |       |       |       |       |       |       |       |       |
| Traffic Volume (vph)       | 225   | 110   | 113   | 9     | 74    | 36    | 85    | 426   | 16    | 41    | 457   | 187   |
| Future Volume (vph)        | 225   | 110   | 113   | 9     | 74    | 36    | 85    | 426   | 16    | 41    | 457   | 187   |
| Ideal Flow (vphpl)         | 1900  | 1900  | 1900  | 1900  | 1900  | 1900  | 1900  | 1900  | 1900  | 1900  | 1900  | 1900  |
| Storage Length (ft)        | 105   |       | 0     | 0     |       | 0     | 90    |       | 0     | 50    |       | 0     |
| Storage Lanes              | 1     |       | 0     | 1     |       | 0     | 1     |       | 0     | 1     |       | 0     |
| Taper Length (ft)          | 25    |       |       | 25    |       |       | 35    |       |       | 55    |       |       |
| Lane Util. Factor          | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 0.95  | 0.95  | 1.00  | 0.95  | 0.95  |
| Ped Bike Factor            |       | 0.99  |       |       | 0.99  |       | 0.99  | 0.99  |       | 0.98  | 0.99  |       |
| Frt                        |       | 0.924 |       |       | 0.951 |       |       | 0.995 |       |       | 0.956 |       |
| Flt Protected              | 0.950 |       |       | 0.950 |       |       | 0.950 |       |       | 0.950 |       |       |
| Satd. Flow (prot)          | 1787  | 1726  | 0     | 1787  | 1781  | 0     | 1770  | 3515  | 0     | 1787  | 3388  | 0     |
| Flt Permitted              | 0.950 |       |       | 0.950 |       |       | 0.950 |       |       | 0.950 |       |       |
| Satd. Flow (perm)          | 1787  | 1726  | 0     | 1787  | 1781  | 0     | 1768  | 3515  | 0     | 1764  | 3388  | 0     |
| Right Turn on Red          |       |       | Yes   |       |       | Yes   |       |       | Yes   |       |       | Yes   |
| Satd. Flow (RTOR)          |       | 36    |       |       | 17    |       |       | 3     |       |       |       | 47    |
| Link Speed (mph)           |       | 30    |       |       | 30    |       |       | 40    |       |       |       | 30    |
| Link Distance (ft)         |       | 790   |       |       | 308   |       |       | 560   |       |       |       | 983   |
| Travel Time (s)            |       | 18.0  |       |       | 7.0   |       |       | 9.5   |       |       |       | 22.3  |
| Confl. Peds. (#/hr)        |       |       |       |       |       |       | 1     |       | 7     | 7     |       | 1     |
| Confl. Bikes (#/hr)        |       |       | 2     |       |       | 1     |       |       | 3     |       |       | 5     |
| Peak Hour Factor           | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Heavy Vehicles (%)         | 1%    | 1%    | 1%    | 1%    | 1%    | 1%    | 2%    | 2%    | 2%    | 1%    | 1%    | 1%    |
| Adj. Flow (vph)            | 225   | 110   | 113   | 9     | 74    | 36    | 85    | 426   | 16    | 41    | 457   | 187   |
| Shared Lane Traffic (%)    |       |       |       |       |       |       |       |       |       |       |       |       |
| Lane Group Flow (vph)      | 225   | 223   | 0     | 9     | 110   | 0     | 85    | 442   | 0     | 41    | 644   | 0     |
| Enter Blocked Intersection | No    |
| Lane Alignment             | Left  | Left  | Right |
| Median Width(ft)           |       | 12    |       |       | 12    |       |       | 12    |       |       |       | 12    |
| Link Offset(ft)            |       | 0     |       |       | 0     |       |       | 0     |       |       |       | 0     |
| Crosswalk Width(ft)        |       | 16    |       |       | 16    |       |       | 16    |       |       |       | 16    |
| Two way Left Turn Lane     |       |       |       |       |       |       |       | Yes   |       |       |       | Yes   |
| Headway Factor             | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Turning Speed (mph)        | 15    |       | 9     | 15    |       | 9     | 15    |       | 9     | 15    |       | 9     |
| Number of Detectors        | 1     | 2     |       | 1     | 2     |       | 1     | 2     |       | 1     | 2     |       |
| Detector Template          | Left  | Thru  |       |
| Leading Detector (ft)      | 20    | 100   |       | 20    | 100   |       | 20    | 100   |       | 20    | 100   |       |
| Trailing Detector (ft)     | 0     | 0     |       | 0     | 0     |       | 0     | 0     |       | 0     | 0     |       |
| Detector 1 Position(ft)    | 0     | 0     |       | 0     | 0     |       | 0     | 0     |       | 0     | 0     |       |
| Detector 1 Size(ft)        | 20    | 6     |       | 20    | 6     |       | 20    | 6     |       | 20    | 6     |       |
| Detector 1 Type            | Cl+Ex | Cl+Ex |       |
| Detector 1 Channel         |       |       |       |       |       |       |       |       |       |       |       |       |
| Detector 1 Extend (s)      | 0.0   | 0.0   |       | 0.0   | 0.0   |       | 0.0   | 0.0   |       | 0.0   | 0.0   |       |
| Detector 1 Queue (s)       | 0.0   | 0.0   |       | 0.0   | 0.0   |       | 0.0   | 0.0   |       | 0.0   | 0.0   |       |
| Detector 1 Delay (s)       | 0.0   | 0.0   |       | 0.0   | 0.0   |       | 0.0   | 0.0   |       | 0.0   | 0.0   |       |
| Detector 2 Position(ft)    |       | 94    |       |       | 94    |       |       | 94    |       |       |       | 94    |
| Detector 2 Size(ft)        |       | 6     |       |       | 6     |       |       | 6     |       |       |       | 6     |
| Detector 2 Type            |       | Cl+Ex |       |       | Cl+Ex |       |       | Cl+Ex |       |       |       | Cl+Ex |
| Detector 2 Channel         |       |       |       |       |       |       |       |       |       |       |       |       |

Lanes, Volumes, Timings  
6: Norwood Avenue & Silver Eagle Road

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| Lane Group              | EBL   | EBT   | EBR | WBL   | WBT   | WBR | NBL   | NBT   | NBR | SBL   | SBT   | SBR |
|-------------------------|-------|-------|-----|-------|-------|-----|-------|-------|-----|-------|-------|-----|
| Detector 2 Extend (s)   |       | 0.0   |     |       | 0.0   |     |       | 0.0   |     |       | 0.0   |     |
| Turn Type               | Prot  | NA    |     |
| Protected Phases        | 1     | 6     |     | 5     | 2     |     | 3     | 8     |     | 7     | 4     |     |
| Permitted Phases        |       |       |     |       |       |     |       |       |     |       |       |     |
| Detector Phase          | 1     | 6     |     | 5     | 2     |     | 3     | 8     |     | 7     | 4     |     |
| Switch Phase            |       |       |     |       |       |     |       |       |     |       |       |     |
| Minimum Initial (s)     | 10.0  | 9.0   |     | 10.0  | 10.0  |     | 9.0   | 8.0   |     | 9.0   | 8.0   |     |
| Minimum Split (s)       | 13.5  | 27.9  |     | 13.5  | 27.5  |     | 12.5  | 23.6  |     | 12.5  | 27.6  |     |
| Total Split (s)         | 30.0  | 30.0  |     | 30.0  | 30.0  |     | 30.0  | 40.0  |     | 30.0  | 40.0  |     |
| Total Split (%)         | 23.1% | 23.1% |     | 23.1% | 23.1% |     | 23.1% | 30.8% |     | 23.1% | 30.8% |     |
| Maximum Green (s)       | 26.5  | 26.1  |     | 26.5  | 26.5  |     | 26.5  | 35.4  |     | 26.5  | 35.4  |     |
| Yellow Time (s)         | 3.5   | 3.9   |     | 3.5   | 3.5   |     | 3.5   | 4.3   |     | 3.5   | 4.3   |     |
| All-Red Time (s)        | 0.0   | 0.0   |     | 0.0   | 0.0   |     | 0.0   | 0.3   |     | 0.0   | 0.3   |     |
| Lost Time Adjust (s)    | 0.0   | 0.0   |     | 0.0   | 0.0   |     | 0.0   | 0.0   |     | 0.0   | 0.0   |     |
| Total Lost Time (s)     | 3.5   | 3.9   |     | 3.5   | 3.5   |     | 3.5   | 4.6   |     | 3.5   | 4.6   |     |
| Lead/Lag                | Lead  | Lag   |     |
| Lead-Lag Optimize?      | Yes   | Yes   |     |
| Vehicle Extension (s)   | 2.0   | 2.0   |     | 2.0   | 2.0   |     | 2.0   | 2.0   |     | 2.0   | 2.0   |     |
| Recall Mode             | None  | None  |     | None  | None  |     | None  | Min   |     | None  | Min   |     |
| Walk Time (s)           |       | 7.0   |     |       | 7.0   |     |       | 7.0   |     |       | 7.0   |     |
| Flash Dont Walk (s)     |       | 17.0  |     |       | 17.0  |     |       | 12.0  |     |       | 16.0  |     |
| Pedestrian Calls (#/hr) |       | 2     |     |       | 2     |     |       | 2     |     |       | 2     |     |
| Act Effct Green (s)     | 16.3  | 25.9  |     | 12.2  | 14.0  |     | 11.7  | 22.8  |     | 11.1  | 19.4  |     |
| Actuated g/C Ratio      | 0.24  | 0.39  |     | 0.18  | 0.21  |     | 0.17  | 0.34  |     | 0.17  | 0.29  |     |
| v/c Ratio               | 0.52  | 0.32  |     | 0.02  | 0.28  |     | 0.27  | 0.36  |     | 0.13  | 0.63  |     |
| Control Delay (s/veh)   | 32.8  | 16.3  |     | 36.5  | 28.1  |     | 36.0  | 20.9  |     | 36.5  | 25.4  |     |
| Queue Delay             | 0.0   | 0.0   |     | 0.0   | 0.0   |     | 0.0   | 0.0   |     | 0.0   | 0.0   |     |
| Total Delay (s/veh)     | 32.8  | 16.3  |     | 36.5  | 28.1  |     | 36.0  | 20.9  |     | 36.5  | 25.4  |     |
| LOS                     | C     | B     |     | D     | C     |     | D     | C     |     | D     | C     |     |
| Approach Delay (s/veh)  |       | 24.6  |     |       | 28.7  |     |       | 23.4  |     |       | 26.1  |     |
| Approach LOS            |       | C     |     |       | C     |     |       | C     |     |       | C     |     |
| Queue Length 50th (ft)  | 82    | 48    |     | 3     | 34    |     | 31    | 76    |     | 15    | 111   |     |
| Queue Length 95th (ft)  | 219   | 159   |     | 22    | 104   |     | 105   | 169   |     | 63    | 255   |     |
| Internal Link Dist (ft) |       | 710   |     |       | 228   |     |       | 480   |     |       | 903   |     |
| Turn Bay Length (ft)    | 105   |       |     |       |       |     | 90    |       |     | 50    |       |     |
| Base Capacity (vph)     | 857   | 896   |     | 857   | 863   |     | 849   | 2065  |     | 857   | 2009  |     |
| Starvation Cap Reductn  | 0     | 0     |     | 0     | 0     |     | 0     | 0     |     | 0     | 0     |     |
| Spillback Cap Reductn   | 0     | 0     |     | 0     | 0     |     | 0     | 0     |     | 0     | 0     |     |
| Storage Cap Reductn     | 0     | 0     |     | 0     | 0     |     | 0     | 0     |     | 0     | 0     |     |
| Reduced v/c Ratio       | 0.26  | 0.25  |     | 0.01  | 0.13  |     | 0.10  | 0.21  |     | 0.05  | 0.32  |     |

Intersection Summary

|                                    |                        |
|------------------------------------|------------------------|
| Area Type:                         | Other                  |
| Cycle Length:                      | 130                    |
| Actuated Cycle Length:             | 67.2                   |
| Natural Cycle:                     | 85                     |
| Control Type:                      | Actuated-Uncoordinated |
| Maximum v/c Ratio:                 | 0.64                   |
| Intersection Signal Delay (s/veh): | 25.1                   |
| Intersection LOS:                  | C                      |

Lanes, Volumes, Timings  
 6: Norwood Avenue & Silver Eagle Road

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Intersection Capacity Utilization 55.8% ICU Level of Service B  
 Analysis Period (min) 15

Splits and Phases: 6: Norwood Avenue & Silver Eagle Road

|   |   |  |   |
|---|---|--|---|
|  Ø1<br> |  Ø2<br> |  Ø3<br> |  Ø4<br> |
|  Ø5<br> |  Ø6<br> |  Ø7<br> |  Ø8<br> |

Queues

6: Norwood Avenue & Silver Eagle Road

12/20/2024



| Lane Group              | EBL  | EBT  | WBL  | WBT  | NBL  | NBT  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 225  | 223  | 9    | 110  | 85   | 442  | 41   | 644  |
| v/c Ratio               | 0.52 | 0.32 | 0.02 | 0.28 | 0.27 | 0.36 | 0.13 | 0.63 |
| Control Delay (s/veh)   | 32.8 | 16.3 | 36.5 | 28.1 | 36.0 | 20.9 | 36.5 | 25.4 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 32.8 | 16.3 | 36.5 | 28.1 | 36.0 | 20.9 | 36.5 | 25.4 |
| Queue Length 50th (ft)  | 82   | 48   | 3    | 34   | 31   | 76   | 15   | 111  |
| Queue Length 95th (ft)  | 219  | 159  | 22   | 104  | 105  | 169  | 63   | 255  |
| Internal Link Dist (ft) |      | 710  |      | 228  |      | 480  |      | 903  |
| Turn Bay Length (ft)    | 105  |      |      |      | 90   |      | 50   |      |
| Base Capacity (vph)     | 857  | 896  | 857  | 863  | 849  | 2065 | 857  | 2009 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.26 | 0.25 | 0.01 | 0.13 | 0.10 | 0.21 | 0.05 | 0.32 |

Intersection Summary

# HCM 6th Signalized Intersection Summary

## 6: Norwood Avenue & Silver Eagle Road

12/20/2024



| Movement   | EBL  | EBT   | EBR  | WBL   | WBT  | WBR  | NBL  | NBT   | NBR  | SBL  | SBT  | SBR  |
|--|------|-------|------|-------|------|------|------|-------|------|------|------|------|
| Lane Configurations  |      |       |      |       |      |      |      |       |      |      |      |      |
| Traffic Volume (veh/h)   | 225  | 110   | 113  | 9     | 74   | 36   | 85   | 426   | 16   | 41   | 457  | 187  |
| Future Volume (veh/h)  | 225  | 110   | 113  | 9     | 74   | 36   | 85   | 426   | 16   | 41   | 457  | 187  |
| Initial Q (Qb), veh  | 0    | 0     | 0    | 0     | 0    | 0    | 0    | 0     | 0    | 0    | 0    | 0    |
| Ped-Bike Adj(A_pbT)  | 1.00 |       | 0.98 | 1.00  |      | 0.98 | 1.00 |       | 0.97 | 1.00 |      | 0.96 |
| Parking Bus, Adj   | 1.00 | 1.00  | 1.00 | 1.00  | 1.00 | 1.00 | 1.00 | 1.00  | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach  |      | No    |      |       | No   |      |      | No    |      |      | No   |      |
| Adj Sat Flow, veh/h/ln   | 1885 | 1885  | 1885 | 1885  | 1885 | 1885 | 1870 | 1870  | 1870 | 1885 | 1885 | 1885 |
| Adj Flow Rate, veh/h   | 225  | 110   | 113  | 9     | 74   | 36   | 85   | 426   | 16   | 41   | 457  | 187  |
| Peak Hour Factor   | 1.00 | 1.00  | 1.00 | 1.00  | 1.00 | 1.00 | 1.00 | 1.00  | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, %   | 1    | 1     | 1    | 1     | 1    | 1    | 2    | 2     | 2    | 1    | 1    | 1    |
| Cap, veh/h   | 320  | 256   | 263  | 42    | 177  | 86   | 214  | 1081  | 40   | 137  | 654  | 265  |
| Arrive On Green  | 0.18 | 0.30  | 0.30 | 0.02  | 0.15 | 0.15 | 0.12 | 0.31  | 0.31 | 0.08 | 0.27 | 0.27 |
| Sat Flow, veh/h  | 1795 | 842   | 865  | 1795  | 1188 | 578  | 1781 | 3487  | 131  | 1795 | 2454 | 994  |
| Grp Volume(v), veh/h   | 225  | 0     | 223  | 9     | 0    | 110  | 85   | 217   | 225  | 41   | 332  | 312  |
| Grp Sat Flow(s),veh/h/ln   | 1795 | 0     | 1706 | 1795  | 0    | 1766 | 1781 | 1777  | 1841 | 1795 | 1791 | 1658 |
| Q Serve(g_s), s  | 6.4  | 0.0   | 5.7  | 0.3   | 0.0  | 3.1  | 2.4  | 5.2   | 5.2  | 1.2  | 9.1  | 9.2  |
| Cycle Q Clear(g_c), s  | 6.4  | 0.0   | 5.7  | 0.3   | 0.0  | 3.1  | 2.4  | 5.2   | 5.2  | 1.2  | 9.1  | 9.2  |
| Prop In Lane   | 1.00 |       | 0.51 | 1.00  |      | 0.33 | 1.00 |       | 0.07 | 1.00 |      | 0.60 |
| Lane Grp Cap(c), veh/h   | 320  | 0     | 519  | 42    | 0    | 264  | 214  | 551   | 571  | 137  | 477  | 442  |
| V/C Ratio(X)   | 0.70 | 0.00  | 0.43 | 0.21  | 0.00 | 0.42 | 0.40 | 0.39  | 0.40 | 0.30 | 0.70 | 0.71 |
| Avail Cap(c_a), veh/h  | 878  | 0     | 822  | 878   | 0    | 864  | 871  | 1161  | 1203 | 878  | 1170 | 1083 |
| HCM Platoon Ratio  | 1.00 | 1.00  | 1.00 | 1.00  | 1.00 | 1.00 | 1.00 | 1.00  | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I)   | 1.00 | 0.00  | 1.00 | 1.00  | 0.00 | 1.00 | 1.00 | 1.00  | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh   | 20.9 | 0.0   | 15.1 | 26.0  | 0.0  | 20.9 | 22.0 | 14.7  | 14.7 | 23.6 | 17.9 | 18.0 |
| Incr Delay (d2), s/veh   | 1.1  | 0.0   | 0.2  | 0.9   | 0.0  | 0.4  | 0.4  | 0.2   | 0.2  | 0.4  | 0.7  | 0.8  |
| Initial Q Delay(d3), s/veh   | 0.0  | 0.0   | 0.0  | 0.0   | 0.0  | 0.0  | 0.0  | 0.0   | 0.0  | 0.0  | 0.0  | 0.0  |
| %ile BackOfQ(50%),veh/ln   | 2.5  | 0.0   | 2.0  | 0.1   | 0.0  | 1.2  | 0.9  | 1.8   | 1.8  | 0.5  | 3.4  | 3.2  |
| Unsig. Movement Delay, s/veh   |      |       |      |       |      |      |      |       |      |      |      |      |
| LnGrp Delay(d), s/veh  | 22.0 | 0.0   | 15.3 | 26.9  | 0.0  | 21.3 | 22.5 | 14.9  | 14.9 | 24.1 | 18.6 | 18.7 |
| LnGrp LOS  | C    |       | B    | C     |      | C    | C    | B     | B    | C    | B    | B    |
| Approach Vol, veh/h  |      | 448   |      |       | 119  |      |      | 527   |      |      | 685  |      |
| Approach Delay, s/veh  |      | 18.6  |      |       | 21.7 |      |      | 16.1  |      |      | 19.0 |      |
| Approach LOS   |      | B     |      |       | C    |      |      | B     |      |      | B    |      |
| Timer - Assigned Phs   | 1    | 2     | 3    | 4     | 5    | 6    | 7    | 8     |      |      |      |      |
| Phs Duration (G+Y+Rc), s   | 13.2 | 12.0  | 10.0 | 19.0  | 4.8  | 20.4 | 7.6  | 21.4  |      |      |      |      |
| Change Period (Y+Rc), s  | 3.5  | * 3.9 | 3.5  | * 4.6 | 3.5  | 3.9  | 3.5  | * 4.6 |      |      |      |      |
| Max Green Setting (Gmax), s  | 26.5 | * 27  | 26.5 | * 35  | 26.5 | 26.1 | 26.5 | * 35  |      |      |      |      |
| Max Q Clear Time (g_c+I1), s   | 8.4  | 5.1   | 4.4  | 11.2  | 2.3  | 7.7  | 3.2  | 7.2   |      |      |      |      |
| Green Ext Time (p_c), s  | 0.3  | 0.3   | 0.1  | 2.8   | 0.0  | 0.8  | 0.0  | 1.5   |      |      |      |      |
| <b>Intersection Summary</b>  |      |       |      |       |      |      |      |       |      |      |      |      |
| HCM 6th Ctrl Delay, s/veh  |      |       | 18.2 |       |      |      |      |       |      |      |      |      |
| HCM 6th LOS  |      |       | B    |       |      |      |      |       |      |      |      |      |
| <b>Notes</b>   |      |       |      |       |      |      |      |       |      |      |      |      |
| * HCM 6th computational engine requires equal clearance times for the phases crossing the barrier. |      |       |      |       |      |      |      |       |      |      |      |      |

HCM 7th Signalized Intersection Summary  
 6: Norwood Avenue & Silver Eagle Road

12/20/2024



| Movement   | EBL  | EBT   | EBR  | WBL   | WBT  | WBR  | NBL  | NBT   | NBR  | SBL  | SBT  | SBR  |
|--|------|-------|------|-------|------|------|------|-------|------|------|------|------|
| Lane Configurations  |      |       |      |       |      |      |      |       |      |      |      |      |
| Traffic Volume (veh/h)   | 225  | 110   | 113  | 9     | 74   | 36   | 85   | 426   | 16   | 41   | 457  | 187  |
| Future Volume (veh/h)  | 225  | 110   | 113  | 9     | 74   | 36   | 85   | 426   | 16   | 41   | 457  | 187  |
| Initial Q (Qb), veh  | 0    | 0     | 0    | 0     | 0    | 0    | 0    | 0     | 0    | 0    | 0    | 0    |
| Lane Width Adj.  | 1.00 | 1.00  | 1.00 | 1.00  | 1.00 | 1.00 | 1.00 | 1.00  | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped-Bike Adj(A_pbT)  | 1.00 |       | 0.98 | 1.00  |      | 0.98 | 1.00 |       | 0.97 | 1.00 |      | 0.96 |
| Parking Bus, Adj   | 1.00 | 1.00  | 1.00 | 1.00  | 1.00 | 1.00 | 1.00 | 1.00  | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach  |      | No    |      |       | No   |      |      | No    |      |      | No   |      |
| Adj Sat Flow, veh/h/ln   | 1885 | 1885  | 1885 | 1885  | 1885 | 1885 | 1870 | 1870  | 1870 | 1885 | 1885 | 1885 |
| Adj Flow Rate, veh/h   | 225  | 110   | 113  | 9     | 74   | 36   | 85   | 426   | 16   | 41   | 457  | 187  |
| Peak Hour Factor   | 1.00 | 1.00  | 1.00 | 1.00  | 1.00 | 1.00 | 1.00 | 1.00  | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, %   | 1    | 1     | 1    | 1     | 1    | 1    | 2    | 2     | 2    | 1    | 1    | 1    |
| Cap, veh/h   | 320  | 256   | 263  | 42    | 177  | 86   | 214  | 1081  | 40   | 137  | 654  | 265  |
| Arrive On Green  | 0.18 | 0.30  | 0.30 | 0.02  | 0.15 | 0.15 | 0.12 | 0.31  | 0.31 | 0.08 | 0.27 | 0.27 |
| Sat Flow, veh/h  | 1795 | 842   | 865  | 1795  | 1188 | 578  | 1781 | 3487  | 131  | 1795 | 2454 | 994  |
| Grp Volume(v), veh/h   | 225  | 0     | 223  | 9     | 0    | 110  | 85   | 217   | 225  | 41   | 332  | 312  |
| Grp Sat Flow(s),veh/h/ln   | 1795 | 0     | 1706 | 1795  | 0    | 1766 | 1781 | 1777  | 1841 | 1795 | 1791 | 1658 |
| Q Serve(g_s), s  | 6.4  | 0.0   | 5.7  | 0.3   | 0.0  | 3.1  | 2.4  | 5.2   | 5.2  | 1.2  | 9.1  | 9.2  |
| Cycle Q Clear(g_c), s  | 6.4  | 0.0   | 5.7  | 0.3   | 0.0  | 3.1  | 2.4  | 5.2   | 5.2  | 1.2  | 9.1  | 9.2  |
| Prop In Lane   | 1.00 |       | 0.51 | 1.00  |      | 0.33 | 1.00 |       | 0.07 | 1.00 |      | 0.60 |
| Lane Grp Cap(c), veh/h   | 320  | 0     | 519  | 42    | 0    | 264  | 214  | 551   | 571  | 137  | 477  | 442  |
| V/C Ratio(X)   | 0.70 | 0.00  | 0.43 | 0.21  | 0.00 | 0.42 | 0.40 | 0.39  | 0.40 | 0.30 | 0.70 | 0.71 |
| Avail Cap(c_a), veh/h  | 878  | 0     | 822  | 878   | 0    | 864  | 871  | 1161  | 1203 | 878  | 1170 | 1083 |
| HCM Platoon Ratio  | 1.00 | 1.00  | 1.00 | 1.00  | 1.00 | 1.00 | 1.00 | 1.00  | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I)   | 1.00 | 0.00  | 1.00 | 1.00  | 0.00 | 1.00 | 1.00 | 1.00  | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh   | 20.9 | 0.0   | 15.1 | 26.0  | 0.0  | 20.9 | 22.0 | 14.7  | 14.7 | 23.6 | 17.9 | 18.0 |
| Incr Delay (d2), s/veh   | 1.1  | 0.0   | 0.2  | 0.9   | 0.0  | 0.4  | 0.4  | 0.2   | 0.2  | 0.4  | 0.7  | 0.8  |
| Initial Q Delay(d3), s/veh   | 0.0  | 0.0   | 0.0  | 0.0   | 0.0  | 0.0  | 0.0  | 0.0   | 0.0  | 0.0  | 0.0  | 0.0  |
| %ile BackOfQ(50%),veh/ln   | 2.5  | 0.0   | 2.0  | 0.1   | 0.0  | 1.2  | 0.9  | 1.8   | 1.8  | 0.5  | 3.4  | 3.2  |
| Unsig. Movement Delay, s/veh   |      |       |      |       |      |      |      |       |      |      |      |      |
| LnGrp Delay(d), s/veh  | 22.0 | 0.0   | 15.3 | 26.9  | 0.0  | 21.3 | 22.5 | 14.9  | 14.9 | 24.1 | 18.6 | 18.7 |
| LnGrp LOS  | C    |       | B    | C     |      | C    | C    | B     | B    | C    | B    | B    |
| Approach Vol, veh/h  |      | 448   |      |       | 119  |      |      | 527   |      |      | 685  |      |
| Approach Delay, s/veh  |      | 18.6  |      |       | 21.7 |      |      | 16.1  |      |      | 19.0 |      |
| Approach LOS   |      | B     |      |       | C    |      |      | B     |      |      | B    |      |
| Timer - Assigned Phs   | 1    | 2     | 3    | 4     | 5    | 6    | 7    | 8     |      |      |      |      |
| Phs Duration (G+Y+Rc), s   | 13.2 | 12.0  | 10.0 | 19.0  | 4.8  | 20.4 | 7.6  | 21.4  |      |      |      |      |
| Change Period (Y+Rc), s  | 3.5  | * 3.9 | 3.5  | * 4.6 | 3.5  | 3.9  | 3.5  | * 4.6 |      |      |      |      |
| Max Green Setting (Gmax), s  | 26.5 | * 27  | 26.5 | * 35  | 26.5 | 26.1 | 26.5 | * 35  |      |      |      |      |
| Max Q Clear Time (g_c+I1), s   | 8.4  | 5.1   | 4.4  | 11.2  | 2.3  | 7.7  | 3.2  | 7.2   |      |      |      |      |
| Green Ext Time (p_c), s  | 0.3  | 0.3   | 0.1  | 2.8   | 0.0  | 0.8  | 0.0  | 1.5   |      |      |      |      |
| <b>Intersection Summary</b>  |      |       |      |       |      |      |      |       |      |      |      |      |
| HCM 7th Control Delay, s/veh   |      |       | 18.2 |       |      |      |      |       |      |      |      |      |
| HCM 7th LOS  |      |       | B    |       |      |      |      |       |      |      |      |      |
| <b>Notes</b>   |      |       |      |       |      |      |      |       |      |      |      |      |
| * HCM 7th computational engine requires equal clearance times for the phases crossing the barrier. |      |       |      |       |      |      |      |       |      |      |      |      |

## **Appendix E: Community Survey Results & Comments**

---

| Entry # | Q1. What is your zip code? | Q2. Daily | Q2. Some Days | Q2. Weekly | Q2. Every Couple of Weeks | Q2. Monthly | Q2. Rarely | Q3. Riding                        |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
|---------|----------------------------|-----------|---------------|------------|---------------------------|-------------|------------|-----------------------------------|----------------------------------|--------------------|-----------------|---------------------|---------------|--------------|-------------------|-----------|-----|-----|--|-----|
|         |                            |           |               |            |                           |             |            | Q3. Driving in a Personal Vehicle | Q3. Riding in a Personal Vehicle | Q3. Public Transit | Q3. Paratransit | Q3. Walking/Rolling | Q3. Bicycling | Q3. Scooting | Q3. Rider-Sharing | Q3. Other |     |     |  |     |
| 1       | 95828                      | YES       |               |            |                           |             |            |                                   |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
| 2       | 95831                      |           |               |            |                           |             | YES        |                                   |                                  |                    |                 |                     |               |              |                   |           |     |     |  | CAR |
| 3       | 95815                      | YES       |               |            |                           |             |            | YES                               |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
| 4       | 95815                      |           | YES           |            |                           |             |            | YES                               |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
| 5       | 95825                      | YES       |               |            |                           |             |            | YES                               |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
| 6       | 95815                      | YES       |               |            |                           |             |            |                                   |                                  |                    |                 |                     | YES           | YES          |                   |           |     |     |  |     |
| 7       | 95834                      |           | YES           |            | YES                       |             |            | YES                               |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
| 8       | 95838                      | YES       |               |            |                           |             |            | YES                               |                                  |                    | YES             |                     |               |              |                   |           |     |     |  |     |
| 9       | 95833                      | YES       |               |            |                           |             |            | YES                               |                                  |                    | YES             |                     |               |              |                   |           |     |     |  |     |
| 10      | 95838                      | YES       |               |            |                           |             |            | YES                               |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
| 11      | 9532                       | YES       |               |            |                           |             |            |                                   |                                  | YES                | YES             |                     |               |              |                   |           |     |     |  |     |
| 12      | 95838                      |           | YES           |            |                           |             |            | YES                               |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
| 13      | 95815                      | YES       |               |            |                           |             |            | YES                               |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
| 14      | 95838                      | YES       |               |            |                           |             |            | YES                               |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
| 15      | 958608                     |           |               |            |                           | YES         |            | YES                               |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
| 16      | 95838                      | YES       |               |            |                           |             |            | YES                               |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
| 17      | 95811                      | YES       |               |            |                           |             |            | YES                               |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
| 18      | 95673                      | YES       |               |            |                           |             |            | YES                               |                                  |                    | YES             |                     |               |              |                   |           |     |     |  |     |
| 19      | 95815                      | YES       |               |            |                           |             |            | YES                               |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
| 20      | 95838                      | YES       |               |            |                           |             |            |                                   |                                  |                    |                 | YES                 |               |              |                   |           |     |     |  |     |
| 21      | 95838                      | YES       |               |            |                           |             |            | YES                               |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
| 22      | 95838                      | YES       | YES           |            |                           |             |            |                                   |                                  |                    |                 |                     |               | YES          |                   |           |     | YES |  |     |
| 23      | 958115                     | YES       |               |            |                           |             |            | YES                               |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
| 24      | 95838                      |           |               |            |                           | YES         |            | YES                               |                                  |                    | YES             |                     |               | YES          |                   |           |     |     |  |     |
| 25      | 95815                      | YES       |               |            |                           |             |            |                                   |                                  |                    |                 |                     |               | YES          |                   |           |     |     |  | YES |
| 26      | 95673                      |           |               |            |                           |             | YES        | YES                               |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
| 27      | 95888                      | YES       |               |            |                           |             |            |                                   |                                  |                    | YES             |                     |               |              |                   |           |     | YES |  |     |
| 28      | 95833                      | YES       |               |            |                           |             |            |                                   |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
| 29      | 95823                      | YES       |               |            |                           |             |            | YES                               |                                  |                    | YES             |                     |               |              |                   |           |     |     |  |     |
| 30      | 95838                      | YES       |               |            |                           |             |            | YES                               |                                  | YES                | YES             | YES                 | YES           | YES          | YES               | YES       | YES |     |  |     |
| 31      | 95838                      | YES       |               |            |                           |             |            |                                   |                                  |                    | YES             |                     |               | YES          | YES               |           |     |     |  |     |
| 32      | 95838                      | YES       |               |            |                           |             |            |                                   |                                  |                    |                 |                     |               | YES          |                   |           |     |     |  |     |
| 33      | 95838                      | YES       |               |            |                           |             |            | YES                               |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
| 34      | 95815                      | YES       |               |            |                           |             |            | YES                               |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
| 35      | 95815                      | YES       |               |            |                           |             |            | YES                               |                                  | YES                |                 |                     |               |              |                   |           |     |     |  |     |
| 36      | 95815                      | YES       |               |            |                           |             |            | YES                               |                                  |                    |                 |                     |               |              |                   |           |     |     |  |     |
| 37      | 95834                      | YES       |               |            |                           |             |            | YES                               |                                  |                    |                 |                     |               | YES          |                   |           |     |     |  |     |
| 38      | 8538                       | YES       |               |            |                           |             |            | YES                               |                                  | YES                | YES             |                     |               | YES          |                   |           |     |     |  |     |

|    |       |     |   |   |     |     |   |     |   |   |   |
|----|-------|-----|---|---|-----|-----|---|-----|---|---|---|
| 39 | 95838 | YES |   |   | YES |     |   |     |   |   |   |
| 40 | 95815 | YES |   |   | YES | YES |   |     |   |   |   |
| 41 | 95815 | YES |   |   | YES |     |   |     |   |   |   |
| 42 | 95838 | YES |   |   | YES |     |   | YES |   |   |   |
| 1  | 95838 | 1   |   |   |     | 1   | 1 |     |   |   |   |
| 2  | 95838 | 1   |   |   |     | 1   |   |     |   |   |   |
| 3  | 95815 | 1   |   |   |     | 1   | 1 |     | 1 | 1 |   |
| 4  | 95835 |     | 1 |   |     | 1   |   |     |   |   |   |
| 5  |       |     |   | 1 |     | 1   | 1 | 1   | 1 |   |   |
| 6  | 95815 | 1   |   |   |     | 1   |   |     |   |   |   |
| 7  | 95838 | 1   |   |   |     | 1   | 1 |     | 1 | 1 | 1 |



|   |   |     |   |     |   |     |     |     |
|---|---|-----|---|-----|---|-----|-----|-----|
|   |   | YES |   | YES |   | YES |     | YES |
|   |   | YES |   | YES |   | YES | YES | YES |
|   |   | YES |   | YES |   |     |     |     |
|   |   | YES |   | YES |   |     |     |     |
|   |   |     | 1 |     | 1 |     |     | 1   |
|   |   |     | 1 |     | 1 |     |     | 1   |
|   | 1 |     |   |     | 1 | 1   |     |     |
|   |   |     | 1 |     | 1 |     |     | 1   |
|   |   |     |   |     | 1 |     |     | 1   |
| 1 |   |     |   |     | 1 |     |     | 1   |
|   |   |     | 1 |     |   |     |     |     |
|   | 1 |     |   | 1   |   | 1   |     | 1   |



|     |     |   |     |   |   |   |     |
|-----|-----|---|-----|---|---|---|-----|
| YES | YES |   | YES |   |   |   | YES |
|     | YES |   | YES |   | YES   |   | YES |
|     | YES |   |     |   |   |   | YES |
|     |     | 1 |     |   | 1   |   | 1   |
|     |     | 1 |     |   | 1 PLEASE LOOK INTO ROBLA ELEMENTARY SCHOOL. THE SC            |   | 1   |
|     |     | 1 |     |   | 1 Center mediums. Ways to slow down vehicular t               | 1 |     |
|     |     | 1 |     |   | 1   |   |     |
|     | 1   |   |     | 1 | Post no parking signs on both sides of the stree              | 1 |     |
| 1   |     |   | 1   |   |   |   |     |
|     |     | 1 |     |   | 1 Keep lanes narrow and only one lane in each direction. This |   | 1   |



YES  
YES  
YES

YES  
YES  
YES

1

1

1

1

1  
1

1

1  
1  
1  
1

1

1

1

| Comments   |
|--|
| CROSSWALKS   |
| NEED MORE PUBLIC HELP AROUND AREA FOR KIDS AND ELDERLY, MAYBE SECURITY   |
| NEED MORE ORDER ON THE ROAD  |
| ROAD REPAIR  |
| RRFB   |
| GOOD   |
| PREGNANCY A LITTLE BIT HARDER TO GET AROUND ON PUBLIC TRANSPORTATION PREGNANT WITH KIDS  |
| CROSSWALK HELP   |
| MORE HELP PLEASE   |
| ANOTHER STOP LIGHT   |
| ADDITIONAL STOP LIGHT, RED LIGHT CAM ON LIGHT ON NORWOOD +GRAND  |
| GRAND/RIO LINDA, STREET TRANSPORTATION IS STILL AROUND?  |
| ACCIDENTS ON NORWOOD, INCLUDING ME REAR ENDED  |
| *SPANISH   |
| WIDER BIKE LANES   |
| SHOULD BE ABLE TO HAVE MORE DESTINATION TO GO TO THEN HAVE TO WALK OR TAKE TRAIN   |
| ACROSS FROM PARK, 15MPH COVERED BY TREE. PEOPLE ARE SPEEDING. MORE TRANSPORTATION SERVICE AND PEOPLE NEED TO LEARN HOW TO LET THE PEDESTRIANS WALK ALL THE WAY ACROSS BECAUSE I ALMOST GOT HIT   |
| PLEASE LOOK INTO ROBLA ELEMENTARY SCHOOL. THE SCHOOL NEED SIDEWALK FOR THE KIDS AND FAMILIES. WE SPOKE WITH THE DISTRICT AND THEY THERE NO ARE FUNDS! PLEASE CONSIDER FOR THE SAFETY OF THE  |
| Center mediums. Ways to slow down vehiclar traffic. Vehicles routinely speed over 40 mph. Add a traffic signal light   |
| Post no parking signs on both sides of the street by the Viva Market.  |
| Keep lanes narrow and only one lane in each direction. This will keep the speed down. There's not actually that much traffic, so one lane is enough.   |
| Use roundabouts. Use them at each intersection and the major shopping entrances. Don't use traffic lights. The cars back up waiting for the lights to change when there's no oncoming traffic. Roundabouts prevent this.                                 |
| Separate pedestrian traffic with a parallel protected bike path. Don't put side walks on either side of the road, use protected bike/pedestrian paths. Reducing to one lane will free up plenty of space for this. Plant trees in the protection buffer. |



The Norwood  
**Mobility Project**

# **B - Alternatives Development Report, July 2025**



# Norwood Avenue Mobility Project – Alternatives Development Report

July 2025

Prepared For:

*City of*  
**SACRAMENTO**

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## Glossary of Terms

**95<sup>th</sup> Percentile Queue:** A queue is a line of vehicles waiting to be served, such as at a traffic signal, that occurs due to demand exceeding the available capacity. The 95<sup>th</sup> percentile queue is the length of the queue which is exceeded five percent of the time during the analysis time period. The 95<sup>th</sup> percentile queue is useful in determining the appropriate storage requirements such as length of turn pockets but is not representative of what an average driver would typically experience during their commute.

**Accessible Pedestrian Signal Systems (APS):** A device that uses audible tones or vibrations to help people with vision or hearing impairments safely cross the street at signalized intersections.

**Average Annual Daily Traffic (AADT):** The average number of vehicles that travel on a street per day over the course of a year.

**Bicycle Detection:** Passive traffic signal system that detects the presence of a person bicycling to trigger a green light without requiring the person bicycling to press a button.

**Bicycle Level of Traffic Stress (BLTS):** A numeric suitability rating (1 = low stress, 4 = high stress) that assesses how safe and comfortable a bike route feels to a person bicycling, accounting for factors like lane separation, width, and traffic speed.

**Bike Box:** A painted area at a traffic signal that gives people on bicycles a designated and visible space to wait in front of cars during a red light.

**Bus Bulb-Out:** A sidewalk extension at bus stops allowing buses to load/unload passengers without leaving the travel lane, improving accessibility and reducing dwell time.

**Cantilevered Bike Lane:** A bike lane built onto the side of a bridge, extending out from the structure to create more space for people biking without removing vehicle lanes.

**Channelized Right Turn:** A dedicated turning lane at an intersection that separates right-turning traffic from through lanes and allows turning traffic to either bypass or experience different traffic control than the adjacent through traffic. Channelized turn lanes often pose challenges for pedestrians due to higher vehicle speeds.

**Class I Shared Use Path :** A fully separated shared use path shared by people walking and biking. A Class I shared use path is defined separately from a Class IV bikeway by its width and the requirement that it have wider horizontal separation from vehicle traffic.

**Class II Bikeway – Bike Lane and Buffered Bike Lane:** A bike lane at street level separated by a painted line (Bike Lane) or a painted or physical buffer space between it and adjacent vehicle travel lanes (Buffered Bike Lane), increasing cyclist comfort and safety.

**Class IV Bikeway – Separated Bikeway:** A fully separated facility for bicycles, often at sidewalk level and protected by landscaping or physical barriers from vehicle travel lanes.

**Conflict Zone:** Area where multiple travel modes cross each other and are in conflict. A few examples are where driveways cross sidewalks or bikeways, where bikeways cross with transit vehicles at bus stops, or at intersections where those walking, rolling, or biking cross with vehicle paths.

**Controlled Pedestrian Crossings:** A designated area for people bicycling, walking, or rolling to cross a street where traffic is controlled (where a traffic signal, stop sign, or yield sign directs driver movement) to allow people a safer opportunity to cross.

**Dilemma Zone Detection:** A type of traffic signal technology that helps reduce crashes by detecting vehicles approaching an intersection near the end of the signal phase and can adjust timing to reduce the likelihood of a collision if it is likely that a driver would enter the intersection on red.

**High Injury Network:** Streets or intersections where a high number of severe or fatal crashes have occurred, as identified by the City in its Vision Zero Plan.

**Leading Pedestrian Interval (LPI):** A traffic signal timing strategy that gives pedestrians a head start to cross the street before vehicles get a green light.

**Level of Service (LOS):** The LOS is a measure of street performance when compared to user’s expectations. Streets are given a “letter grade” of “A” through “F” where “A” represents little to no experienced delay or travel congestion and “F” represents high delay or travel congestion. The calculation of LOS is based on the methodologies as outlined in the Highway Capacity Manual 7<sup>th</sup> Edition published by the Transportation Research Board. The calculation of LOS varies by the type of facility or intersection being reviewed.

**On-Street Parking:** Parking of vehicles along the sides of public streets, often in designated spaces marked by painted lines, signs, or meters.

**Pedestrian/Walking Level of Traffic Stress (PLTS):** A numeric suitability rating (1 = low stress, 4 = high stress) that indicates how safe and comfortable walking conditions are, considering sidewalk width, speed limits, and buffer zones.

**Queue:** A queue is a line of vehicles waiting to be served, such as at a traffic signal.

**Right-of-Way (ROW):** Space designated for use by the public for travel. This typically includes the street, landscaping, and sidewalks. The right-of-way includes land which may be owned by the City, other public agencies, utility companies, or private citizens and includes land which has an easement for use by the public for the purposes of travel infrastructure.

**Roundabout:** A circular intersection, used as an alternative to stop-sign or signal-controlled intersections, designed to improve traffic flow and reduce crash severity by slowing vehicles and eliminating left-turn conflicts.

**Sacramento Regional Transit District (SacRT):** The Sacramento Regional Transit District operates public transit services and collaborates on transit stop modifications and pedestrian access enhancements.

**SacSim-19 Model:** A travel demand forecasting tool developed by the Sacramento Area Council of Governments (SACOG) used to simulate and predict future traffic patterns, volumes, and vehicle miles traveled under different development scenarios.

**Safety Corridor:** A designation street under California Vehicle Code Section 22358.7 which allows local authorities to designate a reduced speed limit from the one that would typically be applied based on an engineering and traffic survey. Safety corridors are designated based on a history of serious injuries and fatalities on a given street. No more than one-fifth of streets may be designated as safety corridors

**Sidewalk Scale Lighting:** Lower height lighting installed along sidewalks to enhance visibility and safety for people walking, especially at night. It is designed specifically to illuminate the sidewalk rather than the vehicle travel lanes and typically includes shorter poles and may include decorative elements.

**Signal Modifications:** Upgrades to traffic signals to meet modern standards, including pedestrian countdown timers, improved visibility, and transit signal priority features.

**Turn Pocket:** Vehicle storage lane at an intersection which does not extend to the previous intersection. Typically used to accommodate turning vehicles at an intersection.

**Vehicle Miles Traveled (VMT):** A metric representing the total distance driven by all vehicles in a specified area and timeframe, used to evaluate environmental and land use impacts.

**Wayfinding:** Signage and visual cues placed along transportation routes to guide people to key destinations, like parks, community centers, or transit stops.

## Introduction

The purpose of this report is to summarize the initially proposed project alternatives for the Norwood Mobility Project. The following conditions were determined from the existing conditions analysis that the project alternatives are to address:

- There are gaps in the walking infrastructure and most of the existing sidewalks on the corridor are 5' in width without separation between the sidewalk and the vehicle travel lanes. Community input identified enhancements to the walking infrastructure as a top priority.
- Only a small portion of the corridor has dedicated space for people riding bicycles.
- There is a trend of injury collisions involving people walking and biking, particularly near the Robertson Community Center and in the block between Bell Avenue and Jessie Avenue. The collision trends, field observations, and community input show that people are crossing where infrastructure does not exist to support them and that additional infrastructure is needed.
- There is a trend of broadside collisions at the majority of intersections along the corridor. Rear end crashes, driving at unsafe speeds, and signal violations were mostly concentrated between the I-80 Interchange and Harris Avenue where congestion during commute periods can occur. The most common cited causes of collisions were:
  - Auto right-of-way (violations involve a street user failing to yield the legal right-of-way to another vehicle when required under the California Vehicle Code (CVC), generally by failing to yield when entering a roadway, intersection, or when merging.);
  - Unsafe speed (a street user travelling faster than is safe for street or weather conditions), and;
  - Signal and sign violations (a street user not following the direction provided by a sign or traffic signal).
- All intersections operate at Level of Service (LOS) C or better during peak hours, but some locations have turn movement queues which extend beyond the available turn pockets. Related to this, travel times along the corridor are highly variable, primarily driven by operations at the I-80 interchange especially during commute periods. Outside commute periods, travel times along the corridor are consistent and uncongested.
- There is limited right of way (ROW) throughout the corridor for modifications. Generally, the corridor varies between 48 and 78 feet in width with limited to no space to widen the paved street without impacting the use of adjacent properties. There is no room to modify the street on the bridge over I-80 without widening the structure.

From these findings, the following priorities were considered when developing project alternatives:

- Improve walking infrastructure including the addition of striped and signal-protected crossing opportunities, wherever feasible.
- Create low stress facilities that improve safety for people biking, walking, and rolling.
- Improve corridor safety, particularly between Jessie Avenue and Bell Avenue and between Silver Eagle Road and Harris Avenue.
- Create low stress, accessible travel paths for people biking, walking, and rolling to reach transit
- Ensure project implementation does not negatively impact the operations and values of any private properties along Norwood Avenue.

The city currently has an Intelligent Transportation System (ITS) project underway for the Norwood corridor. The project would upgrade traffic signal controllers and communications by replacing existing end-of-life equipment and outdated communication systems with fiber optic cable-based systems, network switches, new cabinets and controllers, and traffic monitoring cameras. The project would also provide significant multi-modal safety benefits with updated vehicle and bicycle detection, adding yellow reflective border signal heads, pedestrian countdown signal heads, and accessible pedestrian signal push buttons.

The remainder of this report describes several alternatives for consideration for the Norwood Mobility Project. All alternatives contained herein are draft concepts and subject to change based on input from the community and project partners.

## Feasibility Analysis Methodology

To determine the feasibility of each proposed alternative, several forms of analysis were conducted. This analysis includes:

- Travel Demand Forecasting
- Right-Of-Way Assessment
- Walking Level of Traffic Stress Analysis
- Bicycle Level of Traffic Stress Analysis
- Traffic Operations Analysis
- Safety Benefit Assessment
- Transit Assessment

The analysis methodology for each of these assessments is described in further detail in the following sections.

## Travel Demand Forecasting

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A modified version of the SACOG SacSim-19 Travel Demand Model was used to develop future year vehicle travel demand along Norwood Avenue. This model is consistent with the modeling used for the City's 2040 General Plan Update with only minor revisions made in the vicinity of the study area to better reflect local streets which are part of the project. The model is generally only sensitive to major changes in street design which affect either vehicle capacity or transit capacity. For this reason, changes in future vehicle demand for Norwood Avenue are only shown when the number of vehicle travel lanes is changed in an alternative.

The travel demand model was used to develop future year AADT and future year vehicle turning movement demand. Model outputs for AADT and vehicle turning movement demand were adjusted using the post processing methodology described in the National Cooperative Highway Research Program Report 765 (NCHRP-765) Analytical Travel Forecasting Approaches for Project-Level Planning and Design.

Estimates for VMT were derived from the travel demand model and made in accordance with the California Environmental Quality Act (CEQA) as updated by California Senate Bill 743 (SB 743) based on the Guidelines published by the Natural Resources Agency. VMT is a systemic metric and is a useful indicator of overall land use and transportation efficiency, where the most efficient system is one that minimizes VMT by encouraging shorter vehicle trip lengths, more walking and biking, or increased carpooling and transit. VMT is not a good indicator of congestion nor is it useful for identifying hot-spot locations or infrastructure deficiencies. Measuring VMT requires estimating or measuring the full length of vehicle trips by purpose, such as commutes, deliveries, or shopping trips that often cross between cities, counties, or states. For this reason, regional travel demand models, "big data," and household travel surveys that are less limited by local agency boundaries are the preferred tools to estimate VMT under SB 743. VMT is reported by travel speed for all vehicles on all streets within the region for each alternative.

## **Right-of-Way Assessment**

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The existing right-of-way was measured on publicly available aerial imagery at multiple points along Norwood Avenue to determine the smallest common cross section, from back of sidewalk to back of sidewalk, along the corridor. From this analysis, it was determined that there is generally 72 feet or more of current right-of-way along Norwood Avenue. The exceptions to this are:

- The bridge structure over I-80 (Where Caltrans requires additional lane width between vehicle travel lanes and sidewalks);
- The southern end of the corridor south of Fairbanks Avenue (55 feet), and;
- The Northern end of the corridor north of Berthoud Street (66 feet).

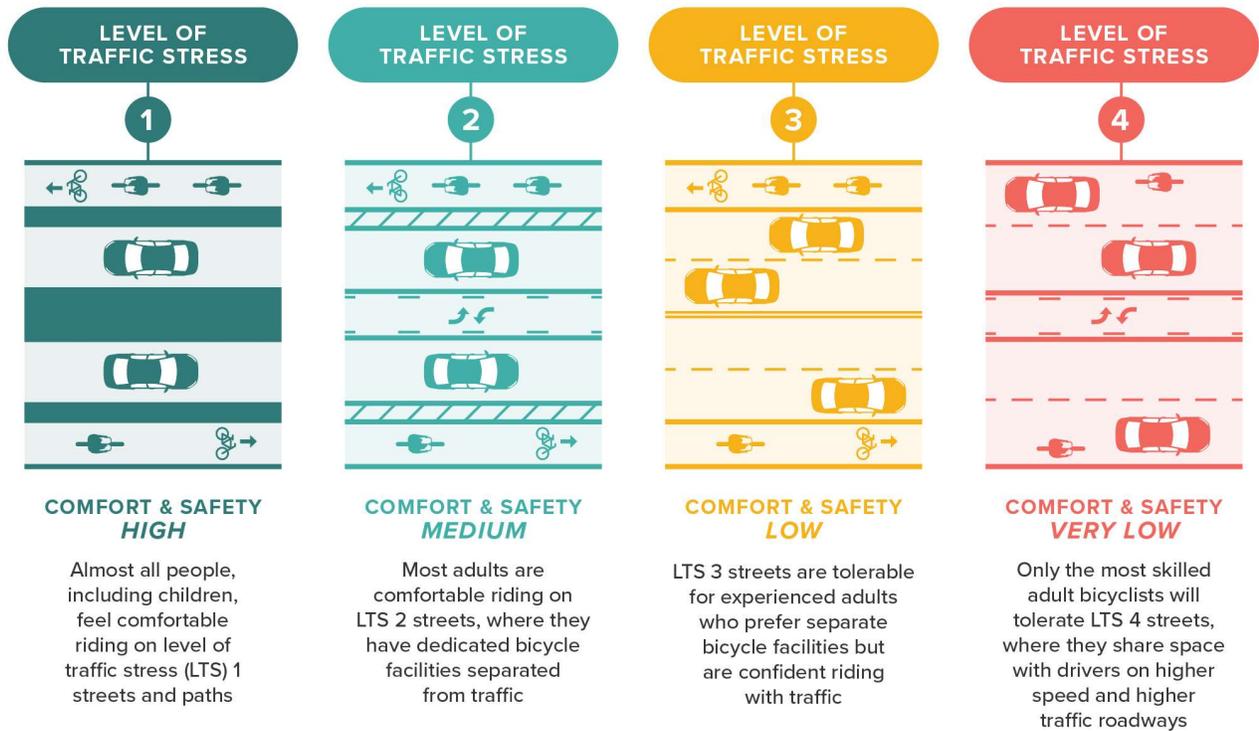
For the bridge over I-80, the plan alternatives specifically avoid making recommendations for changing the allocation of right-of-way as there are limited options available without needing to widen the bridge structure. At the southern end of the corridor, the plan alternatives do not propose any changes, as this section is already two vehicle travel lanes with a Class II bikeway in each direction and seven-foot sidewalks. At the north end of the corridor, the plan alternatives continue with their standard cross sections as there are undeveloped and soon to be developed parcels fronting Norwood Avenue which can implement the plan improvements when they move forward with construction.

## Level of Traffic Stress Analysis

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### Bicycling LTS

The bicycling LTS analysis was calculated using the methodologies describe in the Mineta Transportation Institute Report 11-19 Low Stress Bicycling and Network Connectivity (2012). Bicycling LTS scores quantify the stress level of a street segment through a variety of criteria such as street width (number of lanes), speed limit and/or prevailing speed, presence and width of bike lanes, signals, and presence and width of parking lanes. Bicycle LTS is given a score of 1 through 4, with 1 being the most comfortable and 4 being the least comfortable for people bicycling. Typically, a LTS score of 1 indicates that the stress level of a street is suitable for most people bicycling regardless of skill such as children, while an LTS of 4 indicates that the stress level is better suited for more skilled bicyclists, as shown in **Figure 1**.



**Figure 1. Bicycle Level of Traffic Stress Scores**

### Walking LTS

The walking level of traffic stress (LTS) analysis was done using the Oregon Department of Transportation (ODOT) Level of Traffic Stress Analysis Procedures (2020). Similar to bicycling LTS methodology, walking LTS also undergoes several criteria to develop a LTS score of 1 through 4 including the presence of sidewalks, crosswalks, median refuges, traffic volume, and current speed limits as shown in **Figure 2**.



**Figure 2. Walking Level of Traffic Stress**

## Traffic Operations Analysis

The study intersections were analyzed using the Synchro 12 software package for signalized intersections and Sidra 9.1 software package for roundabouts. Each study intersection was evaluated for operational performance during typical weekday AM and PM peak hour operations. Key performance metrics include average vehicle delay, intersection LOS<sup>1</sup>, and 95<sup>th</sup> percentile queue.

The delay and LOS analysis is based on the latest version of the Transportation Research Board Highway Capacity Manual (HCM) methodology. This methodology assigns an LOS grade to intersection operations based on the average vehicle control delay, ranging from LOS A (free flow) to LOS F (most congested conditions). **Table 1** documents the LOS criteria for signalized intersections and roundabouts. The latest version of the Synchro analysis software was used to report the 95th percentile queue lengths for approach lanes to signalized study intersections. Sidra 9.1 was used to perform this same analysis for study roundabouts.

<sup>1</sup> A Level of Service (LOS) analysis refers to the quantifiable assessment of traffic under various scenarios.

**Table 1: Level of Service Criteria Definitions**

| <b>Level of Service</b> | <b>Description</b>  | <b>Signalized Intersection (Delay in Seconds)</b> |
|-------------------------|---|---|
| <b>A</b>                | Operations with very low delay occurring with favorable progression and/or short cycle lengths.   | ≤10.0   |
| <b>B</b>                | Operations with very low delay occurring with good progression and/or short cycle lengths.  | >10.0 to 20.0                                     |
| <b>C</b>                | Operations with very average delays resulting from fair progression and/or longer cycle lengths. Individual cycle failures begin to appear.   | >20.0 to 35.0                                     |
| <b>D</b>                | Operations with longer delays due to a combination of unfavorable progression, long cycle lengths, and high volume-to-capacity (V/C) ratios. Many vehicles stop and individual cycle failures are noticeable. | >35.0 to 55.0                                     |
| <b>E</b>                | Operations with high delay values indicating poor progression, long cycle lengths, and V/C ratios. Individual cycle failures are frequent occurrences.  | >55.0 to 80.0                                     |
| <b>F</b>                | Operations with delays unacceptable to most drivers occurring due to over-saturation, poor progression, or very long cycle lengths.   | >80.0   |

Source: Highway Capacity Manual, 7<sup>th</sup> Edition

## **Safety Assessment**

Each alternative was qualitatively reviewed for improvements which directly affect collision trends which were identified in the Existing Conditions Report. This includes looking at elements which reduce travel speeds, reduce potential conflicts between vehicles or between vehicles and those walking, biking, or rolling, or better alert people to these potential conflicts. As this project is still in the planning phase, there is not sufficient design data at this time in the project alternatives to quantify collision reductions associated with the proposed improvements.

## **Transit Assessment**

Each alternative was qualitatively reviewed for its compatibility with future transit enhancements. Sacramento Regional Transit (SacRT) owns, operates, and maintains

transit facilities and services along Norwood Avenue and has identified planned and desired improvements to stops along the corridor in their 2023 Bus Stop Improvement Plan. The Norwood Mobility Project is supportive of these proposed improvements and the transit assessment of each alternative will identify if the project option meets or exceeds the planned improvements from SacRT

## Community Priority Alignment

Based on community feedback from the Community Advisory Committee, during the in-person and virtual community workshops, and from the project website, the following community priorities for the project were identified:

- Improve corridor safety, particularly between Jessie Avenue and Bell Avenue, and between Silver Eagle Road and Harris Avenue
- Improve walking infrastructure, including the addition of signal-protected crossing opportunities, wherever feasible
- Create low-stress facilities that improve safety and comfort for people walking, rolling, and bicycling to reach transit
- Create low-stress facilities that improve safety and comfort for people biking

Each alternative will be qualitatively evaluated for alignment with these priorities.

## Alternatives Evaluation

### Common Elements for All Alternatives

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This section lists the common elements that are proposed for all alternatives. The project elements in this section are compatible with all of the major project alternatives and have major safety and functionality benefits without affecting the corridor's vehicle operating capacity.

### **Remove On-Street Parking between Jessie Avenue and Bell Avenue**

Norwood Avenue is one of the few arterial streets in Sacramento, outside of the Central City, that has on-street parking. This condition does not align with current City standards. Over the past five years, collision trends have shown more collisions in this segment with on-street parking compared to the rest of the corridor. Many of these collisions involve people walking or biking. From site observations, people frequently cross the street in this section outside of designated crossing locations, after parking their vehicle. The parked vehicles create sight distance issues for drivers to see these people crossing, particularly in this section where the driver is not alerted to be searching for people crossing the

street. Similarly, there are no bike lanes in this section and bicyclists frequently have to avoid the door zone of parked vehicles by shifting into the path of vehicles traveling at 35 miles per hour.

### **Install Sidewalks**

There are two locations that lack sidewalks along Norwood Avenue. One is on the west side of the street from approximately Berthoud Street to Grace Avenue. In this section, there is an informal asphalt path which is overgrown in places and shows cracking and degradation. The second gap is on the east side of the street from Grace Avenue to Main Avenue. The northern portion of this gap will be constructed by planned housing development in the near future. The Norwood Mobility Project ensures that the corridor has sidewalks along the entire corridor.

### **Signalize Channelized Right Turns at the I-80 Interchange**

Interchanges generally pose a challenge to people walking or biking to cross. At the I-80/Norwood Avenue Interchange there is no dedicated space for people or bicycling and people walking are required to cross channelized uncontrolled right-turn movements at both intersections where people driving enter and exit the freeway. Three out of four of these crossings are currently unmarked (no crosswalk) which creates a higher stress environment for those walking to cross the vehicle lane. Additionally, the lack of marked crosswalks reduces visibility and awareness of someone walking to cross their path. Current Caltrans and City standards support signalizing. Converting the sweeping right turn to an appropriately designed slip lane, with a straight approach, with a pedestrian and bike crossing perpendicular to the lane, placed before the vehicles turning movement, increases driver focus and attention on persons crossing the lane, which can reduce conflicts. It also improves the ability to signalize the approach.

### **Signalize Midblock Pedestrian Crossings**

From both anecdotal evidence during the community workshops and observation during the project site walk, people who walk along Norwood Avenue are looking for additional protected crossing opportunities. People regularly cross Norwood Avenue at unmarked locations which has contributed to a concentration of collisions between Jessie Avenue and Bell Avenue and between Silver Eagle Road and Morey Avenue. There is approximately 1,200 feet and 1,600 feet between signalized crossing opportunities in these two cases respectively. Based on observations and collision data, it is recommended that a signalized crossing be added near the north end of the Robertson Community Center, and another be added near the north end of the Norwood Center shopping plaza. SacRT also identified the need for a pedestrian crossing at Kesner Avenue in their 2023 Bus Stop Improvement Plan to enhance access to transit.

## **Shorten Pedestrian Crossing Distances**

For all alternatives, it is recommended that the project try to achieve the shortest crossing distance feasible to reduce pedestrian exposure to traffic. Reducing lane widths and adding intersection curb extensions are a few ways this may be achieved. Curb extension additionally helps the person walking be more visible and helps drivers determine that the person walking is committed to that crossing, improving the driver's recognition of the person intending to cross.

## **Modify Signal Operations**

For all alternatives, it is recommended that the traffic signals be brought up to current City standards. This process has already started with upgrades at Bell Avenue and Silver Eagle Road. Upgrades at a minimum should include retro-reflective back plates for signal heads, advanced dilemma zone detection, accessible pedestrian signal upgrades, leading pedestrian interval signal timing per city policies and guidelines, curb ramp upgrades to current standards, and crosswalk restriping for high visibility. Consideration should also be given to implementing transit signal priority, especially for alternatives which reallocate ROW away from vehicle travel lanes.

## **Implement Bus Stop Infrastructure and Stop Amenities**

SacRT completed their Bus Stop Improvement Plan in February 2023 which identified several stops along Norwood Avenue for enhancements, including:

- SB Norwood Avenue north of Jessie Street – construct a new concrete pad behind the sidewalk and add a transit shelter and bench
- NB Norwood Avenue north of Jessie Street – construct a new concrete pad behind the sidewalk
- NB Norwood Avenue north of Morrison Avenue – construct a new concrete pad behind the sidewalk with a retaining wall
- NB Norwood Avenue south of Lindsay Avenue – construct a new concrete pad behind the sidewalk and add a transit shelter and bench
- SB Norwood Avenue south of Grand Avenue – construct a new concrete pad behind the sidewalk and add a transit shelter and bench
- NB Norwood Avenue north of Kesner Avenue – construct a new concrete pad behind the sidewalk with a retaining wall
- NB Norwood Avenue north of Hayes Avenue – construct a new concrete pad behind the sidewalk with retaining curbs and add a transit shelter and bench
- SB Norwood Avenue north of Silver Eagle Road (Robertson Community Center) – construct a new concrete pad behind the sidewalk with retaining curbs and add a transit shelter and bench

- SB Norwood Avenue north of Carroll Avenue – construct a new concrete pad behind the sidewalk with a retaining wall
- NB Norwood Avenue north of Carroll Avenue – construct a new concrete pad behind the sidewalk with a retaining wall

The Norwood Mobility Project is an opportunity for the City to support these SacRT efforts.

### **Reduce Posted Speed Limits**

Assembly Bills 43 and 1938 updated the California Vehicle Code to allow for a five mile per hour reduction of posted speed limits below what would be recommended based on 85<sup>th</sup> percentile observed speeds on streets that are designated as Safety Corridors or on streets adjacent to land uses that generate a high number of people walking or biking. Only one speed limit reduction is allowed to be applied on each street. Norwood Avenue is eligible to be designated as a Safety Corridor. Norwood Avenue is also eligible to be designated as a high activity walking or biking corridor based on local land use patterns if it is not designated as a Safety Corridor. Streets in front of and up to ¼ mile from schools, public parks, houses of worship, community centers, and other facilities which encourage walking or biking may be designated as high walking and biking activity areas. Enough of these uses exist along Norwood Avenue that virtually all of the study area is within ¼ mile of one of these land uses.

### **Provide Additional Storage Lanes for the I-80 Westbound On-Ramp**

The City should coordinate with Caltrans to add a second queue storage lane to the I-80 Westbound On-Ramp before the ramp meter. Currently it is the only ramp of four at this interchange which does not have two lanes of travel. The current design provides approximately 550 feet of storage between the ramp meter and Norwood Avenue. Based on vehicle speed and travel time data collected for Norwood Avenue, travel times on the corridor are highly variable and appear to be tied in part to queues at this on-ramp during peak hours. The additional lane could be designed as a high occupancy vehicle preference lane or a standard storage lane and would require additional operational study beyond this plan to determine the specifics of its design. This is not a currently planned Caltrans project and is outside of the City’s jurisdiction. This modification would require coordination between the City and Caltrans.

### **Add Wayfinding for People Walking and Biking**

Installation of wayfinding signs placed at key locations along the corridor such as bus stops and high-volume areas will direct people to popular destinations, such as the community center, shopping opportunities, and the Sacramento Northern Parkway shared use path.

## Alternative 1

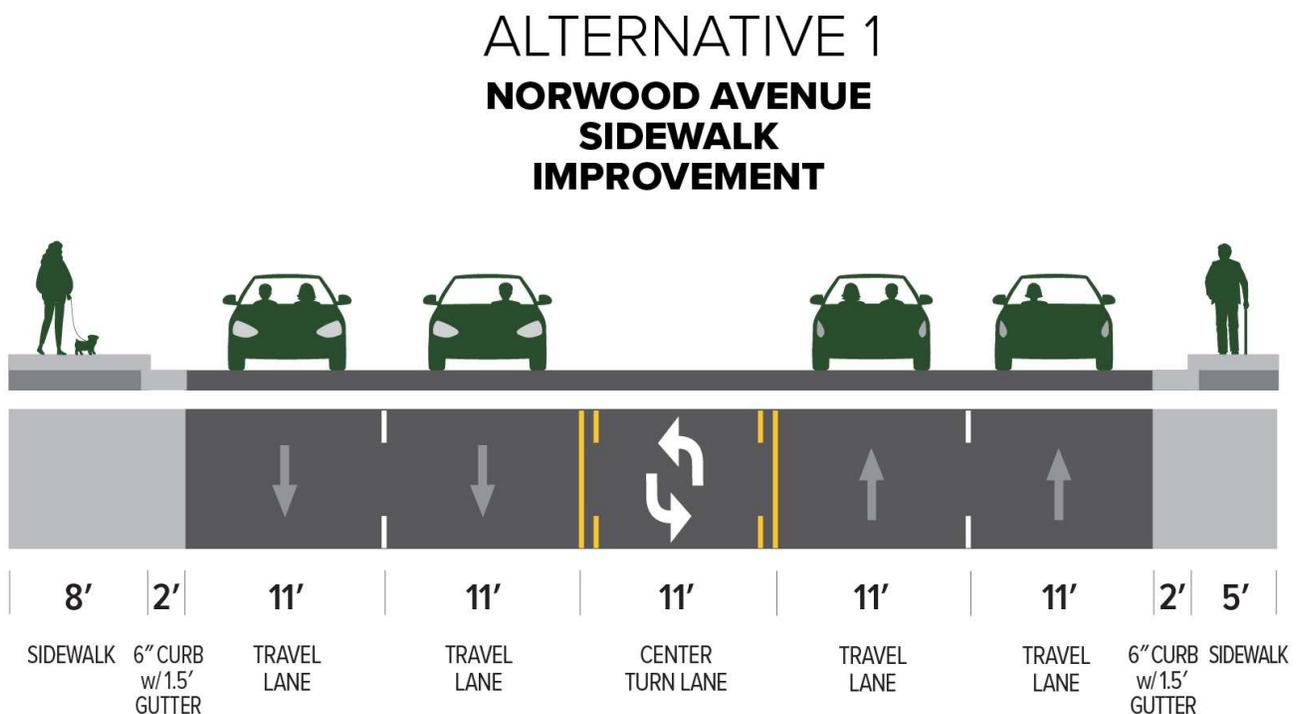
### Description

The majority of items included in Alternative 1 are consistent across all alternatives and presented in the previous section. This alternative is the only one that does not propose a right-of-way reallocation on Norwood Avenue. Elements unique to this alternative include:

#### Widen Sidewalks

Norwood Avenue is generally not wide enough to include standard bikeways without reducing the number of vehicle travel lanes. City Ordinance 10.76.010<sup>2</sup> allows people to bicycle on sidewalk under certain requirements. In lieu of providing on-street bicycle infrastructure, this alternative widens the sidewalk on the west side of the street to allow people bicycling, walking, and rolling to navigate potential conflicts between users.

**Figure 3** shows the general cross section proposed for this alternative. **Figure 4** shows a representative map view of Norwood Avenue and where improvements would be applied.



**Figure 3: Alternative 1 Cross-Section**

<sup>2</sup> [City of Sacramento Ordinance 10.76.010](#)

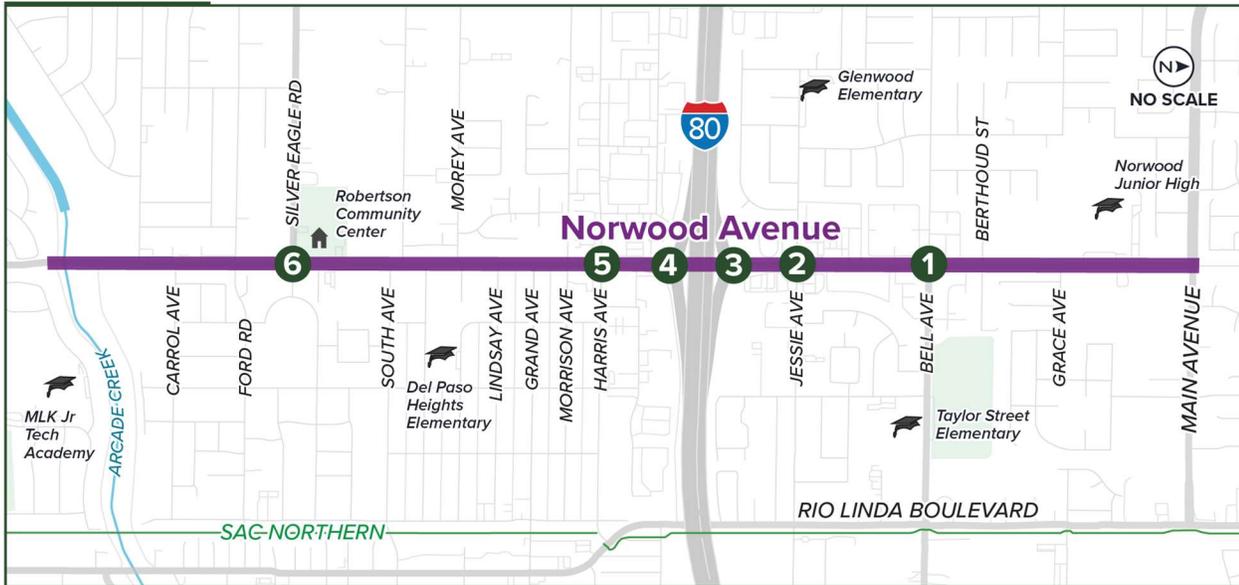


**Figure 4: Alternative 1 Plan View of Proposed Improvements**

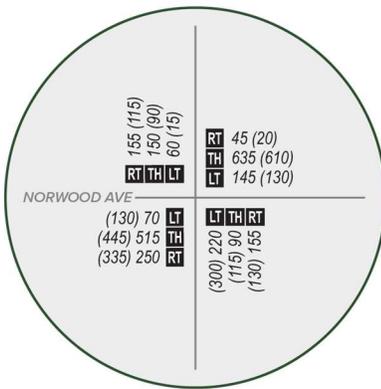
## Feasibility Analysis

### Travel Demand Forecasting

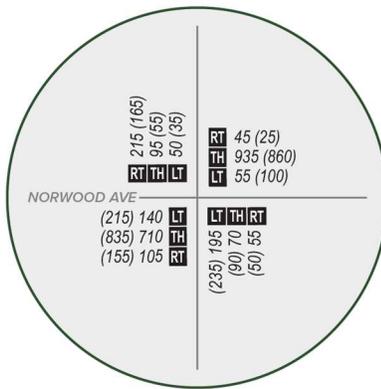
Based on the SacSim-19 travel demand model as modified for the City of Sacramento 2040 General Plan Update, future volumes on Norwood Avenue range between 19,000 and 41,000 AADT for Alternative 1. The highest volumes are on the segment between Jessie Avenue and Harris Avenue. These volumes drop to the 26,000-30,000 AADT range between Jessie Avenue and Bell Avenue and between Harris Avenue and Grand Avenue. North of Bell Avenue and south of Grand Avenue, volumes drop to the 19,000-22,000 AADT range. The Travel demand model was also used to forecast future turning movement demand volumes at study intersection along the corridor. These volumes are shown in **Figure 5**. Because Alternative 1 does not change the vehicle capacity of Norwood Avenue, no net change in future VMT is expected.



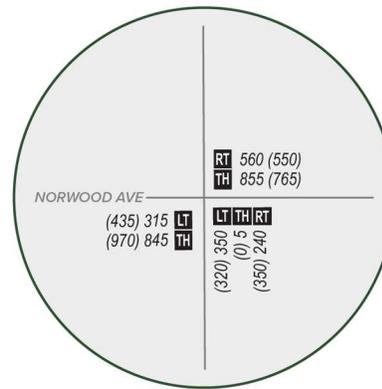
**1** BELL AVE / NORWOOD AVE



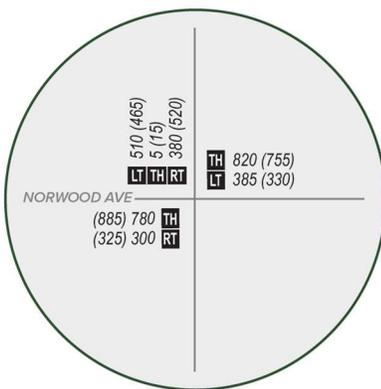
**2** JESSIE AVE / NORWOOD AVE



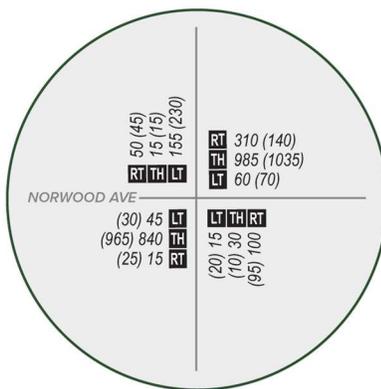
**3** I-80 WB RAMPS / NORWOOD AVE



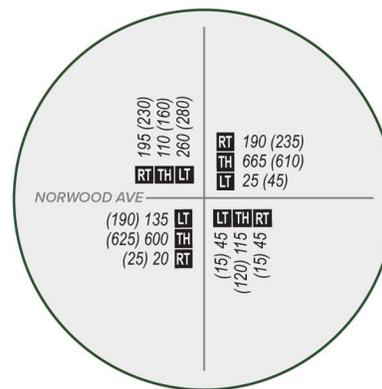
**4** I-80 EB RAMPS / NORWOOD AVE



**5** HARRIS AVE / NORWOOD AVE



**6** SILVER EAGLE RD / NORWOOD AVE



- Plan Corridor
- School
- Community Center
- Study Intersection
- Traffic Volume Movements  
Left • Thru • Right

**Figure 5: Future (2045) Turning Movement Volumes Alternative 1**

## Level of Traffic Stress Analysis

The focus of Alternative 1 is to provide some improvements for those walking, biking, and rolling without significantly altering the vehicle capacity of Norwood Avenue. This alternative adds new crossing opportunities and widens the sidewalk on the west side of Norwood Avenue, but the improvements made do not significantly alter the walking and biking environment. **Table 2** and **Table 3** show the evaluation of the walking and biking level of traffic stress. **Figure 6** and **Figure 7** show the results of this evaluation in a map form.

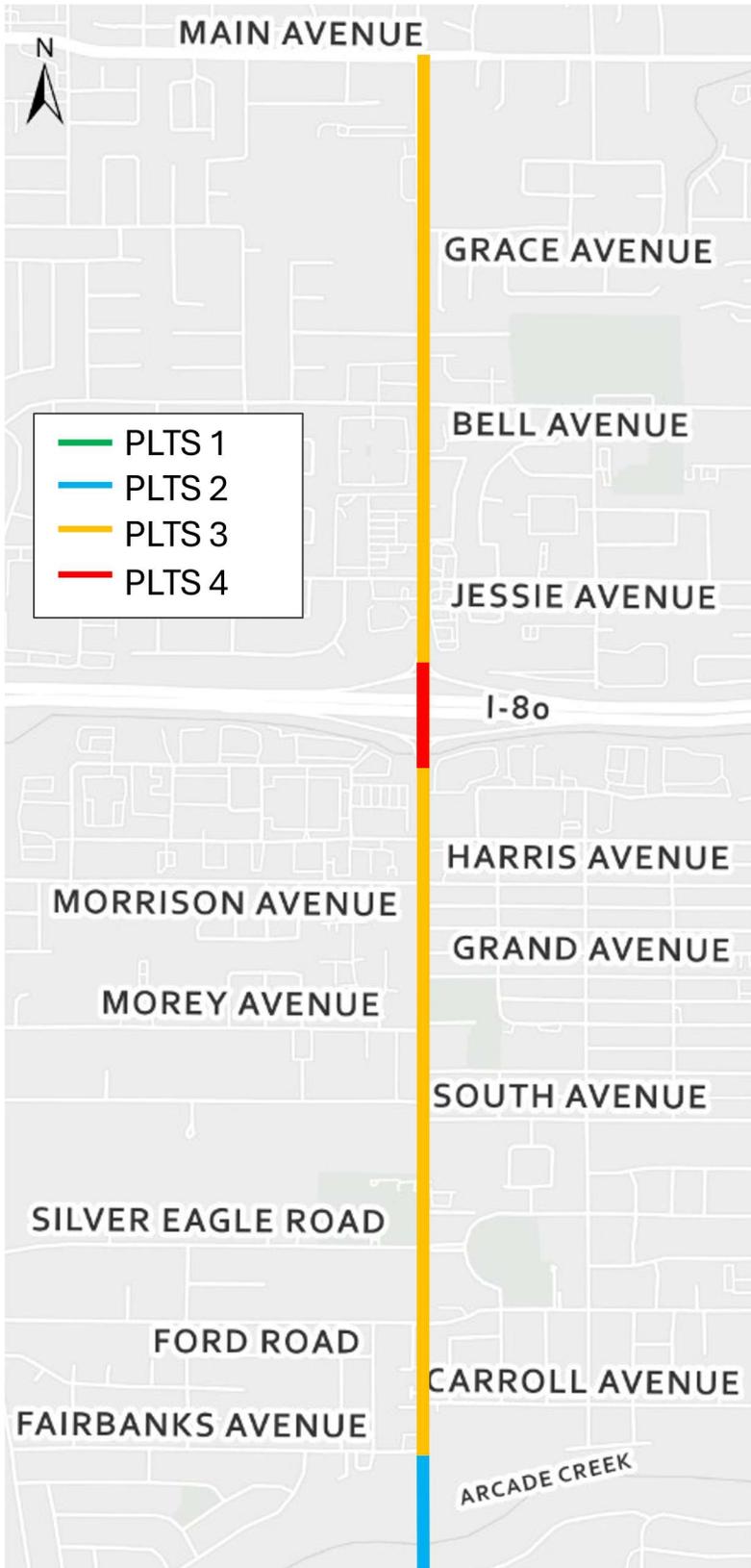
**Table 2: Analysis of Pedestrian Level of Traffic Stress –Alternative 1**

|  | Main Avenue to Bell Avenue | Bell Avenue to I-80 WB Ramps | I-80 EB Ramps to Fairbanks Avenue | Fairbank Avenue to Arcade Creek |
|--|----------------------------|------------------------------|-----------------------------------|---------------------------------|
| <b>Street Width (Through Lanes per Direction)</b>        | 2                          | 2                            | 2                                 | 1                               |
| <b>Buffer Type</b>                                       | None                       | None                         | None                              | None                            |
| <b>Total Buffer Width (Ft)</b>                           | 0                          | 0                            | 0                                 | 0                               |
| <b>Sidewalk Width (Ft)</b>                               | 5ft                        | 5ft                          | 5ft                               | 5ft                             |
| <b>Speed Limit Or Prevailing Speed<sup>A</sup> (MPH)</b> | 30                         | 30                           | 30                                | 25                              |
| <b>Existing PLTS Score<sup>B</sup></b>                   | 4                          | 4                            | 4                                 | 3                               |
| <b>Alternative 1 PLTS Score</b>                          | 3                          | 3                            | 3                                 | 2                               |

Source: DKS Associates, 2025. ODOT Level of Traffic Stress Analysis Procedures.

A Alternative 1 recommends speed limit reductions throughout the corridor. This analysis was conducted under the assumption that existing speed limits have been reduced by 5 mph.

B Existing PLTS has variability in score for each segment as the analysis was done bi-directional. The Existing PLTS Score included in Table 4 is the highest existing score per segment for purposes of this analysis.



**Figure 6: Walking Level of Traffic Stress – Alternative 1**

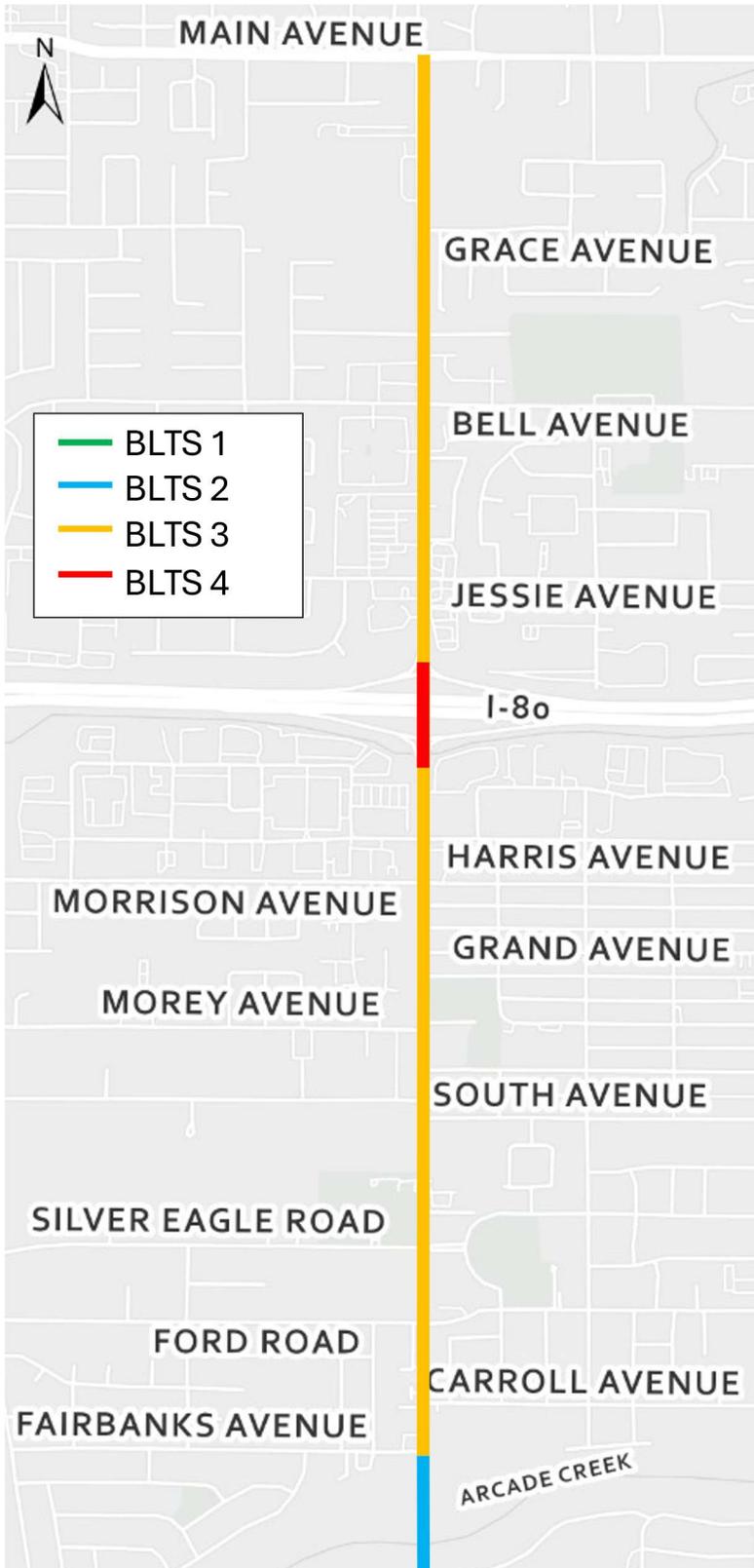
**Table 3. Analysis of Bicycle Level of Traffic Stress – Alternative1**

|  | <b>Main Avenue to Bell Avenue</b> | <b>Bell Avenue to I-80 EB Ramps</b> | <b>I-80 EB Ramps to Fairbanks Avenue</b> | <b>Fairbanks Avenue to Arcade Creek</b> |
|--|-----------------------------------|-------------------------------------|--|---|
| <b>Street Width (Through Lanes per Direction)</b>                  | 2                                 | 2                                   | 2  | 1                                       |
| <b>Bike Lane Width (Inc. Bike Lane, Buffer Width, Gutter) (Ft)</b> | 0                                 | 0                                   | 0  | 5                                       |
| <b>Speed Limit or Prevailing Speed<sup>A</sup> (MPH)</b>           | 30                                | 30                                  | 30                                       | 25                                      |
| <b>Physically Separated Bike Lane?</b>                             | No                                | No                                  | No                                       | No                                      |
| <b>Existing BLTS Score<sup>B</sup></b>                             | 4                                 | 4                                   | 4  | 3                                       |
| <b>Alternative 1 BLTS Score</b>                                    | 3                                 | 3                                   | 3  | 2                                       |

Source: DKS Associates, 2025. Mineta Transportation Institute, Low Stress Bicycling and Network Connectivity.

A Alternative 1 recommends speed limit reductions throughout the corridor. This analysis was conducted under the assumption that existing speed limits have been reduced by 5 mph.

B Existing BLTS has variability in score for Segment 3 and Segment 4 as the analysis was done bi-directional. The Existing BLTS Score included in Table 7 is the highest existing score per segment for the purpose of this analysis.



**Figure 7: Bicycle Level of Traffic Stress – Alternative 1**

## Traffic Operations Analysis

The analysis for Alternative 1 assumed minimal changes from the current operating conditions along the corridor. Signal timing adjustments were made in relation to the proposed improvements and to accommodate higher traffic volumes associated with future growth. All signals were assumed to operate without coordination, but signal coordination would likely improve operations from the results shown. Table 4 shows a comparison of anticipated future intersection delays compared to existing operations.

95<sup>th</sup> percentile queues were also evaluated for Alternative 1. The AM and PM peak hour queues are shown in Figure 8 and Figure 9 respectively. In these figures, lines are shown on each approach to the intersection representing the queue for the left turn lane (if one exists), the through movements, and the right turn lane (if one exists). These queues are generally color coded as green if they are less than the available vehicle storage, yellow if they are at or near the available vehicle storage, and red if they exceed the available vehicle storage or block access to adjacent lanes. Note that 95<sup>th</sup> percentile queues represent the longest queue that is likely to be observed during the peak hour and most queues would be shorter. From this analysis, the key finding is that queues are longest at the intersections which comprise the I-80 interchange. There are other locations where queues exceed their available storage along Norwood Avenue, but in most cases it is due to short formal turn pockets being blocked by through movement queues.

**Table 4: Future (2045) Alternative 1 Intersection Operational Analysis Results**

| Intersection                                     | AM Peak Hour <sup>A</sup> |          | PM Peak Hour <sup>A</sup> |          |
|--|---------------------------|----------|---------------------------|----------|
|  | Existing                  | Future   | Existing                  | Future   |
| <b>1. Norwood Avenue / Bell Avenue</b>           | 20.6 (C)                  | 23.9 (C) | 17.6 (B)                  | 23.7 (C) |
| <b>2. Norwood Avenue / Jessie Avenue</b>         | 28.2 (C)                  | 29.3 (C) | 23.8 (C)                  | 30.7 (C) |
| <b>3. Norwood Avenue / WB 80 Ramps</b>           | 10.9 (B)                  | 13.6 (B) | 10.3 (B)                  | 16.0 (B) |
| <b>4. Norwood Avenue / EB 80 Ramps</b>           | 12.0 (B)                  | 16.3 (B) | 12.0 (B)                  | 16.0 (B) |
| <b>5. Norwood Avenue / Harris Avenue</b>         | 19.7 (B)                  | 25.8 (C) | 19.2 (B)                  | 24.4 (C) |
| <b>Norwood Avenue / Morey Avenue<sup>B</sup></b> | -                         | 22.1 (C) | -                         | 9.7 (A)  |
| <b>6. Norwood Avenue / Silver Eagle Road</b>     | 18.6 (B)                  | 11.4 (B) | 18.2 (B)                  | 23.1 (C) |

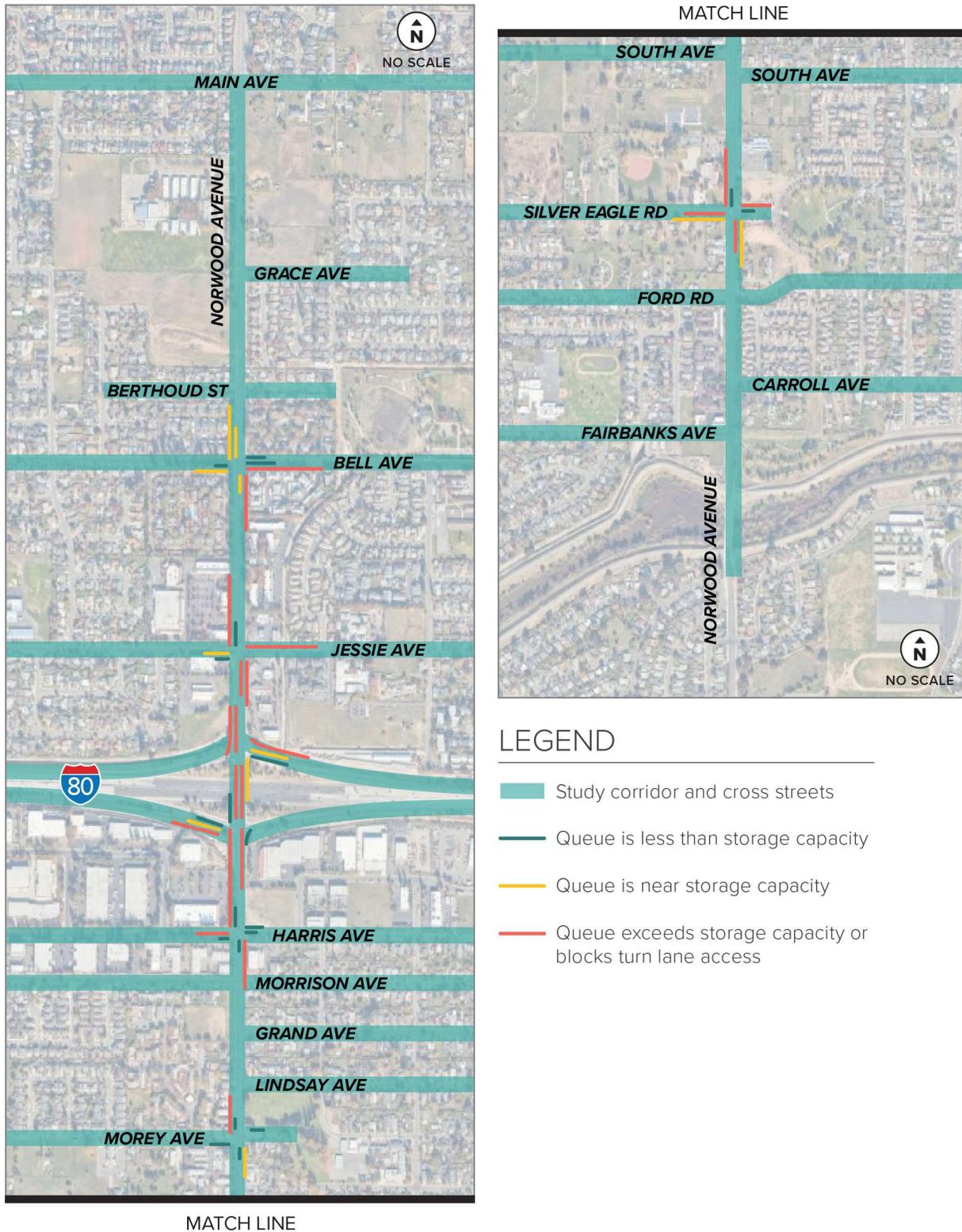
Source: DKS Associates, March 2025.

**Notes:**

- A. 20.6 (C) = Delay (LOS)
- B. Not a study intersection, provided for informational purposes because of recommended control modifications



**Figure 8: Future (2045) AM Peak Hour 95th Percentile Intersection Queues Alternative 1**



**Figure 9: Future (2045) PM Peak Hour 95th Percentile Intersection Queues Alternative 1**

## **Safety Benefit Assessment**

Alternative 1 addresses some of the corridor-wide safety concerns by reducing the speed limit, removing on-street parking between Bell Avenue and Jesse Avenue, adding additional controlled crossing locations, and improving visibility of signals. An additional metered lane on the WB I-80 on-ramp would also help address congestion-based crashes. These safety upgrades come from elements common across all alternatives and are not unique to Alternative 1.

## **Transit Assessment**

Alternative 1 provides only minimal potential benefits for transit operations. This alternative would provide the least amount of improvement by supporting stop enhancements identified by SacRT and closing sidewalk gaps. The wider sidewalk on the west side of the street would provide some additional waiting area for transit stops used by people traveling in the southbound direction.

## **Community Priority Alignment**

Alternative 1 improves corridor safety by removing on-street parking between Jessie Avenue and Bell Avenue and by reducing speed limits along the corridor. It also includes the addition of three new marked and signalized pedestrian crosswalks and signalizes pedestrian crossings at the freeway ramps. Alternative 1, while reducing the level of traffic stress slightly for people walking and biking by reducing traffic speeds, still does not provide any low stress segments or connections to transit.

## Alternative 2

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### Description

Alternative 2 proposes installing a Class IV separated bikeway along Norwood Avenue by reallocating space from one of the vehicle travel lanes in each direction. There are multiple ways in which this alternative can be achieved and thus three sub alternatives (2A, 2B, and 2C) are included under Alternative 2. The primary way these sub alternatives are differentiated is in how they place the separated bikeway within the proposed cross section. The proposed cross sections for Alternatives 2A, 2B, and 2C are shown in **Figure 10**, **Figure 11**, and **Figure 12** respectively. All other elements in the alternative description are shared between the three sub-alternatives. **Figure 4** shows a representative map view of Norwood Avenue and where improvements would be applied for Alternative 2. The elements in this alternative include:

#### **Reallocate Street Space from Driving to Walking and Bicycling: Fairbanks Avenue to Grand Avenue and from Bell Avenue to Grace Avenue**

In order to create space for walking and bicycling enhancements along the lower volume segments of the corridor, the number of vehicle travel lanes would be reduced from two per direction with a center turn lane to one per direction with a center turn lane. Sections south of Fairbanks Avenue and north of Grace Avenue would maintain their current cross-sections. The section between Harris Avenue to Jessie Avenue would be maintained as two lanes per direction to provide capacity for higher car and truck volumes and demands at the I-80 Interchange.

#### **Install Roundabouts at Silver Eagle Road, Morey Avenue, and Bell Avenue**

A single lane roundabout at Silver Eagle Road and at Morey Avenue would slow traffic in the vicinity of the Robertson Community Center and two nearby parks.

A single lane roundabout at Morey Avenue would also provide a direct path for people wanting to cross the street at Morey Avenue, which is currently an offset intersection with a marked crossing in the middle of the intersection.

A single lane roundabout at Bell Avenue would slow southbound vehicles as they approach the higher residential density and commercial portion of the corridor. It would also reduce conflict points at this high crash location.

All three roundabout locations have undergone a preliminary review for right-of-way requirements to install a single lane roundabout, and it was found that a roundabout could be installed at each location without impacting existing structures or causing a loss of use for adjacent developed properties.

#### **Install Separated Bikeway**

Removing an existing vehicle travel lane in each direction would provide sufficient space to add separated bikeways to the corridor. In Alternatives 2A and 2B, the separated bikeway would be kept at the same level as the vehicle travel lanes and separated with a painted buffer and raised elements separating the bikeway from vehicle lanes (precise design to be determined at a later date). In Alternative 2C, the separated bikeway is brought to sidewalk level and would be separated from the vehicle travel lanes by a landscaping strip. An additional one-foot buffer with visually and texturally unique elements placed parallel to the bikeway would be placed between the bikeway and the sidewalk to reduce potential conflicts between people walking and people biking. Due to lack of physical width available on the interchange, people riding bikes seeking to cross I-80 would still need to ride on the sidewalk.

### **Add Bicycle Detection**

The remaining signalized intersections (those not updated to roundabouts) would be updated to include bicycle detection. This would allow the signals to react to people on bicycles and change signal phases without requiring the person riding to dismount and cross the intersection as a pedestrian or wait for a vehicle trigger the signal phase change.

### **Widen Sidewalks and Add Landscape Buffer**

Existing sidewalks along Norwood Avenue would be widened to more than five feet to allow for a more comfortable and low stress walking environment, regardless of existing utility and signal poles. Landscape buffers would be installed between traffic and the sidewalk north of Jessie Avenue and south of Harris Avenue to expand the low-stress walking network while keeping right-of-way acquisition minor and constrained to landscaping. Alternatives 2A, 2B, and 2C allocate this landscaping buffer differently which changes what can ultimately be planted in this space. Alternative 2A would allow for grasses and small bushes to be planted in this space. Alternative 2B eliminates to landscape buffer on the east side of the street to allow for small to medium sized trees to be planted on the west side of the street. Alternative 2C moves the bikeway to sidewalk level eliminating the need for the buffer area between people riding bikes and vehicles and reallocates this space to the planted buffers. This would allow for large trees to be planted on the west side of the street and grasses and small bushes to be planted on the east side of the street.

### **Install Sidewalk Scale Lighting**

Sidewalk scale lighting would ensure the area where people are walking is illuminated, increasing comfort and feelings of security and safety.

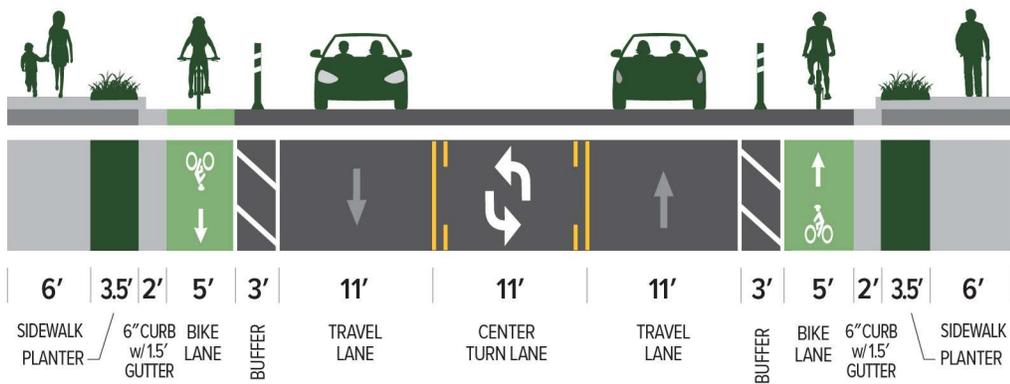
### **Relocate Utilities**

The installation of a landscape buffer and wider sidewalks would allow for an opportunity to relocate utility poles either outside of the walkway or underground to provide appropriate sidewalk widths. This would require collaboration with and support from utility providers.

**Install Bus Bulb-Outs with In-Lane Bus Stops**

The sidewalk would be extended to allow for the bus to load passengers directly from the vehicle travel lane, with the bikeway continuing behind the bus stop. This treatment would also allow some stops to be turned to allow for better protection from the sun. By allowing buses to stop in-lane, transit time reliability is improved by not requiring the bus to seek gaps in traffic to re-enter the travel lane. This is recommended as the default treatment for all bus stops along the corridor, but design specifics would have to be determined in coordination with SacRT, such as those requiring space for a bus to dwell for schedule adherence.

ALTERNATIVE 2a  
**NORWOOD AVENUE  
 BASIC ROAD DIET**



**Figure 10: Alternative 2A Cross-Section**

## ALTERNATIVE 2b NORWOOD AVENUE BASIC ROAD DIET

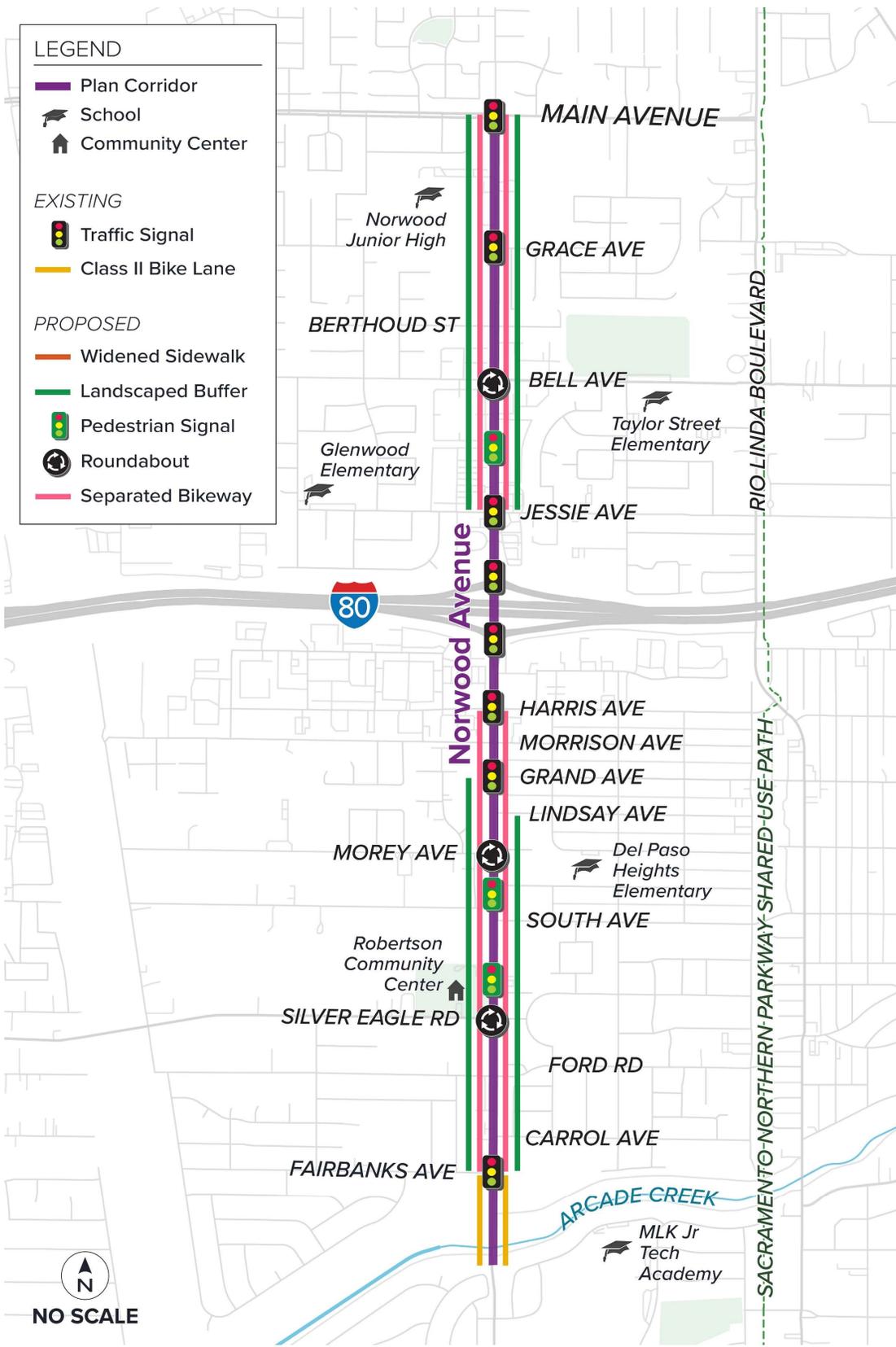


**Figure 11: Alternative 2B Cross-Section**

## ALTERNATIVE 2c NORWOOD AVENUE BASIC ROAD DIET



**Figure 12: Alternative 2C Cross-Section**



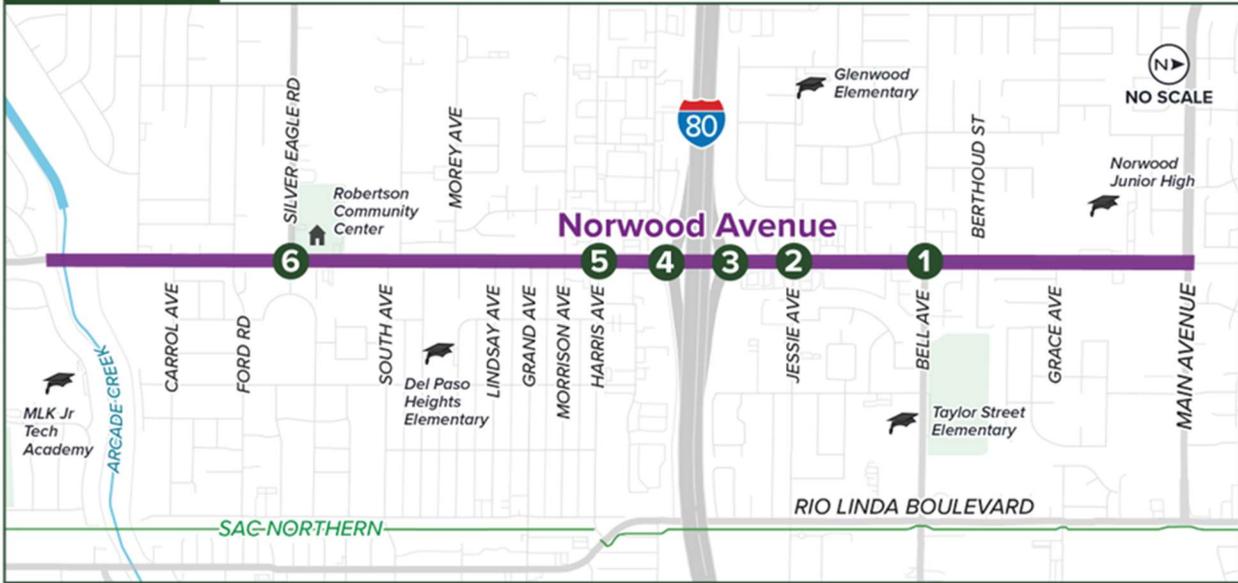
**Figure 13: Alternative 2 Plan View of Proposed Improvements**

## Feasibility Analysis

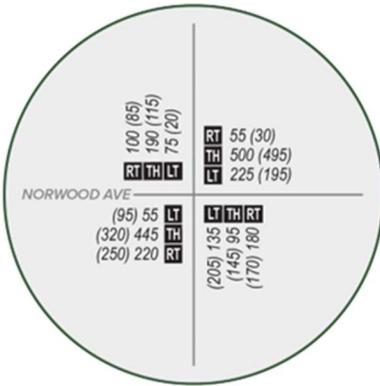
### Travel Demand Forecasting

Based on the SacSim-19 travel demand model as modified for the City of Sacramento 2040 General Plan Update, future volumes on Norwood Avenue range between 17,000 and 37,000 AADT for Alternative 2. The highest volumes are on the segment between Jessie Avenue and Harris Avenue. These volumes drop to the 21,000-25,000 AADT range between Jessie Avenue and Bell Avenue and between Harris Avenue and Grand Avenue. North of Bell Avenue and south of Grand Avenue, volumes drop to the 17,000-20,000 AADT range. These daily volumes are lower than those in Alternative 1 due to the reduction in travel lanes. A portion of the volume which was using Norwood Avenue before the reduction in travel lanes would instead use parallel roads such as Northgate Boulevard and Rio Linda Boulevard. The Travel demand model was also used to forecast future turning movement demand volumes at study intersections along the corridor. These volumes are shown in **Figure 14**.

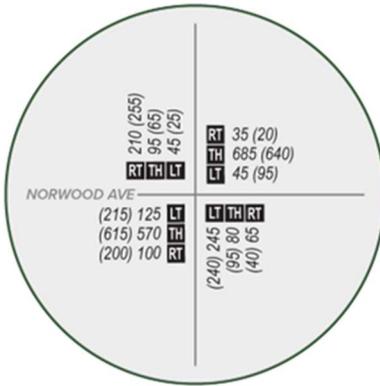
Alternative 2 reduces the total number of vehicle travel lanes on Norwood Avenue which could potentially cause an increase in VMT related to the infrastructure project. Based on the Transportation Analysis under CEQA for Projects on the State Highway System guidelines published by Caltrans, projects which reduce the number of through lanes and projects which add or enhance bikeways and walking facilities would not likely lead to a measurable increase in VMT. All elements which are proposed under Alternative 2 would meet the State's screening criteria guidance for VMT analysis and do not require further evaluation for VMT impacts.



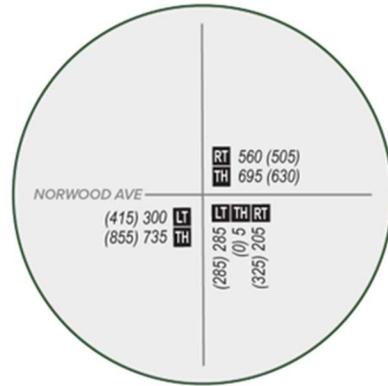
**1** BELL AVE / NORWOOD AVE



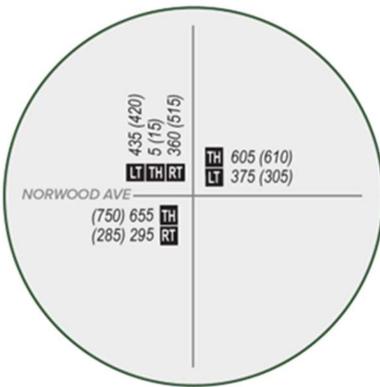
**2** JESSIE AVE / NORWOOD AVE



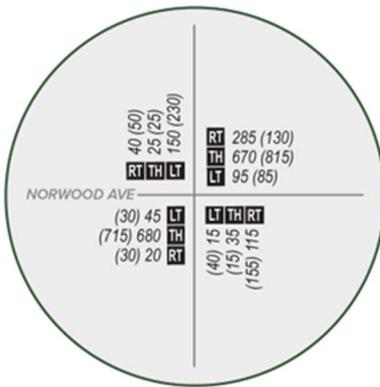
**3** I-80 WB RAMPS / NORWOOD AVE



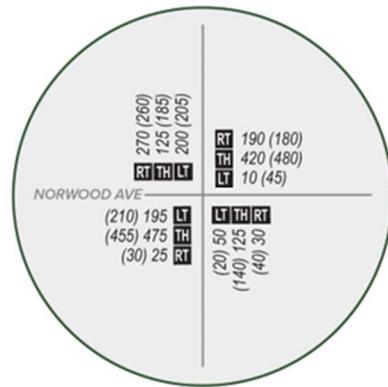
**4** I-80 EB RAMPS / NORWOOD AVE



**5** HARRIS AVE / NORWOOD AVE



**6** SILVER EAGLE RD / NORWOOD AVE



■ Plan Corridor     
 School     
 LT TH RT Traffic Volume Movements  
# Study Intersection     
 Community Center     
 Left • Thru • Right

**Figure 14: Future (2045) Turning Movement Volumes Alternative 2**

## Level of Traffic Stress Analysis

The focus of Alternative 2 is to provide significant improvements for those walking, biking, and rolling by reallocating existing right-of-way away from vehicles and towards walking and biking. This alternative adds new crossing opportunities and widens the sidewalks on Norwood Avenue. Additionally, this alternative provides a separated bikeway to enhance safety and comfort for those biking. **Table 2** and **Table 3** show the evaluation of the walking and biking level of traffic stress. **Figure 6** and **Figure 7** show the results of this evaluation in a map form.

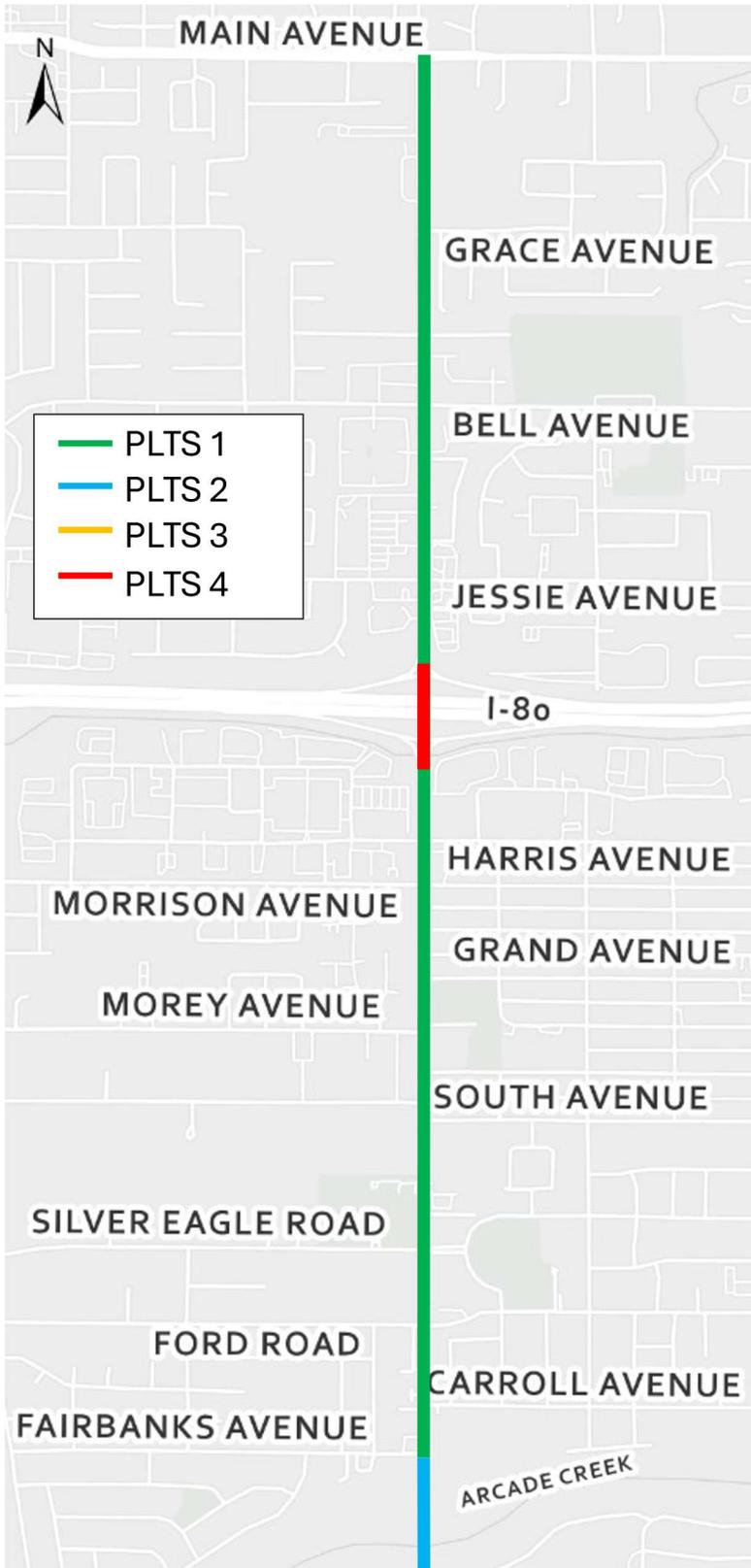
**Table 5: Analysis of Walking Level of Traffic Stress –Alternative 2**

|  | Main Avenue to Bell Avenue | Bell Avenue to I-80 WB Ramps | I-80 EB Ramps to Fairbanks Avenue | Fairbank Avenue to Arcade Creek |
|--|----------------------------|------------------------------|-----------------------------------|---------------------------------|
| <b>Street Width (Through Lanes per Direction)</b>        | 1                          | 1                            | 1                                 | 1                               |
| <b>Buffer Type</b>                                       | Landscaped Buffer          | Landscaped Buffer            | Landscaped Buffer                 | None                            |
| <b>Total Buffer Width (Ft)</b>                           | 13.5ft                     | 13.5ft                       | 13.5ft                            | 0                               |
| <b>Sidewalk Width (Ft)</b>                               | 6                          | 6                            | 6                                 | 6                               |
| <b>Speed Limit or Prevailing Speed<sup>A</sup> (MPH)</b> | 30                         | 30                           | 30                                | 25                              |
| <b>Existing PLTS Score<sup>B</sup></b>                   | 4                          | 4                            | 4                                 | 3                               |
| <b>Alternative 2 PLTS Score</b>                          | 1                          | 1                            | 1                                 | 2                               |

Source: DKS Associates, 2025. ODOT Level of Traffic Stress Analysis Procedures.

A Alternative 1 recommends speed limit reductions throughout the corridor. This analysis was conducted under the assumption that existing speed limits have been reduced by 5 mph.

B Existing PLTS has variability in score for each segment as the analysis was done bi-directional. The Existing PLTS Score included in Table 4 is the highest existing score per segment for the purpose of this analysis.



**Figure 15: Walking Level of Traffic Stress – Alternative 2**

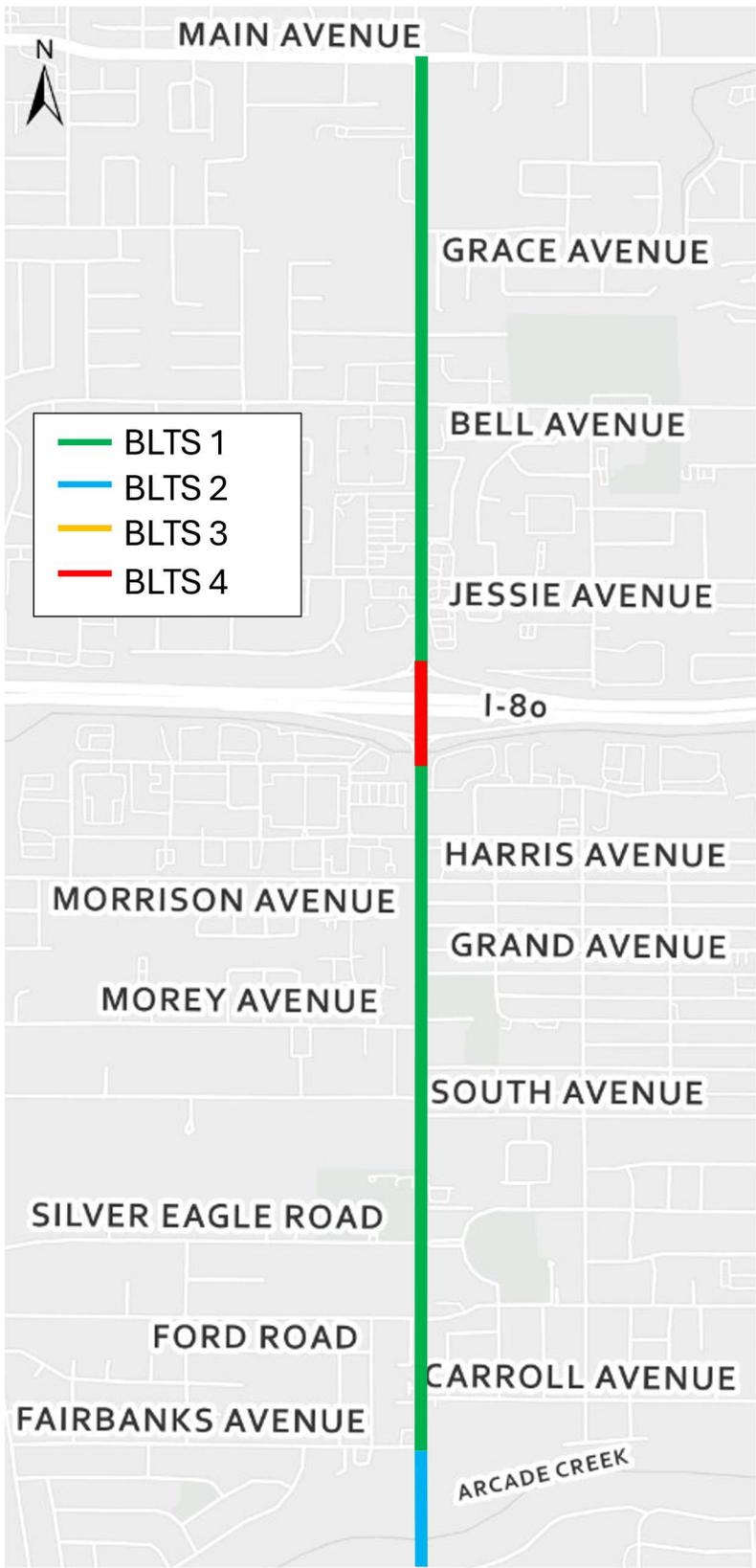
**Table 6. Analysis of Bicycle Level of Traffic Stress – Alternative 2**

|  | <b>Main Avenue to Bell Avenue</b> | <b>Bell Avenue to I-80 EB Ramps</b> | <b>I-80 EB Ramps to Fairbanks Avenue</b> | <b>Fairbanks Avenue to Arcade Creek</b> |
|--|-----------------------------------|-------------------------------------|--|---|
| <b>Street Width (Through Lanes per Direction)</b>                  | 1                                 | 1                                   | 1  | 1                                       |
| <b>Bike Lane Width (Inc. Bike Lane, Buffer Width, Gutter) (Ft)</b> | 9ft to 12ft                       | 9ft to 12ft                         | 9ft to 12ft                              | 5                                       |
| <b>Speed Limit or Prevailing Speed<sup>A</sup> (MPH)</b>           | 30                                | 30                                  | 30                                       | 25                                      |
| <b>Physically Separated Bike Lane?</b>                             | Yes                               | Yes                                 | Yes                                      | No                                      |
| <b>Existing BLTS Score<sup>B</sup></b>                             | 4                                 | 4                                   | 4  | 3                                       |
| <b>Alternative 2 BLTS Score</b>                                    | 1                                 | 1                                   | 1  | 2                                       |

Source: DKS Associates, 2025. Mineta Transportation Institute, Low Stress Bicycling and Network Connectivity.

A Alternative 1 recommends speed limit reductions throughout the corridor. This analysis was conducted under the assumption that existing speed limits have been reduced by 5 mph.

B Existing BLTS has variability in score for Segment 3 and Segment 4 as the analysis was done bi-directional. The Existing BLTS Score included in Table 7 is the highest existing score per segment for the purpose of this analysis.



**Figure 16: Bicycle Level of Traffic Stress – Alternative 2**

## Traffic Operations Analysis

The analysis for Alternative 2 includes adjustments to the number of vehicle lanes on Norwood Avenue and basic changes to intersection operational characteristics that would be associated with this lane removal. Signal timing adjustments were made in relation to the proposed improvements and to accommodate higher traffic volumes associated with future growth. All signals were assumed to operate without coordination, but signal coordination would likely improve operations from the results shown. Due to limitations in the analysis software, dedicated bicycle phases were not evaluated at the study intersections, but it is likely that there is sufficient vehicle capacity based on these results to incorporate dedicated bicycle phasing into the design at select locations. Table 7 shows a comparison of anticipated future intersection delays compared to existing operations. Note that for the purposes of the traffic operations analysis that Alternatives 2A, 2B, and 2C are effectively the same so only one analysis was completed.

95<sup>th</sup> percentile queues were also evaluated for Alternative 2. The AM and PM peak hour queues are shown in Figure 17 and Figure 18 respectively. In these figures, lines are shown on each approach to the intersection representing the queue for the left turn lane (if one exists), the through movements, and the right turn lane (if one exists). These queues are generally color coded as green if they are less than the available vehicle storage, yellow if they are at or near the available vehicle storage, and red if they exceed the available vehicle storage or block access to adjacent lanes. Note that 95<sup>th</sup> percentile queues represent the longest queue that is likely to be observed during the peak hour and most queues would be shorter. From this analysis, the key finding is that queues are longest at the intersections which comprise the I-80 interchange. There are other locations where queues exceed their available storage along Norwood Avenue, but in most cases it is due to short formal turn pockets being blocked by through movement queues. When compared to Alternative 1, queues are shorter in Alternative 2 at Bell Avenue, Morey Avenue, and Silver Eagle Road where the roundabouts would be installed with this alternative. Queues are longer at Harris Avenue and Jessie Avenue due to the reduction in travel lanes through the intersection. At Harris Avenue, this could be an issue as northbound queues would extend back to Grand Avenue. This could be addressed by adjusting the proposed design at Harris Avenue to maintain two through lanes in the northbound direction and should be evaluated further at the project design phase if Alternative 2 is selected as the preferred Alternative.

**Table 7: Future (2045) Alternative 2 Intersection Operational Analysis Results**

| Intersection                                     | AM Peak Hour <sup>A</sup> |               | PM Peak Hour <sup>A</sup> |               |
|--|---------------------------|---------------|---------------------------|---------------|
|  | Existing                  | Future Alt. 2 | Existing                  | Future Alt. 2 |
| <b>1. Norwood Avenue / Bell Avenue</b>           | 20.6 (C)                  | 16.2 (B)      | 17.6 (B)                  | 15.4 (B)      |
| <b>2. Norwood Avenue / Jessie Avenue</b>         | 28.2 (C)                  | 53.1 (D)      | 23.8 (C)                  | 44.6 (D)      |
| <b>3. Norwood Avenue / WB 80 Ramps</b>           | 10.9 (B)                  | 12.6 (B)      | 10.3 (B)                  | 14.2 (B)      |
| <b>4. Norwood Avenue / EB 80 Ramps</b>           | 12.0 (B)                  | 14.4 (B)      | 12.0 (B)                  | 14.2 (B)      |
| <b>5. Norwood Avenue / Harris Avenue</b>         | 19.7 (B)                  | 29.1 (C)      | 19.2 (B)                  | 36.1 (D)      |
| <b>Norwood Avenue / Morey Avenue<sup>B</sup></b> | -                         | 8.5 (A)       | -                         | 9.9 (A)       |
| <b>6. Norwood Avenue / Silver Eagle Road</b>     | 18.6 (B)                  | 13.9 (B)      | 18.2 (B)                  | 18.0 (B)      |

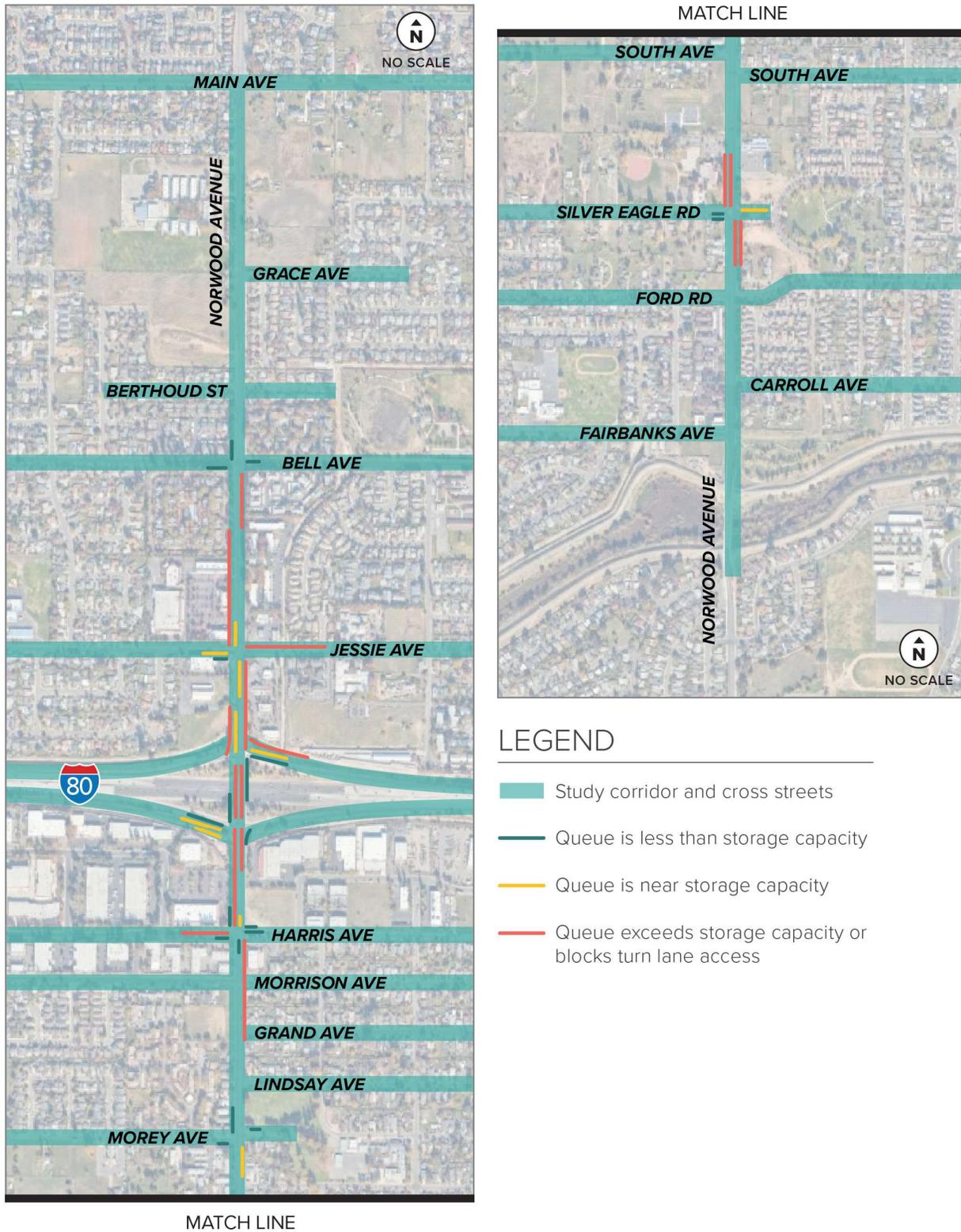
Source: DKS Associates, March 2025.

**Notes:**

- A. 20.6 (C) = Delay (LOS)
- B. Not a study intersection, provided for informational purposes because of recommended control modifications



**Figure 17: Future (2045) AM Peak Hour 95th Percentile Intersection Queues Alternative 2**



**Figure 18: Future (2045) PM Peak Hour 95th Percentile Intersection Queues Alternative 2**

## **Safety Benefit Assessment**

Alternative 2 provides safety benefits through traffic calming and separation of travel modes. This alternative would reduce speeds by narrowing vehicle travel lanes, removing a vehicle travel lane per direction, adding roundabouts at Bell Avenue, Morey Avenue, and Silver Eagle Road, and by reducing the speed limit on Norwood Avenue. The roundabouts at Bell Avenue and Silver Eagle Road also address the collision trends observed at these intersections by lowering speeds and eliminating several vehicle conflicts within the intersections.

The addition of a separated bikeway would separate those riding bicycles from vehicle traffic, reducing the observed trend of bicycle involved collisions. Added crossing opportunities would help address the observed trend of pedestrian involved collisions along Norwood Avenue at unmarked crossing locations.

## **Transit Assessment**

Alternatives 2A and 2B provide opportunities for transit stop enhancements beyond the improvements identified by SacRT. The landscaping strip included with these alternatives gives space for expanding loading platforms and adding stop amenities such as benches and shade structures. Alternative 2B eliminates the landscape strip on the east side of the street to allow for a wider landscape strip on the west side of the street which can include tree planting. This modification means there would be fewer opportunities for enhanced bus stops with Alternative 2B when compared with Alternative 2A. In Alternatives 2A and 2B, the conflicts between the bus and people on bicycles would need to be handled at each stop and would follow SacRTs standard design plans.

Alternative 2C provides the same benefits as Alternative 2A, but because the bike path starts at sidewalk level, it would be easier to address the conflicts between those riding bicycles and those boarding transit. Additionally, the wider landscaping strips would allow for greater space at transit stops for amenities.

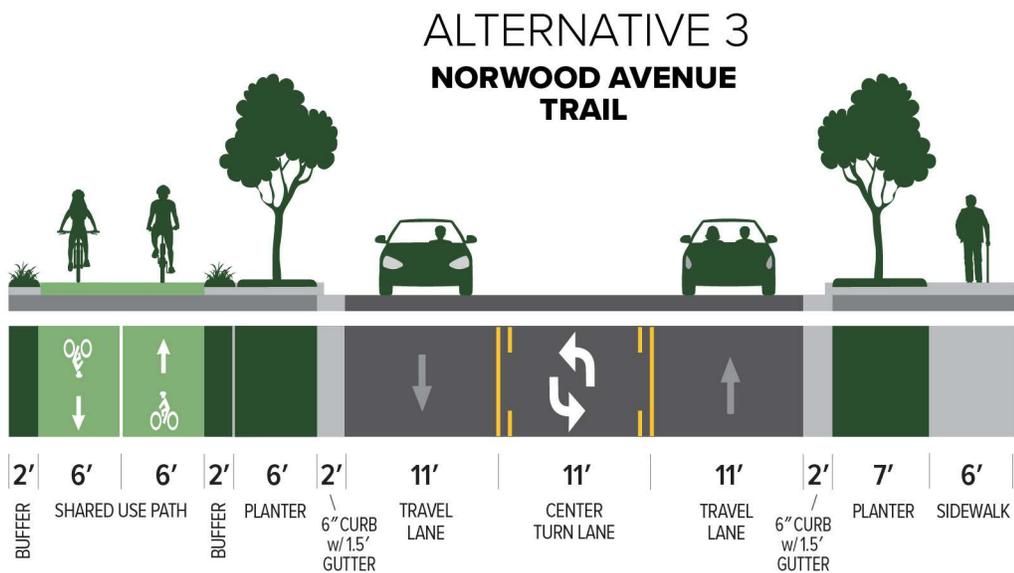
## **Community Priority Alignment**

In addition to the safety benefits described above, Alternative 2 includes the addition of three new marked and signalized pedestrian crosswalks and signalizes pedestrian crossings at the freeway ramps. Alternative 2 also provides a low stress environment for people walking, biking, and accessing transit along most of the corridor by reducing traffic speeds and separating travel modes with physical buffers. The only gap in the low stress environment is across the freeway interchange.

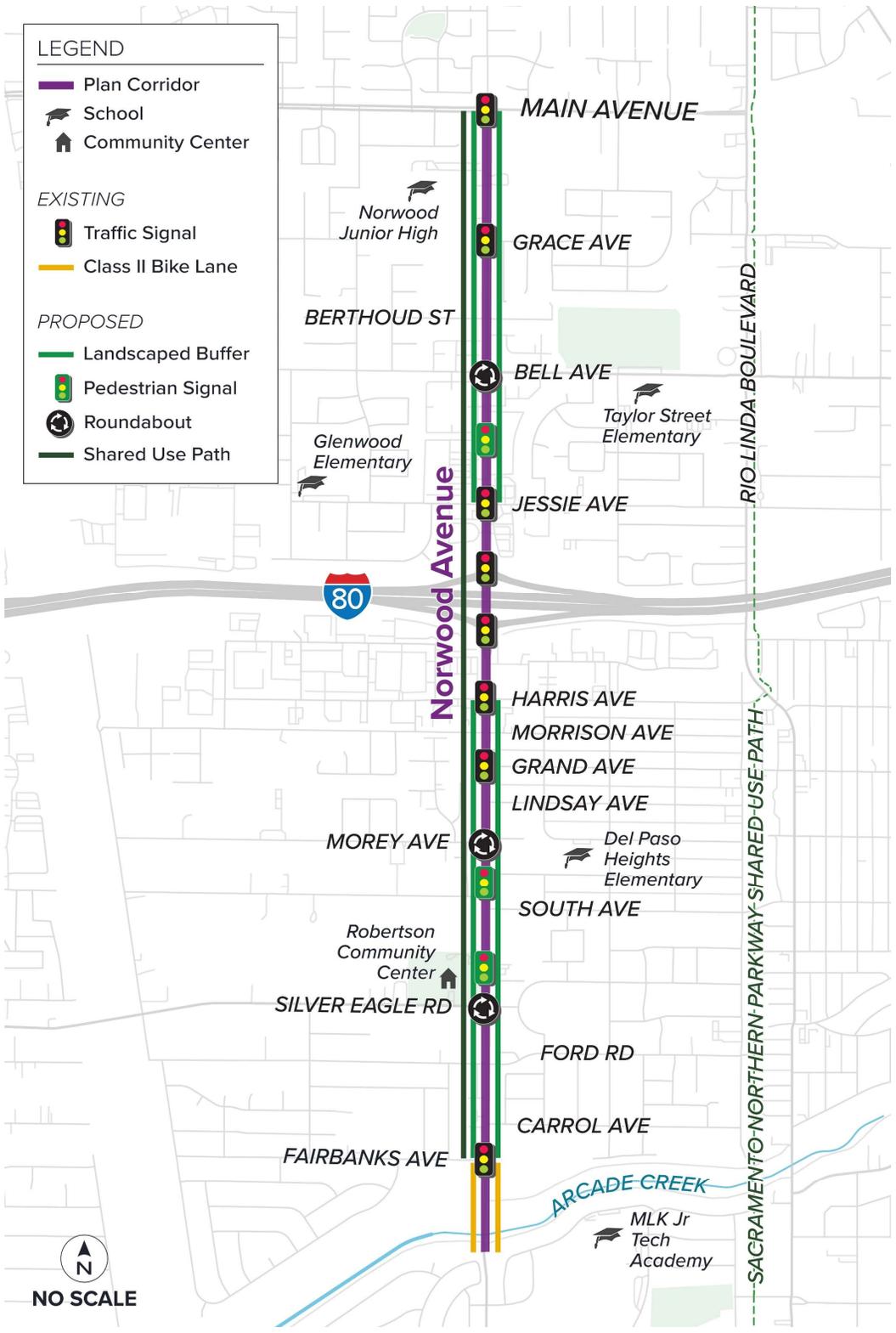
## Alternative 3

### Description

Alternative 3 proposes installing a Class I shared use path along Norwood Avenue by reallocating space from one of the vehicle travel lanes in each direction. The proposed cross section for Alternative 3 is shown in Figure 19. Figure 20 shows a representative map view of Norwood Avenue and where improvements would be applied for Alternative 3. The elements in this alternative include:



**Figure 19: Alternative 3 Cross-Section**



**Figure 20: Alternative 3 Plan View of Proposed Improvements**

## **Reallocate Street Space from Driving to Walking and Bicycling: Fairbanks Avenue to Harris Avenue and from Jessie Avenue to Grace Avenue**

In order to create space for walking and bicycling improvements along the majority of the corridor, the number of vehicle travel lanes would be reduced from two per direction with a center running two way left turn lane to one per direction with a center running two way left turn lane. Sections south of Fairbanks Avenue and north of Grace Avenue would maintain their current cross-sections. The section from Harris Avenue to Jessie Avenue would be maintained as two lanes per direction to provide capacity for higher car and truck volumes and demands at the I-80 Interchange.

## **Install Roundabouts at Silver Eagle Road, Morey Avenue, and Bell Avenue**

A single lane roundabout at Silver Eagle Road and Morey Avenue would slow traffic in the vicinity of the Robertson Community Center and two nearby parks.

A single lane roundabout at Morey Avenue would also provide better pathing for people wanting to cross the street at Morey Avenue, which is currently an offset intersection with a marked crossing in the middle of the intersection.

A single lane roundabout at Bell Avenue would slow southbound vehicles as they approach the higher residential density and commercial portion of the corridor. It would also reduce conflict points at a high crash frequency location.

All three roundabout locations have undergone a preliminary review for right-of-way requirements to install a single lane roundabout and it was found that a roundabout could be installed at each location without impacting existing structures or causing a loss of use for adjacent developed properties.

## **Install Shared Use Path**

Removing an existing vehicle travel lane in each direction would provide sufficient space to add a shared use path to the western side of the corridor. This would be at sidewalk level and be separated from vehicle traffic by a planted buffer. Street and driveway crossings of the path would have conflict zone striping to alert people driving and people using the path of the crossing conflict. North of Grace Avenue, this design should be coordinated with developers so right-of-way can be preserved for this future improvement. The shared use path should end at Fairbanks Avenue with wayfinding directing people on bicycles to the Sacramento Northern Parkway shared use path.

## **Install Shared Use Path over I-80**

There is insufficient width on the existing Norwood Avenue overcrossing structure over I-80 to provide a lower stress crossing of the freeway. To create a lower stress method to connect people walking, rolling, and biking over I-80, a separated facility using either a cantilevered structure attached to the overpass or an independent structure would need to

be constructed between Jessie Avenue and Harris Avenue on the west side of Norwood Avenue. This would require significant design work and right-of-way acquisition beyond the scope of the current study so a specific alignment is not included. The goal should be to place this new facility on the west side of the street to align with the proposed shared use path. An alternative option to a fully separated structure could be a cantilevered path off of the existing bridge structure. This would be a lower cost option but may not be structurally feasible. Both options should be reviewed during the design process should Alternative 3 be selected as the preferred alternative.

### **Widen Sidewalks and Add Landscape Buffer**

Similar to other alternatives, Alternative 3 includes wider sidewalks and a landscape buffer. Sidewalks would be widened to greater than five feet in width along the full corridor. The specific width of the landscaped buffer would vary throughout the corridor based on available right-of-way. Generally, the landscaped buffer would be at least eight feet (six feet dedicated landscaping plus two feet shoulder of shared use path) on the west side of the street and seven feet on the east side of the street. This would allow for larger shade trees to be planted on the west side of the street and small to medium sized trees to be planted on the east side of the street.

### **Install Sidewalk Scale Lighting**

Sidewalk scale lighting along the entire length of the corridor would ensure the area where people are walking is illuminated and increase comfort and feelings of security and safety.

### **Relocate Utilities**

The installation of a landscape buffer and wider sidewalks would allow for an opportunity to relocate utility poles either outside of the walkway or underground to provide appropriate sidewalk widths. This would require collaboration with and support from utility providers.

### **Install In-Lane Bus Stops**

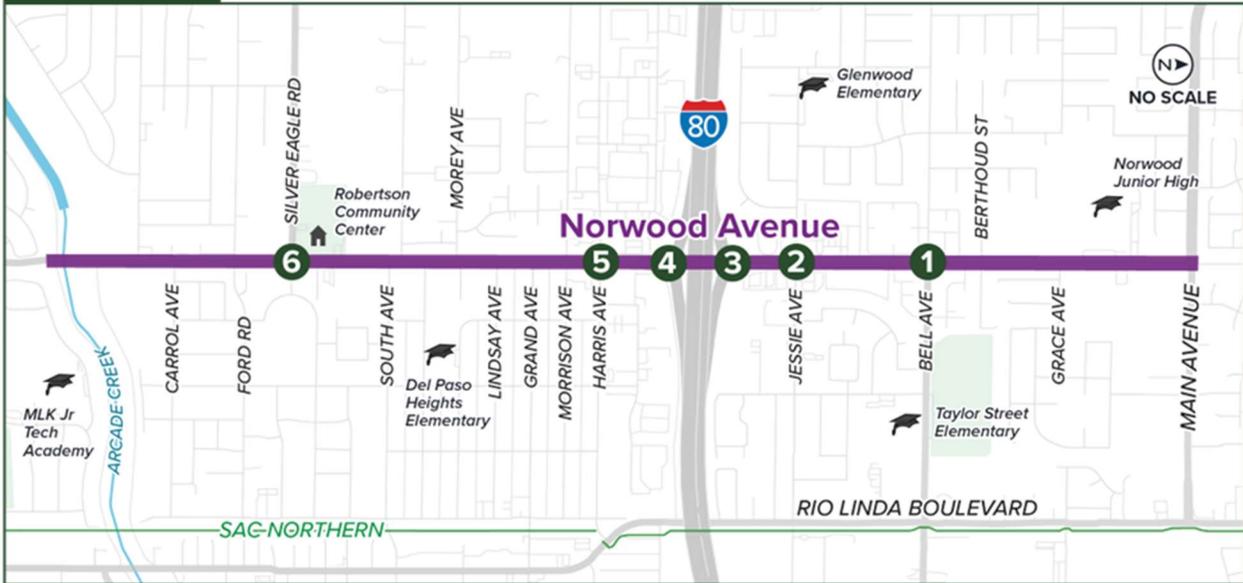
The sidewalk would be extended to allow for the bus to load passengers directly from the vehicle travel lane, with the shared use path continuing behind the bus stop. By allowing buses to stop in-lane, transit time reliability is improved by not requiring the bus to seek gaps in traffic to re-enter the travel lane. This is recommended as the default treatment for all bus stops along the corridor, but design specifics would have to be determined in coordination with SacRT , such as those requiring space for a bus to dwell for schedule adherence.

## Feasibility Analysis

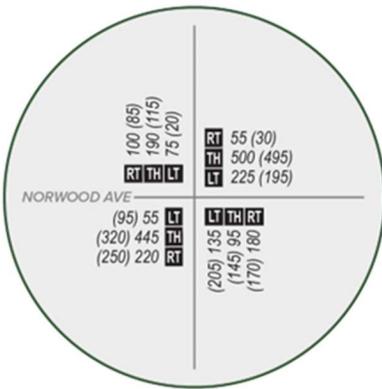
### Travel Demand Forecasting

For the purposes of travel demand forecasting, Alternative 3 is effectively the same as Alternative 2 and thus the results in this section match those reported under Alternative 2. Based on the SacSim-19 travel demand model as modified for the City of Sacramento 2040 General Plan Update, future volumes on Norwood Avenue range between 17,000 and 37,000 AADT for Alternative 3. The highest volumes are on the segment between Jessie Avenue and Harris Avenue. These volumes drop to the 21,000-25,000 AADT range between Jessie Avenue and Bell Avenue and between Harris Avenue and Grand Avenue. North of Bell Avenue and south of Grand Avenue, volumes drop to the 17,000-20,000 AADT range. These daily volumes are lower than Alternative 1 due to the reduction in travel lanes. A portion of the volume which were using Norwood Avenue before the reduction in travel lanes would instead use parallel streets such as Northgate Boulevard and Rio Linda Boulevard. The Travel demand model was also used to forecast future turning movement demand volumes at study intersection along the corridor. These volumes are shown in **Figure 14**.

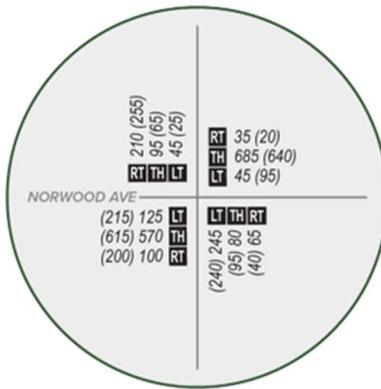
Alternative 3 does reduce the total number of vehicle travel lanes on Norwood Avenue which could potentially cause an increase in VMT related to the infrastructure project. Based on the Transportation Analysis under CEQA for Projects on the State Highway System guidelines published by Caltrans, projects which reduce the number of through lanes and projects which add or enhance bikeways and walking facilities would not likely lead to a measurable increase in VMT. All elements which are proposed under Alternative 3 would meet the State's screening criteria guidance for VMT analysis and do not require further evaluation for VMT impacts.



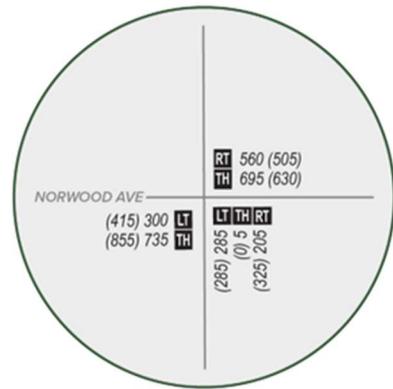
**1** BELL AVE / NORWOOD AVE



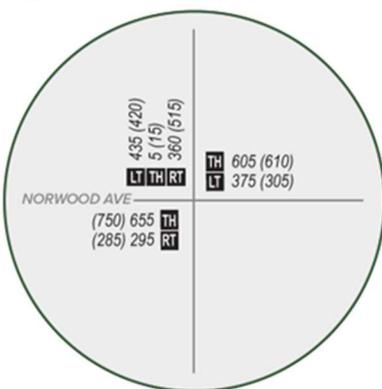
**2** JESSIE AVE / NORWOOD AVE



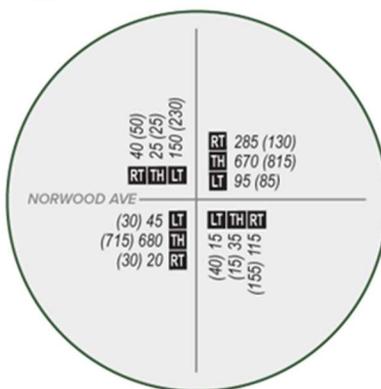
**3** I-80 WB RAMPS / NORWOOD AVE



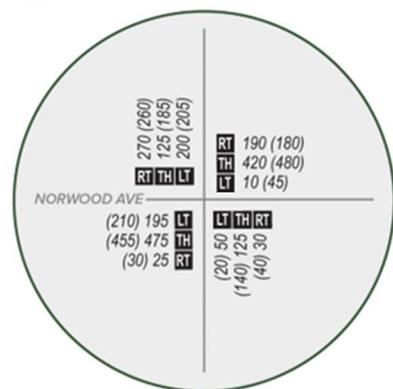
**4** I-80 EB RAMPS / NORWOOD AVE



**5** HARRIS AVE / NORWOOD AVE



**6** SILVER EAGLE RD / NORWOOD AVE



- Plan Corridor
- School
- Community Center
- Study Intersection
- Traffic Volume Movements  
LT • TH • RT

**Figure 21: Future (2045) Turning Movement Volumes Alternative 3**

### Level of Traffic Stress Analysis

The focus of Alternative 3 is to provide significant improvements for those walking, biking, and rolling by reallocating existing right-of-way away from vehicles and towards walking and biking. This alternative adds new crossing opportunities and widens the sidewalks on Norwood Avenue. Additionally, this alternative provides a shared use path on the west side of the street to enhance safety and comfort for those walking, biking, and rolling. Table 8 and Table 9 show the evaluation of the walking and biking level of traffic stress. Figure 22 and Figure 23 show the results of this evaluation in a map form.

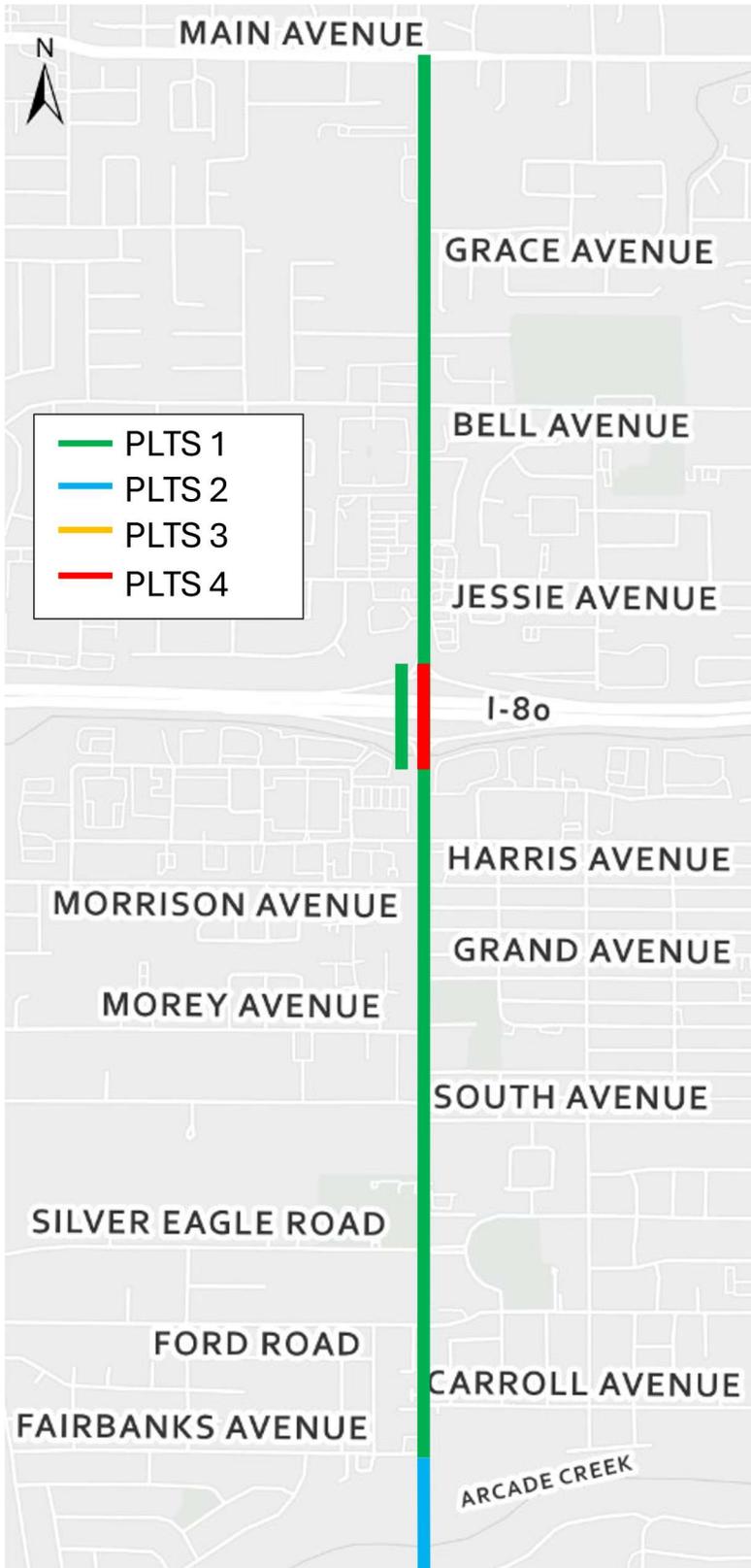
**Table 8: Analysis of Walking Level of Traffic Stress –Alternative 3**

|  | <b>Main Avenue to Bell Avenue</b> | <b>Bell Avenue to I-80 WB Ramps</b> | <b>I-80 EB Ramps to Fairbanks Avenue</b> | <b>Fairbank Avenue to Arcade Creek</b> |
|--|-----------------------------------|-------------------------------------|--|--|
| <b>Street Width (Through Lanes per Direction)</b>        | 1                                 | 1                                   | 1  | 1                                      |
| <b>Buffer Type</b>                                       | Landscaped Buffer                 | Landscaped Buffer                   | Landscaped Buffer                        | None                                   |
| <b>Total Buffer Width (Ft)</b>                           | 16 ft                             | 16 ft                               | 16 ft                                    | 0                                      |
| <b>Sidewalk Width (Ft)</b>                               | 6                                 | 6                                   | 6  | 6                                      |
| <b>Speed Limit Or Prevailing Speed<sup>A</sup> (MPH)</b> | 30                                | 30                                  | 30                                       | 25                                     |
| <b>Existing PLTS Score<sup>B</sup></b>                   | 4                                 | 4                                   | 4  | 3                                      |
| <b>Alternative 3 PLTS Score</b>                          | 1                                 | 1                                   | 1  | 2                                      |

Source: DKS Associates, 2025. ODOT Level of Traffic Stress Analysis Procedures.

A Alternative 1 recommends speed limit reductions throughout the corridor. This analysis was conducted under the assumption that existing speed limits have been reduced by 5 mph.

B Existing PLTS has variability in score for each segment as the analysis was done bi-directional. The Existing PLTS Score included in Table 4 is the highest existing score per segment for purpose of this analysis.



**Figure 22: Walking Level of Traffic Stress – Alternative 3**

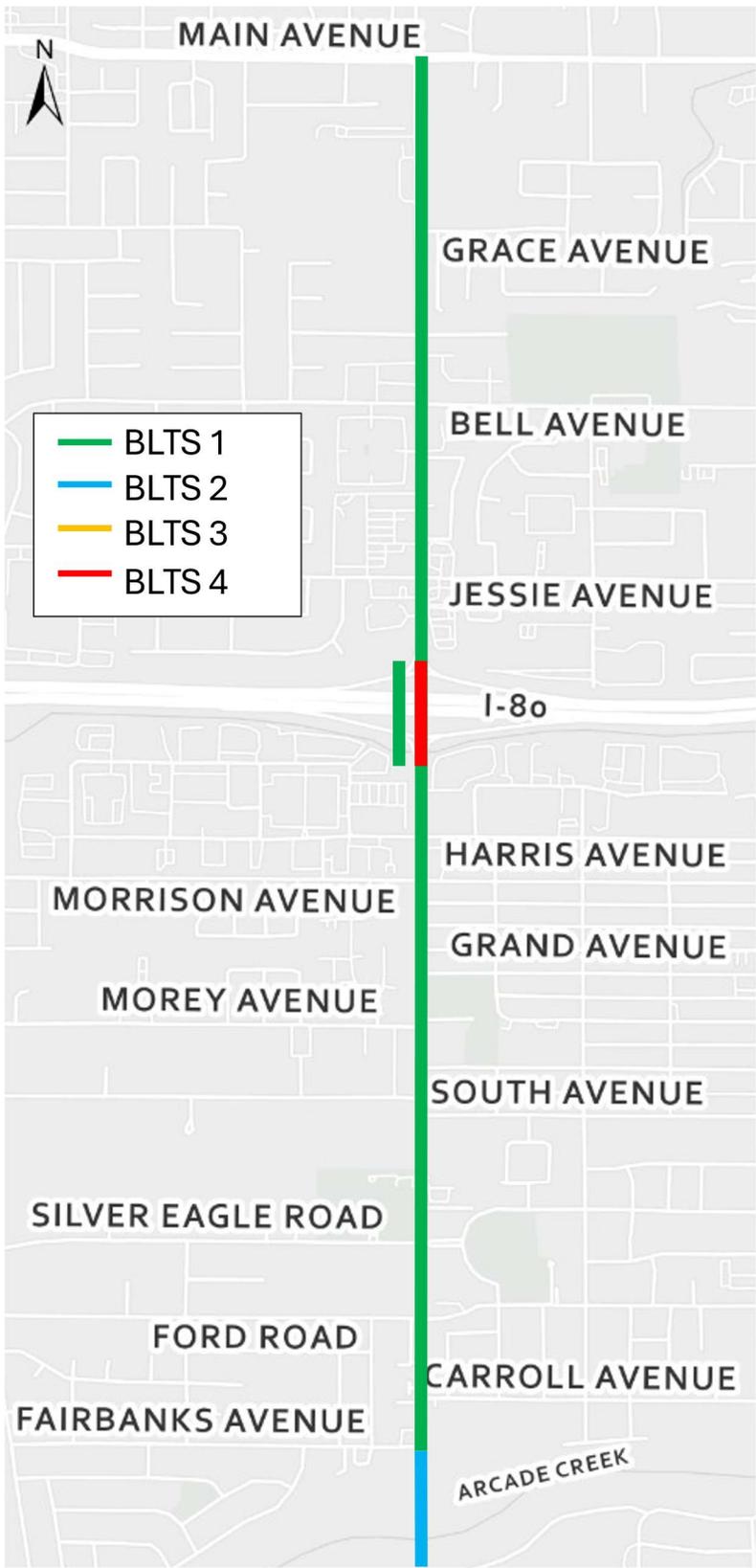
**Table 9. Analysis of Bicycle Level of Traffic Stress – Alternative 3**

|  | <b>Main Avenue to Bell Avenue</b> | <b>Bell Avenue to I-80 EB Ramps</b> | <b>I-80 EB Ramps to Fairbanks Avenue</b> | <b>Fairbanks Avenue to Arcade Creek</b> |
|--|-----------------------------------|-------------------------------------|--|---|
| <b>Street Width (Through Lanes per Direction)</b>                  | 1                                 | 1                                   | 1  | 1                                       |
| <b>Bike Lane Width (Inc. Bike Lane, Buffer Width, Gutter) (Ft)</b> | 16ft                              | 16ft                                | 16ft                                     | 5ft                                     |
| <b>Speed Limit Or Prevailing Speed<sup>A</sup> (MPH)</b>           | 30                                | 30                                  | 30                                       | 25                                      |
| <b>Physically Separated Bike Lane?</b>                             | Yes                               | Yes                                 | Yes                                      | No                                      |
| <b>Existing BLTS Score<sup>B</sup></b>                             | 4                                 | 4                                   | 4  | 3                                       |
| <b>Alternative 3 BLTS Score</b>                                    | 1                                 | 1                                   | 1  | 2                                       |

Source: DKS Associates, 2025. Mineta Transportation Institute, Low Stress Bicycling and Network Connectivity.

A Alternative 1 recommends speed limit reductions throughout the corridor. This analysis was conducted under the assumption that existing speed limits have been reduced by 5 mph.

B Existing BLTS has variability in score for Segment 3 and Segment 4 as the analysis was done bi-directional. The Existing BLTS Score included in Table 7 is the highest existing score per segment for purpose of this analysis.



**Figure 23: Bicycle Level of Traffic Stress – Alternative 3**

## Traffic Operations Analysis

This analysis matches the analysis done for Alternative 2 as from a traffic operations perspective, the two options are nearly identical. Where they differ is in how dedicated bicycle signal phasing would be implemented, but this analysis is beyond the capabilities of the analysis software used for this study. Additionally, more detailed analysis should be conducted on signal operations at a later project phase if Alternative 3 is selected as the preferred alternative.

The analysis for Alternative 3 includes adjustments to the number of vehicle lanes on Norwood Avenue and basic changes to intersection operational characteristics that would be associated with this lane removal. Signal timing adjustments were made in relation to the proposed improvements and to accommodate higher traffic volumes associated with future growth. All signals were assumed to operate without coordination, but signal coordination would likely improve operations from the results shown. Due to limitations in the analysis software, dedicated bicycle phases were not evaluated at the study intersections, but it is likely that there is sufficient vehicle capacity based on these results to incorporate dedicated bicycle phasing into the design at select locations. Table 10 shows a comparison of anticipated future intersection delays compared to existing operations.

95<sup>th</sup> percentile queues were also evaluated for Alternative 2. The AM and PM peak hour queues are shown in Figure 24 and Figure 25 respectively. In these figures, lines are shown on each approach to the intersection representing the queue for the left turn lane (if one exists), the through movements, and the right turn lane (if one exists). These queues are generally color coded as green if they are less than the available vehicle storage, yellow if they are at or near the available vehicle storage, and red if they exceed the available vehicle storage or block access to adjacent lanes. Note that 95<sup>th</sup> percentile queues represent the longest queue that is likely to be observed during the peak hour and most queues would be shorter.

From this analysis, the key finding is that queues are longest at the intersections which comprise the I-80 interchange. There are other locations where queues exceed their available storage along Norwood Avenue, but in most cases it is due to short formal turn pockets being blocked by through movement queues. When compared to Alternative 1, queues are shorter in Alternative 3 at Bell Avenue, Morey Avenue, and Silver Eagle Road where the roundabouts would be installed with this alternative. Queues are longer at Harris Avenue and Jessie Avenue due to the reduction in travel lanes through the intersection. At Harris Avenue, this could be an issue as northbound queues would extend back to Grand Avenue. This could be addressed by adjusting the proposed design at Harris Avenue to maintain two through lanes in the northbound direction and should be evaluated further at the project design phase if Alternative 3 is selected as the preferred Alternative.

**Table 10: Future (2045) Alternative 3 Intersection Operational Analysis Results**

| Intersection                                     | AM Peak Hour <sup>A</sup> |               | PM Peak Hour <sup>A</sup> |               |
|--|---------------------------|---------------|---------------------------|---------------|
|  | Existing                  | Future Alt. 3 | Existing                  | Future Alt. 3 |
| <b>1. Norwood Avenue / Bell Avenue</b>           | 20.6 (C)                  | 16.2 (B)      | 17.6 (B)                  | 15.4 (B)      |
| <b>2. Norwood Avenue / Jessie Avenue</b>         | 28.2 (C)                  | 53.1 (D)      | 23.8 (C)                  | 44.6 (D)      |
| <b>3. Norwood Avenue / WB 80 Ramps</b>           | 10.9 (B)                  | 12.6 (B)      | 10.3 (B)                  | 14.2 (B)      |
| <b>4. Norwood Avenue / EB 80 Ramps</b>           | 12.0 (B)                  | 14.4 (B)      | 12.0 (B)                  | 14.2 (B)      |
| <b>5. Norwood Avenue / Harris Avenue</b>         | 19.7 (B)                  | 29.1 (C)      | 19.2 (B)                  | 36.1 (D)      |
| <b>Norwood Avenue / Morey Avenue<sup>B</sup></b> | -                         | 8.5 (A)       | -                         | 9.9 (A)       |
| <b>6. Norwood Avenue / Silver Eagle Road</b>     | 18.6 (B)                  | 13.9 (B)      | 18.2 (B)                  | 18.0 (B)      |

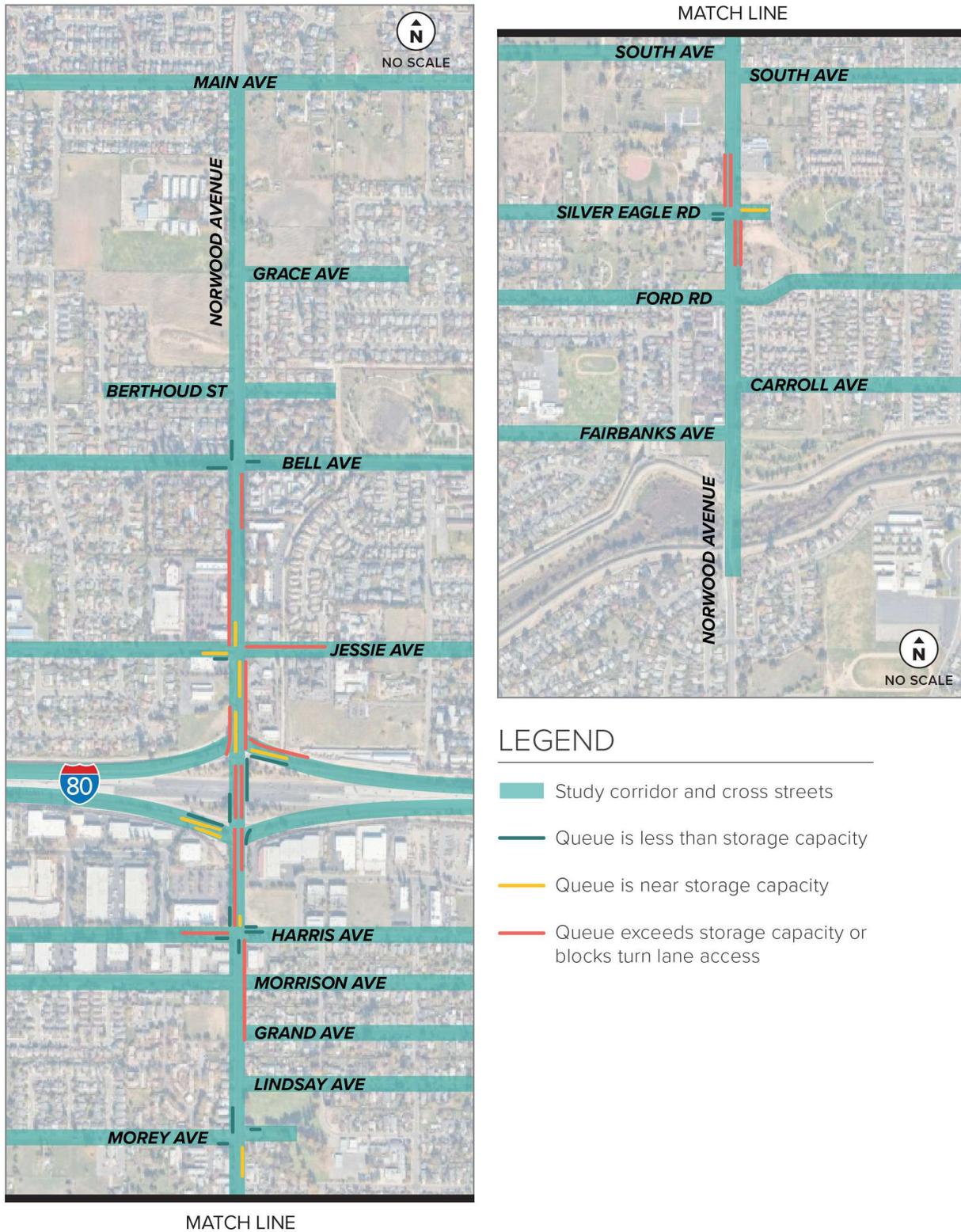
Source: DKS Associates, March 2025.

**Notes:**

- A. 20.6 (C) = Delay (LOS)
- B. Not a study intersection, provided for informational purposes because of recommended control modifications



**Figure 24: Future (2045) AM Peak Hour 95th Percentile Intersection Queues Alternative 3**



**Figure 25: Future (2045) PM Peak Hour 95th Percentile Intersection Queues Alternative 3**

## **Safety Benefit Assessment**

Alternative 3 provides safety benefits through traffic calming and separation of travel modes. This alternative would reduce speeds by narrowing vehicle travel lanes, removing a vehicle travel lane per direction, adding roundabouts at Bell Avenue, Morey Avenue, and Silver Eagle Road, and by reducing the speed limit on Norwood Avenue. The roundabouts at Bell Avenue and Silver Eagle Road also address the collision trends observed at these intersections by lowering speeds and eliminating several vehicle conflicts within the intersections.

The addition of a shared use path would separate those riding bicycles from vehicle traffic, reducing the observed trend of bicycle involved collisions. Added crossing opportunities would help address the observed trend of pedestrian involved collisions along Norwood Avenue at unmarked crossing locations.

## **Transit Assessment**

Alternative 3 would provide similar transit benefit opportunities as Alternative 2C and provide for transit stop enhancements beyond the improvements identified by SacRT. The landscaping strip included with this alternative gives space for expanding loading platforms and adding stop amenities such as benches and shade structures.

Alternative 3 provides space for people riding bikes at the sidewalk level so conflicts between transit vehicles and people riding bikes is not a concern with this alternative. The wide landscaping strip would allow for stops to be designed where those boarding transit are not in conflict with people riding bikes.

## **Community Priority Alignment**

In addition to the safety benefits described above, Alternative 3 includes the addition of three new marked and signalized pedestrian crosswalks and signalizes pedestrian crossings at the freeway ramps. Alternative 3 also provides a low stress environment for people walking, biking, and accessing transit along the entire corridor by reducing traffic speeds and separating travel modes with physical buffers, including a separated structure across the freeway interchange.

## Comparison of Alternative Analysis Results

**Table 11** on the next page summarizes the findings of this report in regards to how the proposed alternatives perform on key metrics in comparison with each other. Each alternative is compared based on how it addresses mobility and safety along the corridor. Discussion with the community is still underway to better understand which alternative best aligns with local community values so no one alternative is recommended over another at this time.

**Table 11: Comparison of Alternatives**

| Metric                                | No Build  | Alt. 1  | Alt. 2  | Alt. 3   |
|---------------------------------------|---|---|---|--|
| Defining Characteristics              | No Change   | <ul style="list-style-type: none"> <li>• Additional Crossing Opportunities</li> <li>• Widen Sidewalk on West Side of Street</li> </ul>                            | <ul style="list-style-type: none"> <li>• Additional Crossing Opportunities</li> <li>• Separated Bikeway</li> <li>• Landscaped buffers</li> <li>• Roundabouts at Bell Ave, Morey Ave, and Silver Eagle Rd</li> </ul> | <ul style="list-style-type: none"> <li>• Additional Crossing Opportunities</li> <li>• Shared Use Path</li> <li>• Landscaped buffers</li> <li>• Roundabouts at Bell Ave, Morey Ave, and Silver Eagle Rd</li> <li>• Shared Use Path Over I-80</li> </ul> |
| Average Level of Traffic Stress       |   |   |   |  |
| Walking                               |   | 3   | 1   | 1  |
| Biking                                |   | 3   | 1   | 1  |
| Travel Demand                         |   |   |   |  |
| Traffic Diversion to Parallel Streets | N/A   | None  | ~10%  | ~10%   |
| Increases in VMT                      | N/A   | None  | None  | None   |
| Traffic Operations                    |   |   |   |  |
| Intersection Delay                    | LOS C or Better   | LOS C or Better   | LOS D or Better   | LOS D or Better  |
| Extensive Queues                      | <ul style="list-style-type: none"> <li>• Jessie Ave</li> <li>• I-80 WB Ramps</li> <li>• I-80 EB Ramps</li> <li>• Harris Ave</li> <li>• Silver Eagle Rd</li> </ul> | <ul style="list-style-type: none"> <li>• Jessie Ave</li> <li>• I-80 WB Ramps</li> <li>• I-80 EB Ramps</li> <li>• Harris Ave</li> <li>• Silver Eagle Rd</li> </ul> | <ul style="list-style-type: none"> <li>• Jessie Ave</li> <li>• I-80 WB Ramps</li> <li>• I-80 EB Ramps</li> <li>• Harris Ave</li> </ul>  | <ul style="list-style-type: none"> <li>• Jessie Ave</li> <li>• I-80 WB Ramps</li> <li>• I-80 EB Ramps</li> <li>• Harris Ave</li> </ul>   |

| Metric                       | No Build | Alt. 1  | Alt. 2   | Alt. 3   |
|------------------------------|----------|---|--|--|
| Safety Improvements          |          |   |  |  |
| Added Crossing Opportunities | N/A      | 3   | 3  | 3  |
| Traffic Calming Elements     | N/A      | <ul style="list-style-type: none"> <li>• Speed Limit Reduction</li> <li>• Lane Width Reduction</li> </ul>                             | <ul style="list-style-type: none"> <li>• Speed Limit Reduction</li> <li>• Lane Width Reduction</li> <li>• Roundabout at Bell Ave</li> <li>• Roundabout at Morey Ave</li> <li>• Roundabout at Silver Eagle Rd</li> </ul>                | <ul style="list-style-type: none"> <li>• Speed Limit Reduction</li> <li>• Lane Width Reduction</li> <li>• Roundabout at Bell Ave</li> <li>• Roundabout at Morey Ave</li> <li>• Roundabout at Silver Eagle Rd</li> </ul>                |
| Other Safety Enhancements    | N/A      | <ul style="list-style-type: none"> <li>• Removal of On-Street Parking</li> <li>• Crossing Enhancements at I-80 Interchange</li> </ul> | <ul style="list-style-type: none"> <li>• Removal of On-Street Parking</li> <li>• Crossing Enhancements at I-80 Interchange</li> <li>• Separated Bikeways</li> <li>• Landscaped Buffers</li> <li>• Pedestrian Scale Lighting</li> </ul> | <ul style="list-style-type: none"> <li>• Removal of On-Street Parking</li> <li>• Crossing Enhancements at I-80 Interchange</li> <li>• Separated Bikeways</li> <li>• Landscaped Buffers</li> <li>• Pedestrian Scale Lighting</li> </ul> |
| Transit Enhancements         | N/A      | <ul style="list-style-type: none"> <li>• Added Bus Shelters</li> <li>• Wider Sidewalks Increase Waiting Area</li> </ul>               | <ul style="list-style-type: none"> <li>• Added Bus Shelters</li> <li>• Wider Sidewalks Increase Waiting Area</li> <li>• In Lane Bus Stops</li> </ul>   | <ul style="list-style-type: none"> <li>• Added Bus Shelters</li> <li>• Wider Sidewalks Increase Waiting Area</li> <li>• In Lane Bus Stops</li> </ul>   |

# Appendix



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## **Section 1. Synchro Intersection Analysis Results**

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# HCM 7th Signalized Intersection Summary

## 1: Norwood Avenue & Bell Avenue

Future No Build AM

|  |  |  |  |  |  |  |  |  |  |  |  |  |
|--|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |  |  |   |  |  |  |  |  |  |  |  |  |
| Traffic Volume (veh/h)   | 60  | 150   | 155   | 220   | 90  | 155   | 70  | 515   | 250   | 145   | 635   | 45  |
| Future Volume (veh/h)  | 60  | 150   | 155   | 220   | 90  | 155   | 70  | 515   | 250   | 145   | 635   | 45  |
| Initial Q (Qb), veh  | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 0.96  | 1.00  |   | 0.97  | 1.00  |   | 0.97  | 1.00  |   | 0.97  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   | No  |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1885  | 1885  | 1885  | 1841  | 1841  | 1841  | 1856  | 1856  | 1856  | 1856  | 1856  | 1856  |
| Adj Flow Rate, veh/h   | 60  | 150   | 155   | 220   | 90  | 155   | 70  | 515   | 250   | 145   | 635   | 45  |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 1   | 1   | 1   | 4   | 4   | 4   | 3   | 3   | 3   | 3   | 3   | 3   |
| Cap, veh/h   | 450   | 203   | 210   | 272   | 253   | 209   | 188   | 740   | 320   | 262   | 853   | 60  |
| Arrive On Green  | 0.25  | 0.24  | 0.24  | 0.16  | 0.14  | 0.14  | 0.11  | 0.21  | 0.21  | 0.15  | 0.26  | 0.26  |
| Sat Flow, veh/h  | 1795  | 831   | 859   | 1753  | 1841  | 1520  | 1767  | 3526  | 1525  | 1767  | 3331  | 236   |
| Grp Volume(v), veh/h   | 60  | 0   | 305   | 220   | 90  | 155   | 70  | 515   | 250   | 145   | 336   | 344   |
| Grp Sat Flow(s),veh/h/ln   | 1795  | 0   | 1690  | 1753  | 1841  | 1520  | 1767  | 1763  | 1525  | 1767  | 1763  | 1804  |
| Q Serve(g_s), s  | 1.8   | 0.0   | 11.6  | 8.5   | 3.1   | 5.1   | 2.6   | 9.4   | 5.6   | 5.3   | 12.2  | 12.3  |
| Cycle Q Clear(g_c), s  | 1.8   | 0.0   | 11.6  | 8.5   | 3.1   | 5.1   | 2.6   | 9.4   | 5.6   | 5.3   | 12.2  | 12.3  |
| Prop In Lane   | 1.00  |   | 0.51  | 1.00  |   | 1.00  | 1.00  |   | 1.00  | 1.00  |   | 0.13  |
| Lane Grp Cap(c), veh/h   | 450   | 0   | 413   | 272   | 253   | 209   | 188   | 740   | 320   | 262   | 451   | 462   |
| V/C Ratio(X)   | 0.13  | 0.00  | 0.74  | 0.81  | 0.36  | 0.74  | 0.37  | 0.70  | 0.78  | 0.55  | 0.74  | 0.75  |
| Avail Cap(c_a), veh/h  | 674   | 0   | 1099  | 658   | 1197  | 988   | 668   | 2293  | 992   | 661   | 1147  | 1174  |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Uniform Delay (d), s/veh   | 20.3  | 0.0   | 24.3  | 28.5  | 27.3  | 15.8  | 29.0  | 25.5  | 6.9   | 27.6  | 23.9  | 23.9  |
| Incr Delay (d2), s/veh   | 0.0   | 0.0   | 1.0   | 2.2   | 0.3   | 1.9   | 0.5   | 0.4   | 1.6   | 0.7   | 0.9   | 0.9   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 0.7   | 0.0   | 4.6   | 3.4   | 1.3   | 2.3   | 1.0   | 3.7   | 3.4   | 2.2   | 4.9   | 5.0   |
| Unsig. Movement Delay, s/veh   |   |   |   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 20.3  | 0.0   | 25.3  | 30.6  | 27.6  | 17.8  | 29.5  | 26.0  | 8.5   | 28.3  | 24.8  | 24.8  |
| LnGrp LOS  | C   |   | C   | C   | C   | B   | C   | C   | A   | C   | C   | C   |
| Approach Vol, veh/h  |   | 365   |   |   | 465   |   |   | 835   |   |   | 825   |   |
| Approach Delay, s/veh  |   | 24.5  |   |   | 25.8  |   |   | 21.0  |   |   | 25.4  |   |
| Approach LOS   |   | C   |   |   | C   |   |   | C   |   |   | C   |   |
| Timer - Assigned Phs   | 1   | 2   | 3   | 4   | 5   | 6   | 7   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s   | 22.1  | 14.2  | 11.0  | 22.5  | 14.6  | 21.7  | 14.2  | 19.3  |   |   |   |   |
| Change Period (Y+Rc), s  | * 4.6   | * 4.6   | 3.6   | * 4.6   | 3.8   | * 4.6   | 3.9   | * 4.6   |   |   |   |   |
| Max Green Setting (Gmax), s  | * 26  | * 45  | 26.4  | * 45  | 26.2  | * 45  | 26.1  | * 45  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s   | 3.8   | 7.1   | 4.6   | 14.3  | 10.5  | 13.6  | 7.3   | 11.4  |   |   |   |   |
| Green Ext Time (p_c), s  | 0.1   | 0.5   | 0.1   | 2.9   | 0.3   | 1.4   | 0.2   | 2.6   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   |   |   | 23.9  |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS  |   |   | C   |   |   |   |   |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| * HCM 7th computational engine requires equal clearance times for the phases crossing the barrier. |   |   |   |   |   |   |   |   |   |   |   |   |

# HCM 7th Signalized Intersection Summary

## 2: Norwood Avenue & Jessie Avenue

Future No Build AM

|  |  |  |  |  |  |  |  |  |  |  |  |  |
|--|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |   |  |  |   |  |   |  |  |  |  |  |  |
| Traffic Volume (veh/h)   | 50  | 95  | 215   | 195   | 70  | 55  | 140   | 710   | 105   | 55  | 935   | 45  |
| Future Volume (veh/h)  | 50  | 95  | 215   | 195   | 70  | 55  | 140   | 710   | 105   | 55  | 935   | 45  |
| Initial Q (Qb), veh  | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 1.00  | 1.00  |   | 0.97  | 1.00  |   | 0.97  | 1.00  |   | 1.00  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   | No  |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1870  | 1870  | 1870  | 1856  | 1856  | 1856  | 1856  | 1856  | 1856  | 1856  | 1856  | 1856  |
| Adj Flow Rate, veh/h   | 50  | 95  | 215   | 195   | 70  | 55  | 140   | 710   | 105   | 55  | 935   | 45  |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 2   | 2   | 2   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| Cap, veh/h   | 104   | 198   | 261   | 245   | 88  | 69  | 179   | 1078  | 159   | 136   | 1119  | 54  |
| Arrive On Green  | 0.16  | 0.16  | 0.16  | 0.23  | 0.23  | 0.23  | 0.10  | 0.35  | 0.35  | 0.08  | 0.33  | 0.33  |
| Sat Flow, veh/h  | 634   | 1205  | 1585  | 1059  | 380   | 299   | 1767  | 3067  | 453   | 1767  | 3423  | 165   |
| Grp Volume(v), veh/h   | 145   | 0   | 215   | 320   | 0   | 0   | 140   | 408   | 407   | 55  | 481   | 499   |
| Grp Sat Flow(s),veh/h/ln   | 1839  | 0   | 1585  | 1738  | 0   | 0   | 1767  | 1763  | 1757  | 1767  | 1763  | 1825  |
| Q Serve(g_s), s  | 6.1   | 0.0   | 11.2  | 14.9  | 0.0   | 0.0   | 6.6   | 16.7  | 16.8  | 2.5   | 21.7  | 21.7  |
| Cycle Q Clear(g_c), s  | 6.1   | 0.0   | 11.2  | 14.9  | 0.0   | 0.0   | 6.6   | 16.7  | 16.8  | 2.5   | 21.7  | 21.7  |
| Prop In Lane   | 0.34  |   | 1.00  | 0.61  |   | 0.17  | 1.00  |   | 0.26  | 1.00  |   | 0.09  |
| Lane Grp Cap(c), veh/h   | 303   | 0   | 261   | 401   | 0   | 0   | 179   | 619   | 617   | 136   | 576   | 596   |
| V/C Ratio(X)   | 0.48  | 0.00  | 0.82  | 0.80  | 0.00  | 0.00  | 0.78  | 0.66  | 0.66  | 0.41  | 0.84  | 0.84  |
| Avail Cap(c_a), veh/h  | 784   | 0   | 676   | 741   | 0   | 0   | 547   | 935   | 932   | 547   | 935   | 968   |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 0.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Uniform Delay (d), s/veh   | 32.4  | 0.0   | 34.6  | 31.0  | 0.0   | 0.0   | 37.6  | 23.4  | 23.4  | 37.7  | 26.7  | 26.7  |
| Incr Delay (d2), s/veh   | 0.4   | 0.0   | 2.5   | 1.4   | 0.0   | 0.0   | 2.8   | 0.4   | 0.5   | 0.7   | 1.7   | 1.6   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 2.7   | 0.0   | 4.3   | 6.2   | 0.0   | 0.0   | 2.9   | 6.5   | 6.5   | 1.1   | 9.0   | 9.3   |
| Unsig. Movement Delay, s/veh   |   |   |   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 32.9  | 0.0   | 37.1  | 32.4  | 0.0   | 0.0   | 40.4  | 23.9  | 23.9  | 38.4  | 28.4  | 28.3  |
| LnGrp LOS  | C   |   | D   | C   |   |   | D   | C   | C   | D   | C   | C   |
| Approach Vol, veh/h  |   | 360   |   |   | 320   |   |   | 955   |   |   | 1035  |   |
| Approach Delay, s/veh  |   | 35.4  |   |   | 32.4  |   |   | 26.3  |   |   | 28.9  |   |
| Approach LOS   |   | D   |   |   | C   |   |   | C   |   |   | C   |   |
| Timer - Assigned Phs   |   | 2   | 3   | 4   |   | 6   | 7   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s   |   | 23.3  | 12.2  | 32.6  |   | 17.6  | 10.1  | 34.7  |   |   |   |   |
| Change Period (Y+Rc), s  |   | 3.5   | 3.5   | * 4.6   |   | 3.5   | 3.5   | * 4.6   |   |   |   |   |
| Max Green Setting (Gmax), s  |   | 36.5  | 26.5  | * 45  |   | 36.5  | 26.5  | * 45  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s   |   | 16.9  | 8.6   | 23.7  |   | 13.2  | 4.5   | 18.8  |   |   |   |   |
| Green Ext Time (p_c), s  |   | 1.2   | 0.2   | 4.3   |   | 0.9   | 0.1   | 3.2   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   |   |   | 29.3  |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS  |   |   | C   |   |   |   |   |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| * HCM 7th computational engine requires equal clearance times for the phases crossing the barrier. |   |   |   |   |   |   |   |   |   |   |   |   |

# HCM 7th Signalized Intersection Summary

## 3: Norwood Avenue & WB 80 On-Ramp/WB 80 Off-Ramp

Future No Build AM

|   |  |  |  |  |  |  |   |  |  |  |  |  |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement  | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations   |   |   |   |  |  |  |  |  |  |   |  |  |
| Traffic Volume (veh/h)  | 0   | 0   | 0   | 350   | 5   | 240   | 315   | 845   | 0   | 0   | 855   | 560   |
| Future Volume (veh/h)   | 0   | 0   | 0   | 350   | 5   | 240   | 315   | 845   | 0   | 0   | 855   | 560   |
| Initial Q (Qb), veh   |   |   |   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.   |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)   |   |   |   | 1.00  |   | 1.00  | 1.00  |   | 1.00  | 1.00  |   | 1.00  |
| Parking Bus, Adj  |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach   |   |   |   | No  |   |   | No  |   |   | No  |   |   |
| Adj Sat Flow, veh/h/ln  |   |   |   | 1841  | 1841  | 1841  | 1841  | 1841  | 0   | 0   | 1870  | 1870  |
| Adj Flow Rate, veh/h  |   |   |   | 354   | 0   | 0   | 315   | 845   | 0   | 0   | 855   | 0   |
| Peak Hour Factor  |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %  |   |   |   | 4   | 4   | 4   | 4   | 4   | 0   | 0   | 2   | 2   |
| Cap, veh/h  |   |   |   | 586   | 0   |   | 388   | 2274  | 0   | 0   | 1266  |   |
| Arrive On Green   |   |   |   | 0.17  | 0.00  | 0.00  | 0.22  | 0.65  | 0.00  | 0.00  | 0.36  | 0.00  |
| Sat Flow, veh/h   |   |   |   | 3506  | 0   | 1560  | 1753  | 3589  | 0   | 0   | 3647  | 1585  |
| Grp Volume(v), veh/h  |   |   |   | 354   | 0   | 0   | 315   | 845   | 0   | 0   | 855   | 0   |
| Grp Sat Flow(s),veh/h/ln  |   |   |   | 1753  | 0   | 1560  | 1753  | 1749  | 0   | 0   | 1777  | 1585  |
| Q Serve(g_s), s   |   |   |   | 4.5   | 0.0   | 0.0   | 8.2   | 5.4   | 0.0   | 0.0   | 9.8   | 0.0   |
| Cycle Q Clear(g_c), s   |   |   |   | 4.5   | 0.0   | 0.0   | 8.2   | 5.4   | 0.0   | 0.0   | 9.8   | 0.0   |
| Prop In Lane  |   |   |   | 1.00  |   | 1.00  | 1.00  |   | 0.00  | 0.00  |   | 1.00  |
| Lane Grp Cap(c), veh/h  |   |   |   | 586   | 0   |   | 388   | 2274  | 0   | 0   | 1266  |   |
| V/C Ratio(X)  |   |   |   | 0.60  | 0.00  |   | 0.81  | 0.37  | 0.00  | 0.00  | 0.68  |   |
| Avail Cap(c_a), veh/h   |   |   |   | 2621  | 0   |   | 965   | 2556  | 0   | 0   | 2598  |   |
| HCM Platoon Ratio   |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)  |   |   |   | 1.00  | 0.00  | 0.00  | 1.00  | 1.00  | 0.00  | 0.00  | 1.00  | 0.00  |
| Uniform Delay (d), s/veh  |   |   |   | 18.6  | 0.0   | 0.0   | 17.8  | 3.9   | 0.0   | 0.0   | 13.1  | 0.0   |
| Incr Delay (d2), s/veh  |   |   |   | 0.4   | 0.0   | 0.0   | 3.1   | 0.1   | 0.0   | 0.0   | 0.5   | 0.0   |
| Initial Q Delay(d3), s/veh  |   |   |   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln  |   |   |   | 1.7   | 0.0   | 0.0   | 3.1   | 0.8   | 0.0   | 0.0   | 3.3   | 0.0   |
| Unsig. Movement Delay, s/veh  |   |   |   |   |   | 26.60   |   |   |   |   |   | 22.40   |
| LnGrp Delay(d), s/veh   |   |   |   | 19.0  | 0.0   | 26.6  | 20.9  | 4.0   | 0.0   | 0.0   | 13.6  | 22.4  |
| LnGrp LOS   |   |   |   | B   |   | C   | C   | A   |   |   | B   | C   |
| Approach Vol, veh/h   |   |   |   |   | 474   |   |   | 1160  |   |   | 1135  |   |
| Approach Delay, s/veh   |   |   |   |   | 20.9  |   |   | 8.6   |   |   | 15.8  |   |
| Approach LOS  |   |   |   |   | C   |   |   | A   |   |   | B   |   |
| Timer - Assigned Phs  | 1   | 2   |   | 4   |   |   | 6   |   |   |   |   |   |
| Phs Duration (G+Y+Rc), s  | 14.1  | 22.0  |   | 12.0  |   |   | 36.1  |   |   |   |   |   |
| Change Period (Y+Rc), s   | 3.5   | 4.8   |   | 4.0   |   |   | 4.8   |   |   |   |   |   |
| Max Green Setting (Gmax), s   | 26.5  | 35.2  |   | 36.0  |   |   | 35.2  |   |   |   |   |   |
| Max Q Clear Time (g_c+I1), s  | 10.2  | 11.8  |   | 6.5   |   |   | 7.4   |   |   |   |   |   |
| Green Ext Time (p_c), s   | 0.6   | 5.3   |   | 0.7   |   |   | 5.0   |   |   |   |   |   |
| <b>Intersection Summary</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh  |   |   |   |   |   | 13.6  |   |   |   |   |   |   |
| HCM 7th LOS   |   |   |   |   |   | B   |   |   |   |   |   |   |
| <b>Notes</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| User approved volume balancing among the lanes for turning movement.  |   |   |   |   |   |   |   |   |   |   |   |   |
| Unsignalized Delay for [WBR, SBR] is included in calculations of the approach delay and intersection delay. |   |   |   |   |   |   |   |   |   |   |   |   |

# HCM 7th Signalized Intersection Summary

## 4: Norwood Avenue & EB 80 Off-Ramp/EB 80 On-Ramp

Future No Build AM

|  |  |  |  |  |  |  |  |  |  |  |  |  |
|--|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL  | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |  |  |  |   |   |   |  |  |  |  |  |  |
| Traffic Volume (veh/h)   | 380   | 5   | 510   | 0   | 0   | 0   | 0  | 780   | 300   | 385   | 820   | 0   |
| Future Volume (veh/h)  | 380   | 5   | 510   | 0   | 0   | 0   | 0  | 780   | 300   | 385   | 820   | 0   |
| Initial Q (Qb), veh  | 0   | 0   | 0   |   |   |   | 0  | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  |   |   |   | 1.00   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 1.00  |   |   |   | 1.00   |   | 1.00  | 1.00  |   | 1.00  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  |   |   |   | 1.00   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   |   |   |  | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1826  | 1826  | 1826  |   |   |   | 0  | 1841  | 1841  | 1841  | 1841  | 0   |
| Adj Flow Rate, veh/h   | 384   | 0   | 0   |   |   |   | 0  | 780   | 0   | 385   | 820   | 0   |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  |   |   |   | 1.00   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 5   | 5   | 5   |   |   |   | 0  | 4   | 4   | 4   | 4   | 0   |
| Cap, veh/h   | 619   | 0   |   |   |   |   | 0  | 1117  |   | 458   | 2271  | 0   |
| Arrive On Green  | 0.18  | 0.00  | 0.00  |   |   |   | 0.00   | 0.32  | 0.00  | 0.26  | 0.65  | 0.00  |
| Sat Flow, veh/h  | 3478  | 0   | 1547  |   |   |   | 0  | 3589  | 1560  | 1753  | 3589  | 0   |
| Grp Volume(v), veh/h   | 384   | 0   | 0   |   |   |   | 0  | 780   | 0   | 385   | 820   | 0   |
| Grp Sat Flow(s),veh/h/ln   | 1739  | 0   | 1547  |   |   |   | 0  | 1749  | 1560  | 1753  | 1749  | 0   |
| Q Serve(g_s), s  | 5.2   | 0.0   | 0.0   |   |   |   | 0.0  | 10.0  | 0.0   | 10.6  | 5.5   | 0.0   |
| Cycle Q Clear(g_c), s  | 5.2   | 0.0   | 0.0   |   |   |   | 0.0  | 10.0  | 0.0   | 10.6  | 5.5   | 0.0   |
| Prop In Lane   | 1.00  |   | 1.00  |   |   |   | 0.00   |   | 1.00  | 1.00  |   | 0.00  |
| Lane Grp Cap(c), veh/h   | 619   | 0   |   |   |   |   | 0  | 1117  |   | 458   | 2271  | 0   |
| V/C Ratio(X)   | 0.62  | 0.00  |   |   |   |   | 0.00   | 0.70  |   | 0.84  | 0.36  | 0.00  |
| Avail Cap(c_a), veh/h  | 2457  | 0   |   |   |   |   | 0  | 2416  |   | 912   | 2416  | 0   |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  |   |   |   | 1.00   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 0.00  |   |   |   | 0.00   | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  |
| Uniform Delay (d), s/veh   | 19.3  | 0.0   | 0.0   |   |   |   | 0.0  | 15.2  | 0.0   | 17.8  | 4.1   | 0.0   |
| Incr Delay (d2), s/veh   | 0.4   | 0.0   | 0.0   |   |   |   | 0.0  | 0.6   | 0.0   | 3.2   | 0.1   | 0.0   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   |   |   |   | 0.0  | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 1.9   | 0.0   | 0.0   |   |   |   | 0.0  | 3.3   | 0.0   | 4.1   | 1.1   | 0.0   |
| Unsig. Movement Delay, s/veh   |   |   | 44.50   |   |   |   |  |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 19.7  | 0.0   | 44.5  |   |   |   | 0.0  | 15.8  | 0.0   | 21.0  | 4.2   | 0.0   |
| LnGrp LOS  | B   |   | D   |   |   |   |  | B   |   | C   | A   |   |
| Approach Vol, veh/h  |   | 639   |   |   |   |   |  | 780   |   |   | 1205  |   |
| Approach Delay, s/veh  |   | 29.6  |   |   |   |   |  | 15.8  |   |   | 9.6   |   |
| Approach LOS   |   | C   |   |   |   |   |  | B   |   |   | A   |   |
| Timer - Assigned Phs   |   | 2   |   |   | 5   | 6   |  | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s   |   | 37.9  |   |   | 16.8  | 21.1  |  | 13.1  |   |   |   |   |
| Change Period (Y+Rc), s  |   | 4.8   |   |   | 3.5   | 4.8   |  | 4.0   |   |   |   |   |
| Max Green Setting (Gmax), s  |   | 35.2  |   |   | 26.5  | 35.2  |  | 36.0  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s   |   | 7.5   |   |   | 12.6  | 12.0  |  | 7.2   |   |   |   |   |
| Green Ext Time (p_c), s  |   | 5.3   |   |   | 0.8   | 4.3   |  | 0.7   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |  |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   |   |   | 16.3  |   |   |   |  |   |   |   |   |   |
| HCM 7th LOS  |   |   | B   |   |   |   |  |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |  |   |   |   |   |   |
| User approved volume balancing among the lanes for turning movement.                                   |   |   |   |   |   |   |  |   |   |   |   |   |
| Unsignalized Delay for [EBR] is included in calculations of the approach delay and intersection delay. |   |   |   |   |   |   |  |   |   |   |   |   |

Unsignalized Delay for [NBR] is excluded from calculations of the approach delay and intersection delay.

# HCM 7th Signalized Intersection Summary

## 5: Norwood Avenue & Harris Avenue

Future No Build AM

|  |  |  |  |  |  |  |  |  |  |  |  |  |
|--|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |   |  |  |   |  |  |  |  |  |  |  |  |
| Traffic Volume (veh/h)   | 155   | 15  | 50  | 15  | 30  | 100   | 45  | 840   | 15  | 60  | 985   | 310   |
| Future Volume (veh/h)  | 155   | 15  | 50  | 15  | 30  | 100   | 45  | 840   | 15  | 60  | 985   | 310   |
| Initial Q (Qb), veh  | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 0.98  | 1.00  |   | 0.99  | 1.00  |   | 0.98  | 1.00  |   | 0.98  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   | No  |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1707  | 1707  | 1707  | 1826  | 1826  | 1826  | 1870  | 1870  | 1870  | 1841  | 1841  | 1841  |
| Adj Flow Rate, veh/h   | 155   | 15  | 50  | 15  | 30  | 100   | 45  | 840   | 15  | 60  | 985   | 310   |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 13  | 13  | 13  | 5   | 5   | 5   | 2   | 2   | 2   | 4   | 4   | 4   |
| Cap, veh/h   | 215   | 21  | 321   | 83  | 166   | 212   | 144   | 1522  | 27  | 150   | 1122  | 351   |
| Arrive On Green  | 0.14  | 0.14  | 0.14  | 0.14  | 0.14  | 0.14  | 0.08  | 0.43  | 0.43  | 0.09  | 0.43  | 0.43  |
| Sat Flow, veh/h  | 1489  | 144   | 1413  | 599   | 1197  | 1526  | 1781  | 3570  | 64  | 1753  | 2606  | 815   |
| Grp Volume(v), veh/h   | 170   | 0   | 50  | 45  | 0   | 100   | 45  | 418   | 437   | 60  | 659   | 636   |
| Grp Sat Flow(s),veh/h/ln   | 1633  | 0   | 1413  | 1796  | 0   | 1526  | 1781  | 1777  | 1857  | 1753  | 1749  | 1672  |
| Q Serve(g_s), s  | 7.5   | 0.0   | 2.1   | 1.7   | 0.0   | 4.6   | 1.8   | 13.3  | 13.3  | 2.4   | 26.0  | 26.4  |
| Cycle Q Clear(g_c), s  | 7.5   | 0.0   | 2.1   | 1.7   | 0.0   | 4.6   | 1.8   | 13.3  | 13.3  | 2.4   | 26.0  | 26.4  |
| Prop In Lane   | 0.91  |   | 1.00  | 0.33  |   | 1.00  | 1.00  |   | 0.03  | 1.00  |   | 0.49  |
| Lane Grp Cap(c), veh/h   | 236   | 0   | 321   | 249   | 0   | 212   | 144   | 757   | 792   | 150   | 753   | 720   |
| V/C Ratio(X)   | 0.72  | 0.00  | 0.16  | 0.18  | 0.00  | 0.47  | 0.31  | 0.55  | 0.55  | 0.40  | 0.87  | 0.88  |
| Avail Cap(c_a), veh/h  | 787   | 0   | 798   | 861   | 0   | 732   | 861   | 833   | 871   | 847   | 820   | 784   |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Uniform Delay (d), s/veh   | 30.8  | 0.0   | 23.5  | 28.7  | 0.0   | 30.0  | 32.7  | 16.3  | 16.3  | 32.7  | 19.6  | 19.8  |
| Incr Delay (d2), s/veh   | 1.6   | 0.0   | 0.1   | 0.1   | 0.0   | 0.6   | 0.5   | 0.5   | 0.5   | 0.6   | 9.6   | 10.8  |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 3.0   | 0.0   | 0.7   | 0.7   | 0.0   | 1.6   | 0.8   | 4.8   | 5.1   | 1.0   | 11.6  | 11.5  |
| Unsig. Movement Delay, s/veh   |   |   |   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 32.4  | 0.0   | 23.6  | 28.9  | 0.0   | 30.6  | 33.2  | 16.7  | 16.7  | 33.3  | 29.2  | 30.5  |
| LnGrp LOS  | C   |   | C   | C   |   | C   | C   | B   | B   | C   | C   | C   |
| Approach Vol, veh/h  |   | 220   |   |   | 145   |   |   | 900   |   |   | 1355  |   |
| Approach Delay, s/veh  |   | 30.4  |   |   | 30.0  |   |   | 17.5  |   |   | 30.0  |   |
| Approach LOS   |   | C   |   |   | C   |   |   | B   |   |   | C   |   |
| Timer - Assigned Phs   |   | 2   | 3   | 4   |   | 6   | 7   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s   |   | 14.3  | 9.6   | 37.1  |   | 14.5  | 9.9   | 36.8  |   |   |   |   |
| Change Period (Y+Rc), s  |   | 3.8   | 3.5   | * 4.6   |   | 3.6   | 3.5   | * 4.6   |   |   |   |   |
| Max Green Setting (Gmax), s  |   | 36.2  | 36.5  | * 35  |   | 36.4  | 36.5  | * 35  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s   |   | 6.6   | 3.8   | 28.4  |   | 9.5   | 4.4   | 15.3  |   |   |   |   |
| Green Ext Time (p_c), s  |   | 0.3   | 0.0   | 4.1   |   | 0.7   | 0.1   | 4.0   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   |   |   | 25.8  |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS  |   |   | C   |   |   |   |   |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| * HCM 7th computational engine requires equal clearance times for the phases crossing the barrier. |   |   |   |   |   |   |   |   |   |   |   |   |

HCM 7th Signalized Intersection Summary  
 6: Norwood Avenue & Silver Eagle Road

Future No Build AM

|  |  |  |  |  |  |  |  |  |  |  |  |  |
|--|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL  | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |  |  |   |  |  |   |  |  |  |  |  |  |
| Traffic Volume (veh/h)   | 260   | 110   | 195   | 45  | 115   | 45  | 135  | 600   | 20  | 25  | 665   | 190   |
| Future Volume (veh/h)  | 260   | 110   | 195   | 45  | 115   | 45  | 135  | 600   | 20  | 25  | 665   | 190   |
| Initial Q (Qb), veh  | 0   | 0   | 0   | 0   | 0   | 0   | 0  | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 0.98  | 1.00  |   | 0.98  | 1.00   |   | 0.99  | 1.00  |   | 0.97  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   | No  |   |  | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1826  | 1826  | 1826  | 1856  | 1856  | 1856  | 1870   | 1870  | 1870  | 1856  | 1856  | 1856  |
| Adj Flow Rate, veh/h   | 260   | 110   | 195   | 45  | 115   | 45  | 135  | 600   | 20  | 25  | 665   | 190   |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 5   | 5   | 5   | 3   | 3   | 3   | 2  | 2   | 2   | 3   | 3   | 3   |
| Cap, veh/h   | 310   | 142   | 251   | 150   | 189   | 74  | 222  | 1358  | 45  | 89  | 840   | 240   |
| Arrive On Green  | 0.18  | 0.24  | 0.24  | 0.09  | 0.15  | 0.15  | 0.12   | 0.39  | 0.39  | 0.05  | 0.31  | 0.31  |
| Sat Flow, veh/h  | 1739  | 584   | 1035  | 1767  | 1261  | 493   | 1781   | 3509  | 117   | 1767  | 2688  | 767   |
| Grp Volume(v), veh/h   | 260   | 0   | 305   | 45  | 0   | 160   | 135  | 304   | 316   | 25  | 436   | 419   |
| Grp Sat Flow(s),veh/h/ln   | 1739  | 0   | 1619  | 1767  | 0   | 1754  | 1781   | 1777  | 1849  | 1767  | 1763  | 1692  |
| Q Serve(g_s), s  | 9.5   | 0.0   | 11.6  | 1.6   | 0.0   | 5.6   | 4.7  | 8.3   | 8.3   | 0.9   | 14.9  | 14.9  |
| Cycle Q Clear(g_c), s  | 9.5   | 0.0   | 11.6  | 1.6   | 0.0   | 5.6   | 4.7  | 8.3   | 8.3   | 0.9   | 14.9  | 14.9  |
| Prop In Lane   | 1.00  |   | 0.64  | 1.00  |   | 0.28  | 1.00   |   | 0.06  | 1.00  |   | 0.45  |
| Lane Grp Cap(c), veh/h   | 310   | 0   | 393   | 150   | 0   | 262   | 222  | 688   | 716   | 89  | 551   | 529   |
| V/C Ratio(X)   | 0.84  | 0.00  | 0.78  | 0.30  | 0.00  | 0.61  | 0.61   | 0.44  | 0.44  | 0.28  | 0.79  | 0.79  |
| Avail Cap(c_a), veh/h  | 698   | 0   | 641   | 710   | 0   | 705   | 715  | 953   | 992   | 710   | 946   | 908   |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 1.00  | 1.00   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Uniform Delay (d), s/veh   | 26.2  | 0.0   | 23.3  | 28.3  | 0.0   | 26.3  | 27.3   | 14.9  | 14.9  | 30.2  | 20.7  | 20.7  |
| Incr Delay (d2), s/veh   | 2.3   | 0.0   | 1.3   | 0.4   | 0.0   | 0.9   | 1.0  | 0.2   | 0.2   | 0.6   | 1.0   | 1.0   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0  | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 3.9   | 0.0   | 4.3   | 0.7   | 0.0   | 2.3   | 1.9  | 2.9   | 3.0   | 0.4   | 5.8   | 5.6   |
| Unsig. Movement Delay, s/veh   |   |   |   |   |   |   |  |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 28.5  | 0.0   | 24.6  | 28.7  | 0.0   | 27.1  | 28.3   | 15.1  | 15.1  | 30.8  | 21.7  | 21.8  |
| LnGrp LOS  | C   |   | C   | C   |   | C   | C  | B   | B   | C   | C   | C   |
| Approach Vol, veh/h  |   | 565   |   |   | 205   |   |  | 755   |   |   | 880   |   |
| Approach Delay, s/veh  |   | 26.4  |   |   | 27.5  |   |  | 17.5  |   |   | 22.0  |   |
| Approach LOS   |   | C   |   |   | C   |   |  | B   |   |   | C   |   |
| Timer - Assigned Phs   | 1   | 2   | 3   | 4   | 5   | 6   | 7  | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s   | 15.3  | 13.8  | 11.7  | 25.2  | 9.1   | 19.9  | 6.8  | 30.1  |   |   |   |   |
| Change Period (Y+Rc), s  | 3.5   | * 3.9   | 3.5   | * 4.6   | 3.5   | 3.9   | 3.5  | * 4.6   |   |   |   |   |
| Max Green Setting (Gmax), s  | 26.5  | * 27  | 26.5  | * 35  | 26.5  | 26.1  | 26.5   | * 35  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s   | 11.5  | 7.6   | 6.7   | 16.9  | 3.6   | 13.6  | 2.9  | 10.3  |   |   |   |   |
| Green Ext Time (p_c), s  | 0.3   | 0.5   | 0.1   | 3.6   | 0.0   | 1.0   | 0.0  | 2.2   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |  |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   |   |   | 22.1  |   |   |   |  |   |   |   |   |   |
| HCM 7th LOS  |   |   | C   |   |   |   |  |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |  |   |   |   |   |   |
| * HCM 7th computational engine requires equal clearance times for the phases crossing the barrier. |   |   |   |   |   |   |  |   |   |   |   |   |

# HCM 7th Signalized Intersection Summary

## 33: Norwood Avenue & Morey Avenue

Future No Build AM

|                              |  |  |  |  |  |  |   |  |  |  |  |  |
|------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement                     | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations          |   |  |   |   |  |   |  |  |   |  |  |   |
| Traffic Volume (veh/h)       | 90  | 1   | 45  | 5   | 1   | 5   | 23  | 881   | 1   | 1   | 1004  | 45  |
| Future Volume (veh/h)        | 90  | 1   | 45  | 5   | 1   | 5   | 23  | 881   | 1   | 1   | 1004  | 45  |
| Initial Q (Qb), veh          | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.              | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)          | 1.00  |   | 1.00  | 1.00  |   | 1.00  | 1.00  |   | 1.00  | 1.00  |   | 1.00  |
| Parking Bus, Adj             | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach        |   | No  |   |   | No  |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln       | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  |
| Adj Flow Rate, veh/h         | 98  | 1   | 49  | 5   | 1   | 5   | 25  | 958   | 1   | 1   | 1091  | 49  |
| Peak Hour Factor             | 0.92  | 0.92  | 0.92  | 0.92  | 0.92  | 0.92  | 0.92  | 0.92  | 0.92  | 0.92  | 0.92  | 0.92  |
| Percent Heavy Veh, %         | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   |
| Cap, veh/h                   | 136   | 1   | 68  | 11  | 2   | 11  | 52  | 1825  | 2   | 4   | 1638  | 74  |
| Arrive On Green              | 0.12  | 0.12  | 0.12  | 0.01  | 0.01  | 0.01  | 0.03  | 0.50  | 0.50  | 0.00  | 0.47  | 0.47  |
| Sat Flow, veh/h              | 1133  | 12  | 567   | 770   | 154   | 770   | 1781  | 3643  | 4   | 1781  | 3464  | 156   |
| Grp Volume(v), veh/h         | 148   | 0   | 0   | 11  | 0   | 0   | 25  | 467   | 492   | 1   | 560   | 580   |
| Grp Sat Flow(s),veh/h/ln     | 1712  | 0   | 0   | 1693  | 0   | 0   | 1781  | 1777  | 1870  | 1781  | 1777  | 1842  |
| Q Serve(g_s), s              | 4.1   | 0.0   | 0.0   | 0.3   | 0.0   | 0.0   | 0.7   | 8.8   | 8.8   | 0.0   | 12.0  | 12.0  |
| Cycle Q Clear(g_c), s        | 4.1   | 0.0   | 0.0   | 0.3   | 0.0   | 0.0   | 0.7   | 8.8   | 8.8   | 0.0   | 12.0  | 12.0  |
| Prop In Lane                 | 0.66  |   | 0.33  | 0.45  |   | 0.45  | 1.00  |   | 0.00  | 1.00  |   | 0.08  |
| Lane Grp Cap(c), veh/h       | 206   | 0   | 0   | 24  | 0   | 0   | 52  | 890   | 936   | 4   | 840   | 871   |
| V/C Ratio(X)                 | 0.72  | 0.00  | 0.00  | 0.46  | 0.00  | 0.00  | 0.48  | 0.53  | 0.53  | 0.28  | 0.67  | 0.67  |
| Avail Cap(c_a), veh/h        | 867   | 0   | 0   | 854   | 0   | 0   | 183   | 1681  | 1769  | 180   | 1678  | 1740  |
| HCM Platoon Ratio            | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)           | 1.00  | 0.00  | 0.00  | 1.00  | 0.00  | 0.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Uniform Delay (d), s/veh     | 21.0  | 0.0   | 0.0   | 24.2  | 0.0   | 0.0   | 23.7  | 8.4   | 8.4   | 24.7  | 10.1  | 10.1  |
| Incr Delay (d2), s/veh       | 4.6   | 0.0   | 0.0   | 13.0  | 0.0   | 0.0   | 6.6   | 0.5   | 0.5   | 37.4  | 0.9   | 0.9   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln     | 1.8   | 0.0   | 0.0   | 0.2   | 0.0   | 0.0   | 0.4   | 2.4   | 2.5   | 0.0   | 3.8   | 3.9   |
| Unsig. Movement Delay, s/veh |   |   |   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh        | 25.6  | 0.0   | 0.0   | 37.2  | 0.0   | 0.0   | 30.3  | 8.9   | 8.8   | 62.1  | 11.0  | 10.9  |
| LnGrp LOS                    | C   |   |   | D   |   |   | C   | A   | A   | E   | B   | B   |
| Approach Vol, veh/h          |   | 148   |   |   | 11  |   |   | 984   |   |   | 1141  |   |
| Approach Delay, s/veh        |   | 25.6  |   |   | 37.2  |   |   | 9.4   |   |   | 11.0  |   |
| Approach LOS                 |   | C   |   |   | D   |   |   | A   |   |   | B   |   |
| Timer - Assigned Phs         | 1   | 2   |   | 4   | 5   | 6   |   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s     | 4.6   | 29.3  |   | 10.5  | 6.0   | 27.9  |   | 5.2   |   |   |   |   |
| Change Period (Y+Rc), s      | 4.5   | 4.5   |   | 4.5   | 4.5   | 4.5   |   | 4.5   |   |   |   |   |
| Max Green Setting (Gmax), s  | 5.0   | 46.9  |   | 25.1  | 5.1   | 46.8  |   | 25.0  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s | 2.0   | 10.8  |   | 6.1   | 2.7   | 14.0  |   | 2.3   |   |   |   |   |
| Green Ext Time (p_c), s      | 0.0   | 6.7   |   | 0.7   | 0.0   | 9.4   |   | 0.0   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh |   |   | 11.4  |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS                  |   |   | B   |   |   |   |   |   |   |   |   |   |

Queues

1: Norwood Avenue & Bell Avenue

Future No Build AM



| Lane Group              | EBL  | EBT  | WBL  | WBT  | WBR  | NBL  | NBT  | NBR  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 60   | 305  | 220  | 90   | 155  | 70   | 515  | 250  | 145  | 680  |
| v/c Ratio               | 0.12 | 0.73 | 0.65 | 0.26 | 0.38 | 0.33 | 0.64 | 0.46 | 0.54 | 0.63 |
| Control Delay (s/veh)   | 27.7 | 42.7 | 48.4 | 45.0 | 10.3 | 50.6 | 39.0 | 7.8  | 49.6 | 34.0 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 27.7 | 42.7 | 48.4 | 45.0 | 10.3 | 50.6 | 39.0 | 7.8  | 49.6 | 34.0 |
| Queue Length 50th (ft)  | 24   | 147  | 118  | 50   | 0    | 38   | 141  | 0    | 80   | 186  |
| Queue Length 95th (ft)  | 73   | 309  | 261  | 120  | 60   | 106  | 267  | 69   | 184  | 331  |
| Internal Link Dist (ft) |      | 878  |      | 976  |      |      | 1238 |      |      | 453  |
| Turn Bay Length (ft)    | 150  |      | 195  |      | 200  | 75   |      | 200  | 95   |      |
| Base Capacity (vph)     | 610  | 880  | 510  | 931  | 849  | 519  | 1787 | 896  | 513  | 1767 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.10 | 0.35 | 0.43 | 0.10 | 0.18 | 0.13 | 0.29 | 0.28 | 0.28 | 0.38 |

Intersection Summary

Queues

2: Norwood Avenue & Jessie Avenue

Future No Build AM



| Lane Group              | EBT  | EBR  | WBT  | NBL  | NBT  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 145  | 215  | 320  | 140  | 815  | 55   | 980  |
| v/c Ratio               | 0.60 | 0.54 | 0.79 | 0.63 | 0.54 | 0.35 | 0.75 |
| Control Delay (s/veh)   | 60.2 | 12.0 | 57.2 | 63.7 | 27.2 | 62.0 | 37.5 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 60.2 | 12.0 | 57.2 | 63.7 | 27.2 | 62.0 | 37.5 |
| Queue Length 50th (ft)  | 103  | 0    | 220  | 100  | 225  | 39   | 316  |
| Queue Length 95th (ft)  | 196  | 73   | 381  | 195  | 388  | 95   | #550 |
| Internal Link Dist (ft) | 758  |      | 547  |      | 632  |      | 1238 |
| Turn Bay Length (ft)    |      | 100  |      | 100  |      | 120  |      |
| Base Capacity (vph)     | 610  | 671  | 581  | 423  | 1534 | 423  | 1442 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.24 | 0.32 | 0.55 | 0.33 | 0.53 | 0.13 | 0.68 |

Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.  
 Queue shown is maximum after two cycles.

Queues

3: Norwood Avenue & WB 80 On-Ramp/WB 80 Off-Ramp

Future No Build AM



| Lane Group              | WBL  | WBT  | WBR  | NBL  | NBT  | SBT  | SBR  |
|-------------------------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 178  | 177  | 240  | 315  | 845  | 855  | 560  |
| v/c Ratio               | 0.56 | 0.56 | 0.56 | 0.72 | 0.36 | 0.63 | 0.76 |
| Control Delay (s/veh)   | 37.5 | 37.3 | 16.4 | 38.2 | 5.8  | 22.8 | 20.6 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.1  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 37.5 | 37.3 | 16.4 | 38.2 | 5.9  | 22.8 | 20.6 |
| Queue Length 50th (ft)  | 86   | 85   | 32   | 143  | 70   | 167  | 126  |
| Queue Length 95th (ft)  | 167  | 166  | 108  | 274  | 146  | 307  | #356 |
| Internal Link Dist (ft) |      | 874  |      |      | 446  | 632  |      |
| Turn Bay Length (ft)    |      |      | 50   | 175  |      |      | 75   |
| Base Capacity (vph)     | 834  | 837  | 856  | 646  | 2929 | 1750 | 883  |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 700  | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.21 | 0.21 | 0.28 | 0.49 | 0.38 | 0.49 | 0.63 |

Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.  
 Queue shown is maximum after two cycles.

Queues

4: Norwood Avenue & EB 80 Off-Ramp/EB 80 On-Ramp

Future No Build AM



| Lane Group              | EBL  | EBT  | EBR  | NBT  | NBR  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 194  | 191  | 510  | 780  | 300  | 385  | 820  |
| v/c Ratio               | 0.40 | 0.39 | 0.89 | 0.76 | 0.45 | 0.84 | 0.39 |
| Control Delay (s/veh)   | 29.8 | 29.6 | 40.1 | 35.9 | 5.7  | 53.2 | 11.1 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 29.8 | 29.6 | 40.1 | 35.9 | 5.7  | 53.2 | 11.1 |
| Queue Length 50th (ft)  | 101  | 98   | 210  | 238  | 0    | 234  | 137  |
| Queue Length 95th (ft)  | 177  | 174  | #420 | 323  | 61   | #448 | 194  |
| Internal Link Dist (ft) |      | 679  |      | 657  |      |      | 446  |
| Turn Bay Length (ft)    |      |      | 50   |      | 220  | 180  |      |
| Base Capacity (vph)     | 662  | 665  | 718  | 1376 | 782  | 518  | 2502 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.29 | 0.29 | 0.71 | 0.57 | 0.38 | 0.74 | 0.33 |

Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.  
 Queue shown is maximum after two cycles.

Queues

5: Norwood Avenue & Harris Avenue

Future No Build AM



| Lane Group              | EBT  | EBR  | WBT  | WBR  | NBL  | NBT  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 170  | 50   | 45   | 100  | 45   | 855  | 60   | 1295 |
| v/c Ratio               | 0.61 | 0.11 | 0.19 | 0.35 | 0.21 | 0.56 | 0.31 | 0.90 |
| Control Delay (s/veh)   | 42.5 | 6.4  | 38.3 | 12.2 | 39.7 | 21.3 | 42.3 | 34.6 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 42.5 | 6.4  | 38.3 | 12.2 | 39.7 | 21.3 | 42.3 | 34.6 |
| Queue Length 50th (ft)  | 87   | 0    | 22   | 0    | 22   | 176  | 30   | 332  |
| Queue Length 95th (ft)  | 150  | 23   | 60   | 47   | 60   | 298  | 74   | #592 |
| Internal Link Dist (ft) | 655  |      | 515  |      |      | 251  |      | 657  |
| Turn Bay Length (ft)    |      | 140  |      |      | 85   |      | 110  |      |
| Base Capacity (vph)     | 703  | 891  | 774  | 717  | 776  | 1526 | 761  | 1432 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.24 | 0.06 | 0.06 | 0.14 | 0.06 | 0.56 | 0.08 | 0.90 |

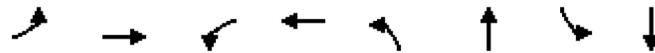
Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.  
 Queue shown is maximum after two cycles.

Queues

6: Norwood Avenue & Silver Eagle Road

Future No Build AM



| Lane Group              | EBL  | EBT  | WBL  | WBT  | NBL  | NBT  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 260  | 305  | 45   | 160  | 135  | 620  | 25   | 855  |
| v/c Ratio               | 0.73 | 0.54 | 0.22 | 0.56 | 0.55 | 0.39 | 0.14 | 0.78 |
| Control Delay (s/veh)   | 48.6 | 27.2 | 47.0 | 43.2 | 49.4 | 19.7 | 47.6 | 34.1 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 48.6 | 27.2 | 47.0 | 43.2 | 49.4 | 19.7 | 47.6 | 34.1 |
| Queue Length 50th (ft)  | 138  | 128  | 24   | 79   | 73   | 102  | 13   | 214  |
| Queue Length 95th (ft)  | 280  | 243  | 72   | 168  | 162  | 243  | 48   | 398  |
| Internal Link Dist (ft) |      | 710  |      | 228  |      | 480  |      | 903  |
| Turn Bay Length (ft)    | 110  |      |      |      | 95   |      | 55   |      |
| Base Capacity (vph)     | 526  | 585  | 537  | 548  | 542  | 1646 | 537  | 1395 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.49 | 0.52 | 0.08 | 0.29 | 0.25 | 0.38 | 0.05 | 0.61 |

Intersection Summary

Queues

33: Norwood Avenue & Morey Avenue

Future No Build AM



| Lane Group              | EBT  | WBT  | NBL  | NBT  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 148  | 11   | 25   | 959  | 1    | 1140 |
| v/c Ratio               | 0.44 | 0.06 | 0.16 | 0.45 | 0.01 | 0.56 |
| Control Delay (s/veh)   | 26.5 | 27.4 | 35.9 | 8.8  | 36.0 | 11.3 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 26.5 | 27.4 | 35.9 | 8.8  | 36.0 | 11.3 |
| Queue Length 50th (ft)  | 33   | 2    | 7    | 67   | 0    | 86   |
| Queue Length 95th (ft)  | 129  | 21   | 41   | 254  | 6    | 322  |
| Internal Link Dist (ft) | 329  | 438  |      | 256  |      | 304  |
| Turn Bay Length (ft)    |      |      | 100  |      | 50   |      |
| Base Capacity (vph)     | 776  | 760  | 159  | 2938 | 156  | 2916 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.19 | 0.01 | 0.16 | 0.33 | 0.01 | 0.39 |
| Intersection Summary    |      |      |      |      |      |      |

# HCM 7th Signalized Intersection Summary

## 1: Norwood Avenue & Bell Avenue

Future No Build PM

|  |  |  |  |  |  |  |  |  |  |  |  |  |
|--|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |  |  |   |  |  |  |  |  |  |  |  |  |
| Traffic Volume (veh/h)   | 15  | 90  | 115   | 300   | 115   | 130   | 130   | 445   | 335   | 130   | 610   | 20  |
| Future Volume (veh/h)  | 15  | 90  | 115   | 300   | 115   | 130   | 130   | 445   | 335   | 130   | 610   | 20  |
| Initial Q (Qb), veh  | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 0.98  | 1.00  |   | 0.97  | 1.00  |   | 0.97  | 1.00  |   | 0.97  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   | No  |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1885  | 1885  | 1885  | 1870  | 1870  | 1870  | 1885  | 1885  | 1885  | 1885  | 1885  | 1885  |
| Adj Flow Rate, veh/h   | 15  | 90  | 115   | 300   | 115   | 130   | 130   | 445   | 335   | 130   | 610   | 20  |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 1   | 1   | 1   | 2   | 2   | 2   | 1   | 1   | 1   | 1   | 1   | 1   |
| Cap, veh/h   | 376   | 125   | 159   | 353   | 271   | 224   | 253   | 767   | 333   | 278   | 823   | 27  |
| Arrive On Green  | 0.21  | 0.17  | 0.17  | 0.20  | 0.14  | 0.14  | 0.14  | 0.21  | 0.21  | 0.15  | 0.23  | 0.23  |
| Sat Flow, veh/h  | 1795  | 741   | 947   | 1781  | 1870  | 1544  | 1795  | 3582  | 1557  | 1795  | 3536  | 116   |
| Grp Volume(v), veh/h   | 15  | 0   | 205   | 300   | 115   | 130   | 130   | 445   | 335   | 130   | 309   | 321   |
| Grp Sat Flow(s),veh/h/ln   | 1795  | 0   | 1688  | 1781  | 1870  | 1544  | 1795  | 1791  | 1557  | 1795  | 1791  | 1861  |
| Q Serve(g_s), s  | 0.4   | 0.0   | 7.3   | 10.4  | 3.6   | 3.4   | 4.3   | 7.1   | 7.5   | 4.2   | 10.2  | 10.2  |
| Cycle Q Clear(g_c), s  | 0.4   | 0.0   | 7.3   | 10.4  | 3.6   | 3.4   | 4.3   | 7.1   | 7.5   | 4.2   | 10.2  | 10.2  |
| Prop In Lane   | 1.00  |   | 0.56  | 1.00  |   | 1.00  | 1.00  |   | 1.00  | 1.00  |   | 0.06  |
| Lane Grp Cap(c), veh/h   | 376   | 0   | 284   | 353   | 271   | 224   | 253   | 767   | 333   | 278   | 417   | 433   |
| V/C Ratio(X)   | 0.04  | 0.00  | 0.72  | 0.85  | 0.42  | 0.58  | 0.51  | 0.58  | 1.00  | 0.47  | 0.74  | 0.74  |
| Avail Cap(c_a), veh/h  | 736   | 0   | 1199  | 730   | 1328  | 1097  | 741   | 2543  | 1106  | 733   | 1272  | 1321  |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Uniform Delay (d), s/veh   | 20.2  | 0.0   | 25.2  | 24.7  | 24.9  | 12.0  | 25.4  | 22.5  | 7.6   | 24.6  | 22.7  | 22.7  |
| Incr Delay (d2), s/veh   | 0.0   | 0.0   | 1.3   | 2.2   | 0.4   | 0.9   | 0.6   | 0.3   | 15.1  | 0.5   | 1.0   | 0.9   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 0.2   | 0.0   | 2.9   | 4.1   | 1.5   | 1.7   | 1.7   | 2.7   | 5.3   | 1.7   | 4.1   | 4.3   |
| Unsig. Movement Delay, s/veh   |   |   |   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 20.2  | 0.0   | 26.5  | 26.9  | 25.3  | 12.9  | 26.0  | 22.8  | 22.7  | 25.1  | 23.7  | 23.7  |
| LnGrp LOS  | C   |   | C   | C   | C   | B   | C   | C   | F   | C   | C   | C   |
| Approach Vol, veh/h  |   | 220   |   |   | 545   |   |   | 910   |   |   | 760   |   |
| Approach Delay, s/veh  |   | 26.0  |   |   | 23.2  |   |   | 23.2  |   |   | 23.9  |   |
| Approach LOS   |   | C   |   |   | C   |   |   | C   |   |   | C   |   |
| Timer - Assigned Phs   | 1   | 2   | 3   | 4   | 5   | 6   | 7   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s   | 18.0  | 13.9  | 12.6  | 19.5  | 16.5  | 15.4  | 13.8  | 18.3  |   |   |   |   |
| Change Period (Y+Rc), s  | * 4.6   | * 4.6   | 3.6   | * 4.6   | 3.8   | * 4.6   | 3.9   | * 4.6   |   |   |   |   |
| Max Green Setting (Gmax), s  | * 26  | * 45  | 26.4  | * 45  | 26.2  | * 45  | 26.1  | * 45  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s   | 2.4   | 5.6   | 6.3   | 12.2  | 12.4  | 9.3   | 6.2   | 9.5   |   |   |   |   |
| Green Ext Time (p_c), s  | 0.0   | 0.6   | 0.1   | 2.6   | 0.4   | 0.9   | 0.2   | 2.4   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   |   |   |   | 23.7  |   |   |   |   |   |   |   |   |
| HCM 7th LOS  |   |   |   | C   |   |   |   |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| * HCM 7th computational engine requires equal clearance times for the phases crossing the barrier. |   |   |   |   |   |   |   |   |   |   |   |   |

# HCM 7th Signalized Intersection Summary

## 2: Norwood Avenue & Jessie Avenue

Future No Build PM

|  |  |  |  |  |  |  |   |  |  |  |  |  |
|--|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |   |  |  |   |  |   |  |  |  |  |  |  |
| Traffic Volume (veh/h)   | 35  | 55  | 165   | 235   | 90  | 50  | 215   | 835   | 155   | 100   | 860   | 25  |
| Future Volume (veh/h)  | 35  | 55  | 165   | 235   | 90  | 50  | 215   | 835   | 155   | 100   | 860   | 25  |
| Initial Q (Qb), veh  | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 0.98  | 1.00  |   | 0.98  | 1.00  |   | 0.97  | 1.00  |   | 0.97  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   | No  |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1885  | 1885  | 1885  | 1885  | 1885  | 1885  | 1885  | 1885  | 1885  | 1885  | 1885  | 1885  |
| Adj Flow Rate, veh/h   | 35  | 55  | 165   | 235   | 90  | 50  | 215   | 835   | 155   | 100   | 860   | 25  |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 1   | 1   | 1   | 1   | 1   | 1   | 1   | 1   | 1   | 1   | 1   | 1   |
| Cap, veh/h   | 101   | 159   | 219   | 275   | 105   | 59  | 255   | 1022  | 190   | 172   | 1044  | 30  |
| Arrive On Green  | 0.14  | 0.14  | 0.14  | 0.25  | 0.25  | 0.25  | 0.14  | 0.34  | 0.34  | 0.10  | 0.29  | 0.29  |
| Sat Flow, veh/h  | 719   | 1130  | 1559  | 1115  | 427   | 237   | 1795  | 3001  | 557   | 1795  | 3551  | 103   |
| Grp Volume(v), veh/h   | 90  | 0   | 165   | 375   | 0   | 0   | 215   | 498   | 492   | 100   | 434   | 451   |
| Grp Sat Flow(s),veh/h/ln   | 1849  | 0   | 1559  | 1780  | 0   | 0   | 1795  | 1791  | 1767  | 1795  | 1791  | 1863  |
| Q Serve(g_s), s  | 3.8   | 0.0   | 8.7   | 17.2  | 0.0   | 0.0   | 10.0  | 21.7  | 21.7  | 4.6   | 19.3  | 19.3  |
| Cycle Q Clear(g_c), s  | 3.8   | 0.0   | 8.7   | 17.2  | 0.0   | 0.0   | 10.0  | 21.7  | 21.7  | 4.6   | 19.3  | 19.3  |
| Prop In Lane   | 0.39  |   | 1.00  | 0.63  |   | 0.13  | 1.00  |   | 0.32  | 1.00  |   | 0.06  |
| Lane Grp Cap(c), veh/h   | 260   | 0   | 219   | 439   | 0   | 0   | 255   | 610   | 602   | 172   | 527   | 548   |
| V/C Ratio(X)   | 0.35  | 0.00  | 0.75  | 0.85  | 0.00  | 0.00  | 0.84  | 0.82  | 0.82  | 0.58  | 0.82  | 0.82  |
| Avail Cap(c_a), veh/h  | 790   | 0   | 666   | 760   | 0   | 0   | 557   | 952   | 939   | 557   | 952   | 990   |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 0.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Uniform Delay (d), s/veh   | 33.2  | 0.0   | 35.3  | 30.7  | 0.0   | 0.0   | 35.7  | 25.7  | 25.7  | 37.0  | 28.1  | 28.1  |
| Incr Delay (d2), s/veh   | 0.3   | 0.0   | 2.0   | 1.9   | 0.0   | 0.0   | 2.9   | 1.6   | 1.6   | 1.2   | 1.3   | 1.2   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 1.7   | 0.0   | 3.3   | 7.4   | 0.0   | 0.0   | 4.4   | 8.8   | 8.7   | 2.0   | 8.1   | 8.4   |
| Unsig. Movement Delay, s/veh   |   |   |   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 33.5  | 0.0   | 37.3  | 32.6  | 0.0   | 0.0   | 38.6  | 27.3  | 27.4  | 38.2  | 29.4  | 29.3  |
| LnGrp LOS  | C   |   | D   | C   |   |   | D   | C   | C   | D   | C   | C   |
| Approach Vol, veh/h  |   | 255   |   |   | 375   |   |   | 1205  |   |   | 985   |   |
| Approach Delay, s/veh  |   | 35.9  |   |   | 32.6  |   |   | 29.4  |   |   | 30.2  |   |
| Approach LOS   |   | D   |   |   | C   |   |   | C   |   |   | C   |   |
| Timer - Assigned Phs   |   | 2   | 3   | 4   |   | 6   | 7   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s   |   | 24.6  | 15.6  | 29.7  |   | 15.5  | 11.7  | 33.7  |   |   |   |   |
| Change Period (Y+Rc), s  |   | 3.5   | 3.5   | * 4.6   |   | 3.5   | 3.5   | * 4.6   |   |   |   |   |
| Max Green Setting (Gmax), s  |   | 36.5  | 26.5  | * 45  |   | 36.5  | 26.5  | * 45  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s   |   | 19.2  | 12.0  | 21.3  |   | 10.7  | 6.6   | 23.7  |   |   |   |   |
| Green Ext Time (p_c), s  |   | 1.4   | 0.2   | 3.8   |   | 0.6   | 0.1   | 3.9   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   |   |   | 30.7  |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS  |   |   | C   |   |   |   |   |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| * HCM 7th computational engine requires equal clearance times for the phases crossing the barrier. |   |   |   |   |   |   |   |   |   |   |   |   |

# HCM 7th Signalized Intersection Summary

## 3: Norwood Avenue & WB 80 On-Ramp/WB 80 Off-Ramp

Future No Build PM

|   |  |  |  |  |  |  |  |  |  |  |  |  |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement  | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations   |   |   |   |  |  |  |  |  |   |   |  |  |
| Traffic Volume (veh/h)  | 0   | 0   | 0   | 320   | 0   | 350   | 435   | 970   | 0   | 0   | 765   | 550   |
| Future Volume (veh/h)   | 0   | 0   | 0   | 320   | 0   | 350   | 435   | 970   | 0   | 0   | 765   | 550   |
| Initial Q (Qb), veh   |   |   |   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.   |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)   |   |   |   | 1.00  |   | 1.00  | 1.00  |   | 1.00  | 1.00  |   | 1.00  |
| Parking Bus, Adj  |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach   |   |   |   | No  | No  | No  | No  | No  | No  | No  | No  | No  |
| Adj Sat Flow, veh/h/ln  |   |   |   | 1885  | 1885  | 1885  | 1885  | 1885  | 0   | 0   | 1885  | 1885  |
| Adj Flow Rate, veh/h  |   |   |   | 320   | 0   | 0   | 435   | 970   | 0   | 0   | 765   | 0   |
| Peak Hour Factor  |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %  |   |   |   | 1   | 1   | 1   | 1   | 1   | 0   | 0   | 1   | 1   |
| Cap, veh/h  |   |   |   | 579   | 0   |   | 509   | 2390  | 0   | 0   | 1131  |   |
| Arrive On Green   |   |   |   | 0.16  | 0.00  | 0.00  | 0.28  | 0.67  | 0.00  | 0.00  | 0.32  | 0.00  |
| Sat Flow, veh/h   |   |   |   | 3591  | 0   | 1598  | 1795  | 3676  | 0   | 0   | 3676  | 1598  |
| Grp Volume(v), veh/h  |   |   |   | 320   | 0   | 0   | 435   | 970   | 0   | 0   | 765   | 0   |
| Grp Sat Flow(s),veh/h/ln  |   |   |   | 1795  | 0   | 1598  | 1795  | 1791  | 0   | 0   | 1791  | 1598  |
| Q Serve(g_s), s   |   |   |   | 4.2   | 0.0   | 0.0   | 11.8  | 6.3   | 0.0   | 0.0   | 9.5   | 0.0   |
| Cycle Q Clear(g_c), s   |   |   |   | 4.2   | 0.0   | 0.0   | 11.8  | 6.3   | 0.0   | 0.0   | 9.5   | 0.0   |
| Prop In Lane  |   |   |   | 1.00  |   | 1.00  | 1.00  |   | 0.00  | 0.00  |   | 1.00  |
| Lane Grp Cap(c), veh/h  |   |   |   | 579   | 0   |   | 509   | 2390  | 0   | 0   | 1131  |   |
| V/C Ratio(X)  |   |   |   | 0.55  | 0.00  |   | 0.86  | 0.41  | 0.00  | 0.00  | 0.68  |   |
| Avail Cap(c_a), veh/h   |   |   |   | 2517  | 0   |   | 927   | 2455  | 0   | 0   | 2455  |   |
| HCM Platoon Ratio   |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)  |   |   |   | 1.00  | 0.00  | 0.00  | 1.00  | 1.00  | 0.00  | 0.00  | 1.00  | 0.00  |
| Uniform Delay (d), s/veh  |   |   |   | 19.8  | 0.0   | 0.0   | 17.4  | 3.9   | 0.0   | 0.0   | 15.3  | 0.0   |
| Incr Delay (d2), s/veh  |   |   |   | 0.3   | 0.0   | 0.0   | 3.2   | 0.1   | 0.0   | 0.0   | 0.5   | 0.0   |
| Initial Q Delay(d3), s/veh  |   |   |   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln  |   |   |   | 1.6   | 0.0   | 0.0   | 4.4   | 0.9   | 0.0   | 0.0   | 3.4   | 0.0   |
| Unsig. Movement Delay, s/veh  |   |   |   |   |   | 38.50   |   |   |   |   |   | 32.30   |
| LnGrp Delay(d), s/veh   |   |   |   | 20.1  | 0.0   | 38.5  | 20.6  | 4.0   | 0.0   | 0.0   | 15.8  | 32.3  |
| LnGrp LOS   |   |   |   | C   |   | D   | C   | A   |   |   | B   | C   |
| Approach Vol, veh/h   |   |   |   |   | 495   |   |   | 1405  |   |   | 1040  |   |
| Approach Delay, s/veh   |   |   |   |   | 26.6  |   |   | 9.1   |   |   | 20.2  |   |
| Approach LOS  |   |   |   |   | C   |   |   | A   |   |   | C   |   |
| Timer - Assigned Phs  | 1   | 2   |   | 4   |   | 6   |   |   |   |   |   |   |
| Phs Duration (G+Y+Rc), s  | 18.1  | 21.0  |   | 12.3  |   | 39.1  |   |   |   |   |   |   |
| Change Period (Y+Rc), s   | 3.5   | 4.8   |   | 4.0   |   | 4.8   |   |   |   |   |   |   |
| Max Green Setting (Gmax), s   | 26.5  | 35.2  |   | 36.0  |   | 35.2  |   |   |   |   |   |   |
| Max Q Clear Time (g_c+I1), s  | 13.8  | 11.5  |   | 6.2   |   | 8.3   |   |   |   |   |   |   |
| Green Ext Time (p_c), s   | 0.8   | 4.7   |   | 0.6   |   | 5.9   |   |   |   |   |   |   |
| <b>Intersection Summary</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh  |   |   |   | 16.0  |   |   |   |   |   |   |   |   |
| HCM 7th LOS   |   |   |   | B   |   |   |   |   |   |   |   |   |
| <b>Notes</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| User approved volume balancing among the lanes for turning movement.  |   |   |   |   |   |   |   |   |   |   |   |   |
| Unsignalized Delay for [WBR, SBR] is included in calculations of the approach delay and intersection delay. |   |   |   |   |   |   |   |   |   |   |   |   |

# HCM 7th Signalized Intersection Summary

## 4: Norwood Avenue & EB 80 Off-Ramp/EB 80 On-Ramp

Future No Build PM

|  |  |  |  |  |  |  |  |  |  |  |  |  |
|--|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |  |  |  |   |   |   |   |  |  |  |  |  |
| Traffic Volume (veh/h)   | 520   | 15  | 465   | 0   | 0   | 0   | 0   | 885   | 325   | 330   | 755   | 0   |
| Future Volume (veh/h)  | 520   | 15  | 465   | 0   | 0   | 0   | 0   | 885   | 325   | 330   | 755   | 0   |
| Initial Q (Qb), veh  | 0   | 0   | 0   |   |   |   |   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 1.00  |   |   |   | 1.00  |   | 1.00  | 1.00  |   | 1.00  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   |   |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1856  | 1856  | 1856  |   |   |   | 0   | 1870  | 1870  | 1885  | 1885  | 0   |
| Adj Flow Rate, veh/h   | 531   | 0   | 0   |   |   |   | 0   | 885   | 0   | 330   | 755   | 0   |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 3   | 3   | 3   |   |   |   | 0   | 2   | 2   | 1   | 1   | 0   |
| Cap, veh/h   | 708   | 0   |   |   |   |   | 0   | 1232  |   | 400   | 2274  | 0   |
| Arrive On Green  | 0.20  | 0.00  | 0.00  |   |   |   | 0.00  | 0.35  | 0.00  | 0.22  | 0.63  | 0.00  |
| Sat Flow, veh/h  | 3534  | 0   | 1572  |   |   |   | 0   | 3647  | 1585  | 1795  | 3676  | 0   |
| Grp Volume(v), veh/h   | 531   | 0   | 0   |   |   |   | 0   | 885   | 0   | 330   | 755   | 0   |
| Grp Sat Flow(s),veh/h/ln   | 1767  | 0   | 1572  |   |   |   | 0   | 1777  | 1585  | 1795  | 1791  | 0   |
| Q Serve(g_s), s  | 7.6   | 0.0   | 0.0   |   |   |   | 0.0   | 11.6  | 0.0   | 9.3   | 5.2   | 0.0   |
| Cycle Q Clear(g_c), s  | 7.6   | 0.0   | 0.0   |   |   |   | 0.0   | 11.6  | 0.0   | 9.3   | 5.2   | 0.0   |
| Prop In Lane   | 1.00  |   | 1.00  |   |   |   | 0.00  |   | 1.00  | 1.00  |   | 0.00  |
| Lane Grp Cap(c), veh/h   | 708   | 0   |   |   |   |   | 0   | 1232  |   | 400   | 2274  | 0   |
| V/C Ratio(X)   | 0.75  | 0.00  |   |   |   |   | 0.00  | 0.72  |   | 0.82  | 0.33  | 0.00  |
| Avail Cap(c_a), veh/h  | 2382  | 0   |   |   |   |   | 0   | 2342  |   | 891   | 2361  | 0   |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 0.00  |   |   |   | 0.00  | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  |
| Uniform Delay (d), s/veh   | 20.1  | 0.0   | 0.0   |   |   |   | 0.0   | 15.2  | 0.0   | 19.8  | 4.5   | 0.0   |
| Incr Delay (d2), s/veh   | 0.6   | 0.0   | 0.0   |   |   |   | 0.0   | 0.6   | 0.0   | 3.3   | 0.1   | 0.0   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   |   |   |   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 2.9   | 0.0   | 0.0   |   |   |   | 0.0   | 3.8   | 0.0   | 3.9   | 1.2   | 0.0   |
| Unsig. Movement Delay, s/veh   |   |   | 33.50   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 20.7  | 0.0   | 33.5  |   |   |   | 0.0   | 15.8  | 0.0   | 23.0  | 4.6   | 0.0   |
| LnGrp LOS  | C   |   | C   |   |   |   |   | B   |   | C   | A   |   |
| Approach Vol, veh/h  |   | 761   |   |   |   |   |   | 885   |   |   | 1085  |   |
| Approach Delay, s/veh  |   | 24.6  |   |   |   |   |   | 15.8  |   |   | 10.2  |   |
| Approach LOS   |   | C   |   |   |   |   |   | B   |   |   | B   |   |
| Timer - Assigned Phs   |   | 2   |   |   | 5   | 6   |   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s   |   | 38.7  |   |   | 15.4  | 23.3  |   | 14.7  |   |   |   |   |
| Change Period (Y+Rc), s  |   | 4.8   |   |   | 3.5   | 4.8   |   | 4.0   |   |   |   |   |
| Max Green Setting (Gmax), s  |   | 35.2  |   |   | 26.5  | 35.2  |   | 36.0  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s   |   | 7.2   |   |   | 11.3  | 13.6  |   | 9.6   |   |   |   |   |
| Green Ext Time (p_c), s  |   | 4.8   |   |   | 0.6   | 4.9   |   | 1.0   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   |   |   | 16.0  |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS  |   |   | B   |   |   |   |   |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| User approved volume balancing among the lanes for turning movement.                                   |   |   |   |   |   |   |   |   |   |   |   |   |
| Unsignalized Delay for [EBR] is included in calculations of the approach delay and intersection delay. |   |   |   |   |   |   |   |   |   |   |   |   |

Unsignalized Delay for [NBR] is excluded from calculations of the approach delay and intersection delay.

# HCM 7th Signalized Intersection Summary

## 5: Norwood Avenue & Harris Avenue

Future No Build PM

|  |  |  |  |  |  |  |   |  |  |  |  |  |
|--|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |   |  |  |   |  |  |  |  |  |  |  |  |
| Traffic Volume (veh/h)   | 230   | 15  | 45  | 20  | 10  | 95  | 30  | 965   | 25  | 70  | 1035  | 140   |
| Future Volume (veh/h)  | 230   | 15  | 45  | 20  | 10  | 95  | 30  | 965   | 25  | 70  | 1035  | 140   |
| Initial Q (Qb), veh  | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 0.98  | 1.00  |   | 0.99  | 1.00  |   | 0.97  | 1.00  |   | 0.97  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   | No  |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1856  | 1856  | 1856  | 1856  | 1856  | 1856  | 1885  | 1885  | 1885  | 1856  | 1856  | 1856  |
| Adj Flow Rate, veh/h   | 230   | 15  | 45  | 20  | 10  | 95  | 30  | 965   | 25  | 70  | 1035  | 140   |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 3   | 3   | 3   | 3   | 3   | 3   | 1   | 1   | 1   | 3   | 3   | 3   |
| Cap, veh/h   | 302   | 20  | 377   | 168   | 84  | 217   | 112   | 1316  | 34  | 166   | 1245  | 168   |
| Arrive On Green  | 0.18  | 0.18  | 0.18  | 0.14  | 0.14  | 0.14  | 0.06  | 0.37  | 0.37  | 0.09  | 0.40  | 0.40  |
| Sat Flow, veh/h  | 1664  | 109   | 1537  | 1197  | 599   | 1549  | 1795  | 3564  | 92  | 1767  | 3107  | 420   |
| Grp Volume(v), veh/h   | 245   | 0   | 45  | 30  | 0   | 95  | 30  | 485   | 505   | 70  | 587   | 588   |
| Grp Sat Flow(s),veh/h/ln   | 1772  | 0   | 1537  | 1796  | 0   | 1549  | 1795  | 1791  | 1865  | 1767  | 1763  | 1764  |
| Q Serve(g_s), s  | 9.5   | 0.0   | 1.6   | 1.1   | 0.0   | 4.0   | 1.1   | 16.9  | 16.9  | 2.7   | 21.5  | 21.6  |
| Cycle Q Clear(g_c), s  | 9.5   | 0.0   | 1.6   | 1.1   | 0.0   | 4.0   | 1.1   | 16.9  | 16.9  | 2.7   | 21.5  | 21.6  |
| Prop In Lane   | 0.94  |   | 1.00  | 0.67  |   | 1.00  | 1.00  |   | 0.05  | 1.00  |   | 0.24  |
| Lane Grp Cap(c), veh/h   | 321   | 0   | 377   | 252   | 0   | 217   | 112   | 661   | 689   | 166   | 706   | 707   |
| V/C Ratio(X)   | 0.76  | 0.00  | 0.12  | 0.12  | 0.00  | 0.44  | 0.27  | 0.73  | 0.73  | 0.42  | 0.83  | 0.83  |
| Avail Cap(c_a), veh/h  | 895   | 0   | 875   | 902   | 0   | 778   | 910   | 880   | 916   | 895   | 866   | 867   |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Uniform Delay (d), s/veh   | 28.0  | 0.0   | 21.2  | 27.1  | 0.0   | 28.4  | 32.2  | 19.7  | 19.7  | 30.8  | 19.4  | 19.4  |
| Incr Delay (d2), s/veh   | 1.4   | 0.0   | 0.1   | 0.1   | 0.0   | 0.5   | 0.5   | 1.8   | 1.7   | 0.6   | 5.4   | 5.4   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 4.0   | 0.0   | 0.6   | 0.4   | 0.0   | 1.4   | 0.5   | 6.5   | 6.8   | 1.1   | 9.1   | 9.1   |
| Unsig. Movement Delay, s/veh   |   |   |   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 29.4  | 0.0   | 21.3  | 27.2  | 0.0   | 28.9  | 32.7  | 21.5  | 21.4  | 31.4  | 24.7  | 24.9  |
| LnGrp LOS  | C   |   | C   | C   |   | C   | C   | C   | C   | C   | C   | C   |
| Approach Vol, veh/h  |   | 290   |   |   | 125   |   |   | 1020  |   |   | 1245  |   |
| Approach Delay, s/veh  |   | 28.2  |   |   | 28.5  |   |   | 21.8  |   |   | 25.2  |   |
| Approach LOS   |   | C   |   |   | C   |   |   | C   |   |   | C   |   |
| Timer - Assigned Phs   |   | 2   | 3   | 4   |   | 6   | 7   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s   |   | 13.9  | 8.0   | 33.5  |   | 16.7  | 10.3  | 31.2  |   |   |   |   |
| Change Period (Y+Rc), s  |   | 3.8   | 3.5   | * 4.6   |   | 3.6   | 3.5   | * 4.6   |   |   |   |   |
| Max Green Setting (Gmax), s  |   | 36.2  | 36.5  | * 35  |   | 36.4  | 36.5  | * 35  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s   |   | 6.0   | 3.1   | 23.6  |   | 11.5  | 4.7   | 18.9  |   |   |   |   |
| Green Ext Time (p_c), s  |   | 0.3   | 0.0   | 5.3   |   | 1.0   | 0.1   | 4.5   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   |   |   | 24.4  |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS  |   |   | C   |   |   |   |   |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| * HCM 7th computational engine requires equal clearance times for the phases crossing the barrier. |   |   |   |   |   |   |   |   |   |   |   |   |

HCM 7th Signalized Intersection Summary  
6: Norwood Avenue & Silver Eagle Road

Future No Build PM

|  |  |  |  |  |  |  |  |  |  |  |  |  |
|--|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |  |  |   |  |  |   |  |  |  |  |  |  |
| Traffic Volume (veh/h)   | 280   | 160   | 230   | 15  | 120   | 40  | 190   | 625   | 25  | 45  | 610   | 235   |
| Future Volume (veh/h)  | 280   | 160   | 230   | 15  | 120   | 40  | 190   | 625   | 25  | 45  | 610   | 235   |
| Initial Q (Qb), veh  | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 0.99  | 1.00  |   | 0.99  | 1.00  |   | 0.97  | 1.00  |   | 0.97  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   | No  |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1885  | 1885  | 1885  | 1885  | 1885  | 1885  | 1870  | 1870  | 1870  | 1885  | 1885  | 1885  |
| Adj Flow Rate, veh/h   | 280   | 160   | 230   | 15  | 120   | 40  | 190   | 625   | 25  | 45  | 610   | 235   |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 1   | 1   | 1   | 1   | 1   | 1   | 2   | 2   | 2   | 1   | 1   | 1   |
| Cap, veh/h   | 332   | 202   | 290   | 65  | 192   | 64  | 237   | 1265  | 51  | 137   | 771   | 296   |
| Arrive On Green  | 0.18  | 0.29  | 0.29  | 0.04  | 0.14  | 0.14  | 0.13  | 0.36  | 0.36  | 0.08  | 0.31  | 0.31  |
| Sat Flow, veh/h  | 1795  | 693   | 996   | 1795  | 1348  | 449   | 1781  | 3478  | 139   | 1795  | 2506  | 964   |
| Grp Volume(v), veh/h   | 280   | 0   | 390   | 15  | 0   | 160   | 190   | 319   | 331   | 45  | 436   | 409   |
| Grp Sat Flow(s),veh/h/ln   | 1795  | 0   | 1690  | 1795  | 0   | 1797  | 1781  | 1777  | 1840  | 1795  | 1791  | 1679  |
| Q Serve(g_s), s  | 10.0  | 0.0   | 14.2  | 0.5   | 0.0   | 5.6   | 6.9   | 9.3   | 9.3   | 1.6   | 14.8  | 14.9  |
| Cycle Q Clear(g_c), s  | 10.0  | 0.0   | 14.2  | 0.5   | 0.0   | 5.6   | 6.9   | 9.3   | 9.3   | 1.6   | 14.8  | 14.9  |
| Prop In Lane   | 1.00  |   | 0.59  | 1.00  |   | 0.25  | 1.00  |   | 0.08  | 1.00  |   | 0.57  |
| Lane Grp Cap(c), veh/h   | 332   | 0   | 491   | 65  | 0   | 256   | 237   | 647   | 669   | 137   | 551   | 516   |
| V/C Ratio(X)   | 0.84  | 0.00  | 0.79  | 0.23  | 0.00  | 0.63  | 0.80  | 0.49  | 0.49  | 0.33  | 0.79  | 0.79  |
| Avail Cap(c_a), veh/h  | 714   | 0   | 662   | 714   | 0   | 715   | 708   | 944   | 977   | 714   | 951   | 892   |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Uniform Delay (d), s/veh   | 26.2  | 0.0   | 21.8  | 31.2  | 0.0   | 26.9  | 28.1  | 16.4  | 16.4  | 29.2  | 21.1  | 21.1  |
| Incr Delay (d2), s/veh   | 2.3   | 0.0   | 3.3   | 0.7   | 0.0   | 0.9   | 2.4   | 0.2   | 0.2   | 0.5   | 1.0   | 1.1   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 4.3   | 0.0   | 5.6   | 0.2   | 0.0   | 2.3   | 2.9   | 3.3   | 3.4   | 0.7   | 5.9   | 5.5   |
| Unsig. Movement Delay, s/veh   |   |   |   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 28.5  | 0.0   | 25.1  | 31.9  | 0.0   | 27.8  | 30.5  | 16.7  | 16.6  | 29.7  | 22.1  | 22.2  |
| LnGrp LOS  | C   |   | C   | C   |   | C   | C   | B   | B   | C   | C   | C   |
| Approach Vol, veh/h  |   | 670   |   |   | 175   |   |   | 840   |   |   | 890   |   |
| Approach Delay, s/veh  |   | 26.5  |   |   | 28.2  |   |   | 19.8  |   |   | 22.5  |   |
| Approach LOS   |   | C   |   |   | C   |   |   | B   |   |   | C   |   |
| Timer - Assigned Phs   | 1   | 2   | 3   | 4   | 5   | 6   | 7   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s   | 15.8  | 13.4  | 12.3  | 25.1  | 5.9   | 23.3  | 8.6   | 28.8  |   |   |   |   |
| Change Period (Y+Rc), s  | 3.5   | * 3.9   | 3.5   | * 4.6   | 3.5   | 3.9   | 3.5   | * 4.6   |   |   |   |   |
| Max Green Setting (Gmax), s  | 26.5  | * 27  | 26.5  | * 35  | 26.5  | 26.1  | 26.5  | * 35  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s   | 12.0  | 7.6   | 8.9   | 16.9  | 2.5   | 16.2  | 3.6   | 11.3  |   |   |   |   |
| Green Ext Time (p_c), s  | 0.4   | 0.5   | 0.2   | 3.6   | 0.0   | 1.2   | 0.0   | 2.3   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   |   |   | 23.1  |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS  |   |   | C   |   |   |   |   |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| * HCM 7th computational engine requires equal clearance times for the phases crossing the barrier. |   |   |   |   |   |   |   |   |   |   |   |   |

# HCM 7th Signalized Intersection Summary

## 33: Norwood Avenue & Morey Avenue

Future No Build PM

|                              |  |  |  |  |  |  |   |  |  |  |  |  |
|------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement                     | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations          |   |  |   |   |  |   |  |  |  |  |  |   |
| Traffic Volume (veh/h)       | 45  | 1   | 23  | 5   | 1   | 5   | 45  | 899   | 1   | 1   | 1009  | 90  |
| Future Volume (veh/h)        | 45  | 1   | 23  | 5   | 1   | 5   | 45  | 899   | 1   | 1   | 1009  | 90  |
| Initial Q (Qb), veh          | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.              | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)          | 1.00  |   | 1.00  | 1.00  |   | 1.00  | 1.00  |   | 1.00  | 1.00  |   | 1.00  |
| Parking Bus, Adj             | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach        |   | No  |   |   | No  |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln       | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  |
| Adj Flow Rate, veh/h         | 45  | 1   | 23  | 5   | 1   | 5   | 45  | 899   | 1   | 1   | 1009  | 90  |
| Peak Hour Factor             | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %         | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   |
| Cap, veh/h                   | 72  | 2   | 37  | 11  | 2   | 11  | 85  | 1899  | 2   | 4   | 1567  | 140   |
| Arrive On Green              | 0.06  | 0.06  | 0.06  | 0.01  | 0.01  | 0.01  | 0.05  | 0.52  | 0.52  | 0.00  | 0.47  | 0.47  |
| Sat Flow, veh/h              | 1116  | 25  | 571   | 770   | 154   | 770   | 1781  | 3642  | 4   | 1781  | 3300  | 294   |
| Grp Volume(v), veh/h         | 69  | 0   | 0   | 11  | 0   | 0   | 45  | 439   | 461   | 1   | 543   | 556   |
| Grp Sat Flow(s),veh/h/ln     | 1712  | 0   | 0   | 1693  | 0   | 0   | 1781  | 1777  | 1870  | 1781  | 1777  | 1817  |
| Q Serve(g_s), s              | 1.8   | 0.0   | 0.0   | 0.3   | 0.0   | 0.0   | 1.1   | 7.1   | 7.1   | 0.0   | 10.4  | 10.4  |
| Cycle Q Clear(g_c), s        | 1.8   | 0.0   | 0.0   | 0.3   | 0.0   | 0.0   | 1.1   | 7.1   | 7.1   | 0.0   | 10.4  | 10.4  |
| Prop In Lane                 | 0.65  |   | 0.33  | 0.45  |   | 0.45  | 1.00  |   | 0.00  | 1.00  |   | 0.16  |
| Lane Grp Cap(c), veh/h       | 110   | 0   | 0   | 24  | 0   | 0   | 85  | 926   | 975   | 4   | 844   | 863   |
| V/C Ratio(X)                 | 0.63  | 0.00  | 0.00  | 0.46  | 0.00  | 0.00  | 0.53  | 0.47  | 0.47  | 0.25  | 0.64  | 0.64  |
| Avail Cap(c_a), veh/h        | 952   | 0   | 0   | 938   | 0   | 0   | 257   | 1843  | 1939  | 201   | 1788  | 1829  |
| HCM Platoon Ratio            | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)           | 1.00  | 0.00  | 0.00  | 1.00  | 0.00  | 0.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Uniform Delay (d), s/veh     | 20.6  | 0.0   | 0.0   | 22.1  | 0.0   | 0.0   | 21.0  | 6.9   | 6.9   | 22.5  | 9.0   | 9.0   |
| Incr Delay (d2), s/veh       | 5.8   | 0.0   | 0.0   | 12.8  | 0.0   | 0.0   | 5.0   | 0.4   | 0.4   | 30.6  | 0.8   | 0.8   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln     | 0.8   | 0.0   | 0.0   | 0.2   | 0.0   | 0.0   | 0.5   | 1.6   | 1.7   | 0.0   | 3.1   | 3.1   |
| Unsig. Movement Delay, s/veh |   |   |   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh        | 26.4  | 0.0   | 0.0   | 34.8  | 0.0   | 0.0   | 26.0  | 7.2   | 7.2   | 53.1  | 9.8   | 9.8   |
| LnGrp LOS                    | C   |   |   | C   |   |   | C   | A   | A   | D   | A   | A   |
| Approach Vol, veh/h          |   | 69  |   |   | 11  |   |   | 945   |   |   | 1100  |   |
| Approach Delay, s/veh        |   | 26.4  |   |   | 34.8  |   |   | 8.1   |   |   | 9.8   |   |
| Approach LOS                 |   | C   |   |   | C   |   |   | A   |   |   | A   |   |
| Timer - Assigned Phs         | 1   | 2   |   | 4   | 5   | 6   |   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s     | 4.6   | 28.0  |   | 7.4   | 6.7   | 25.9  |   | 5.1   |   |   |   |   |
| Change Period (Y+Rc), s      | 4.5   | 4.5   |   | 4.5   | 4.5   | 4.5   |   | 4.5   |   |   |   |   |
| Max Green Setting (Gmax), s  | 5.1   | 46.8  |   | 25.1  | 6.5   | 45.4  |   | 25.0  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s | 2.0   | 9.1   |   | 3.8   | 3.1   | 12.4  |   | 2.3   |   |   |   |   |
| Green Ext Time (p_c), s      | 0.0   | 6.1   |   | 0.3   | 0.0   | 9.0   |   | 0.0   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh |   |   | 9.7   |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS                  |   |   | A   |   |   |   |   |   |   |   |   |   |

Queues

1: Norwood Avenue & Bell Avenue

Future No Build PM



| Lane Group              | EBL  | EBT  | WBL  | WBT  | WBR  | NBL  | NBT  | NBR  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 15   | 205  | 300  | 115  | 130  | 130  | 445  | 335  | 130  | 630  |
| v/c Ratio               | 0.06 | 0.66 | 0.59 | 0.14 | 0.17 | 0.54 | 0.55 | 0.55 | 0.52 | 0.75 |
| Control Delay (s/veh)   | 36.8 | 41.0 | 38.4 | 23.9 | 6.6  | 49.6 | 35.4 | 7.4  | 48.6 | 40.3 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 36.8 | 41.0 | 38.4 | 23.9 | 6.6  | 49.6 | 35.4 | 7.4  | 48.6 | 40.3 |
| Queue Length 50th (ft)  | 8    | 90   | 148  | 35   | 0    | 72   | 117  | 0    | 72   | 175  |
| Queue Length 95th (ft)  | 27   | 190  | #349 | 134  | 53   | 158  | 205  | 73   | 158  | 294  |
| Internal Link Dist (ft) |      | 878  |      | 976  |      |      | 1238 |      |      | 453  |
| Turn Bay Length (ft)    | 150  |      | 195  |      | 200  | 75   |      | 200  | 95   |      |
| Base Capacity (vph)     | 521  | 861  | 505  | 930  | 838  | 513  | 1767 | 941  | 508  | 1758 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.03 | 0.24 | 0.59 | 0.12 | 0.16 | 0.25 | 0.25 | 0.36 | 0.26 | 0.36 |

Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.  
 Queue shown is maximum after two cycles.

Queues

2: Norwood Avenue & Jessie Avenue

Future No Build PM



| Lane Group              | EBT  | EBR  | WBT  | NBL  | NBT  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 90   | 165  | 375  | 215  | 990  | 100  | 885  |
| v/c Ratio               | 0.43 | 0.51 | 0.79 | 0.73 | 0.74 | 0.54 | 0.77 |
| Control Delay (s/veh)   | 58.9 | 13.7 | 53.9 | 64.2 | 35.7 | 65.2 | 42.5 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 58.9 | 13.7 | 53.9 | 64.2 | 35.7 | 65.2 | 42.5 |
| Queue Length 50th (ft)  | 65   | 0    | 248  | 153  | 324  | 72   | 314  |
| Queue Length 95th (ft)  | 133  | 66   | #510 | 289  | 520  | 155  | 497  |
| Internal Link Dist (ft) | 758  |      | 547  |      | 632  |      | 1238 |
| Turn Bay Length (ft)    |      | 100  |      | 100  |      | 120  |      |
| Base Capacity (vph)     | 593  | 614  | 576  | 417  | 1470 | 417  | 1423 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.15 | 0.27 | 0.65 | 0.52 | 0.67 | 0.24 | 0.62 |

Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.  
 Queue shown is maximum after two cycles.

Queues

3: Norwood Avenue & WB 80 On-Ramp/WB 80 Off-Ramp

Future No Build PM



| Lane Group              | WBL  | WBT  | WBR  | NBL  | NBT  | SBT  | SBR  |
|-------------------------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 160  | 160  | 350  | 435  | 970  | 765  | 550  |
| v/c Ratio               | 0.43 | 0.43 | 0.80 | 0.78 | 0.40 | 0.67 | 0.82 |
| Control Delay (s/veh)   | 33.3 | 33.3 | 34.8 | 42.6 | 7.9  | 29.4 | 26.2 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.1  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 33.3 | 33.3 | 34.8 | 42.6 | 8.1  | 29.4 | 26.2 |
| Queue Length 50th (ft)  | 83   | 83   | 125  | 230  | 110  | 187  | 147  |
| Queue Length 95th (ft)  | 148  | 148  | 232  | #502 | 220  | 301  | #383 |
| Internal Link Dist (ft) |      | 874  |      |      | 446  | 632  |      |
| Turn Bay Length (ft)    |      |      | 50   | 175  |      |      | 75   |
| Base Capacity (vph)     | 722  | 722  | 739  | 559  | 2752 | 1487 | 787  |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 754  | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.22 | 0.22 | 0.47 | 0.78 | 0.49 | 0.51 | 0.70 |

Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.  
 Queue shown is maximum after two cycles.

Queues

4: Norwood Avenue & EB 80 Off-Ramp/EB 80 On-Ramp

Future No Build PM



| Lane Group              | EBL  | EBT  | EBR  | NBT  | NBR  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 265  | 270  | 465  | 885  | 325  | 330  | 755  |
| v/c Ratio               | 0.57 | 0.58 | 0.81 | 0.78 | 0.30 | 0.76 | 0.35 |
| Control Delay (s/veh)   | 33.3 | 33.5 | 29.2 | 33.3 | 1.9  | 45.5 | 9.5  |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 33.3 | 33.5 | 29.2 | 33.3 | 1.9  | 45.5 | 9.5  |
| Queue Length 50th (ft)  | 132  | 135  | 141  | 232  | 0    | 170  | 98   |
| Queue Length 95th (ft)  | 241  | 247  | 297  | 375  | 35   | #347 | 174  |
| Internal Link Dist (ft) |      | 679  |      | 657  |      |      | 446  |
| Turn Bay Length (ft)    |      |      | 50   |      | 220  | 180  |      |
| Base Capacity (vph)     | 763  | 767  | 817  | 1586 | 1267 | 603  | 2770 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.35 | 0.35 | 0.57 | 0.56 | 0.26 | 0.55 | 0.27 |

Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.  
 Queue shown is maximum after two cycles.

Queues

5: Norwood Avenue & Harris Avenue

Future No Build PM



| Lane Group              | EBT  | EBR  | WBT  | WBR  | NBL  | NBT  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 245  | 45   | 30   | 95   | 30   | 990  | 70   | 1175 |
| v/c Ratio               | 0.69 | 0.08 | 0.12 | 0.32 | 0.13 | 0.62 | 0.33 | 0.77 |
| Control Delay (s/veh)   | 43.9 | 6.4  | 38.6 | 12.2 | 39.7 | 23.4 | 43.2 | 27.5 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 43.9 | 6.4  | 38.6 | 12.2 | 39.7 | 23.4 | 43.2 | 27.5 |
| Queue Length 50th (ft)  | 130  | 0    | 15   | 0    | 15   | 230  | 37   | 305  |
| Queue Length 95th (ft)  | 214  | 22   | 45   | 47   | 46   | 366  | 84   | #495 |
| Internal Link Dist (ft) | 655  |      | 515  |      |      | 251  |      | 657  |
| Turn Bay Length (ft)    |      | 140  |      |      | 85   |      | 110  |      |
| Base Capacity (vph)     | 803  | 1042 | 810  | 753  | 817  | 1597 | 801  | 1533 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.31 | 0.04 | 0.04 | 0.13 | 0.04 | 0.62 | 0.09 | 0.77 |

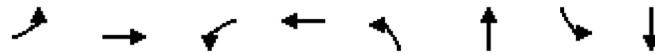
Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.  
 Queue shown is maximum after two cycles.

Queues

6: Norwood Avenue & Silver Eagle Road

Future No Build PM



| Lane Group              | EBL  | EBT  | WBL  | WBT  | NBL  | NBT  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 280  | 390  | 15   | 160  | 190  | 650  | 45   | 845  |
| v/c Ratio               | 0.75 | 0.62 | 0.08 | 0.55 | 0.66 | 0.43 | 0.25 | 0.80 |
| Control Delay (s/veh)   | 51.1 | 30.4 | 49.3 | 45.6 | 51.7 | 21.9 | 50.9 | 36.8 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 51.1 | 30.4 | 49.3 | 45.6 | 51.7 | 21.9 | 50.9 | 36.8 |
| Queue Length 50th (ft)  | 158  | 157  | 8    | 85   | 109  | 150  | 26   | 226  |
| Queue Length 95th (ft)  | #329 | 356  | 34   | 178  | 220  | 260  | 75   | #409 |
| Internal Link Dist (ft) |      | 710  |      | 228  |      | 480  |      | 903  |
| Turn Bay Length (ft)    | 110  |      |      |      | 95   |      | 55   |      |
| Base Capacity (vph)     | 526  | 632  | 526  | 540  | 521  | 1576 | 526  | 1363 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.53 | 0.62 | 0.03 | 0.30 | 0.36 | 0.41 | 0.09 | 0.62 |

Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.  
 Queue shown is maximum after two cycles.

Queues

33: Norwood Avenue & Morey Avenue

Future No Build PM



| Lane Group              | EBT  | WBT  | NBL  | NBT  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 69   | 11   | 45   | 900  | 1    | 1099 |
| v/c Ratio               | 0.26 | 0.06 | 0.21 | 0.35 | 0.01 | 0.49 |
| Control Delay (s/veh)   | 23.8 | 25.1 | 31.6 | 6.3  | 32.0 | 10.2 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 23.8 | 25.1 | 31.6 | 6.3  | 32.0 | 10.2 |
| Queue Length 50th (ft)  | 15   | 2    | 14   | 46   | 0    | 125  |
| Queue Length 95th (ft)  | 63   | 19   | 56   | 203  | 6    | 274  |
| Internal Link Dist (ft) | 329  | 438  |      | 256  |      | 304  |
| Turn Bay Length (ft)    |      |      | 100  |      | 50   |      |
| Base Capacity (vph)     | 863  | 847  | 227  | 2898 | 178  | 2801 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.08 | 0.01 | 0.20 | 0.31 | 0.01 | 0.39 |
| Intersection Summary    |      |      |      |      |      |      |

# HCM 7th Signalized Intersection Summary

## 1: Norwood Avenue & Bell Avenue

## Future AM Road Diet

|  |  |  |  |  |  |  |  |  |  |  |  |  |
|--|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |  |  |   |  |  |  |  |  |   |  |  |  |
| Traffic Volume (veh/h)   | 75  | 190   | 100   | 135   | 95  | 180   | 55  | 445   | 220   | 225   | 500   | 55  |
| Future Volume (veh/h)  | 75  | 190   | 100   | 135   | 95  | 180   | 55  | 445   | 220   | 225   | 500   | 55  |
| Initial Q (Qb), veh  | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 0.96  | 1.00  |   | 0.96  | 1.00  |   | 0.97  | 1.00  |   | 0.97  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   | No  |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1885  | 1885  | 1885  | 1841  | 1841  | 1841  | 1856  | 1856  | 1856  | 1856  | 1856  | 1856  |
| Adj Flow Rate, veh/h   | 75  | 190   | 100   | 135   | 95  | 180   | 55  | 445   | 220   | 225   | 500   | 55  |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 1   | 1   | 1   | 4   | 4   | 4   | 3   | 3   | 3   | 3   | 3   | 3   |
| Cap, veh/h   | 295   | 232   | 122   | 172   | 238   | 193   | 130   | 466   | 230   | 256   | 778   | 86  |
| Arrive On Green  | 0.16  | 0.20  | 0.20  | 0.10  | 0.13  | 0.13  | 0.07  | 0.40  | 0.40  | 0.14  | 0.48  | 0.48  |
| Sat Flow, veh/h  | 1795  | 1143  | 602   | 1753  | 1841  | 1490  | 1767  | 1161  | 574   | 1767  | 1637  | 180   |
| Grp Volume(v), veh/h   | 75  | 0   | 290   | 135   | 95  | 180   | 55  | 0   | 665   | 225   | 0   | 555   |
| Grp Sat Flow(s),veh/h/ln   | 1795  | 0   | 1744  | 1753  | 1841  | 1490  | 1767  | 0   | 1735  | 1767  | 0   | 1818  |
| Q Serve(g_s), s  | 4.0   | 0.0   | 17.6  | 8.3   | 5.2   | 11.0  | 3.3   | 0.0   | 41.1  | 13.8  | 0.0   | 25.5  |
| Cycle Q Clear(g_c), s  | 4.0   | 0.0   | 17.6  | 8.3   | 5.2   | 11.0  | 3.3   | 0.0   | 41.1  | 13.8  | 0.0   | 25.5  |
| Prop In Lane   | 1.00  |   | 0.34  | 1.00  |   | 1.00  | 1.00  |   | 0.33  | 1.00  |   | 0.10  |
| Lane Grp Cap(c), veh/h   | 295   | 0   | 354   | 172   | 238   | 193   | 130   | 0   | 696   | 256   | 0   | 863   |
| V/C Ratio(X)   | 0.25  | 0.00  | 0.82  | 0.79  | 0.40  | 0.93  | 0.42  | 0.00  | 0.95  | 0.88  | 0.00  | 0.64  |
| Avail Cap(c_a), veh/h  | 426   | 0   | 717   | 416   | 756   | 613   | 390   | 0   | 744   | 386   | 0   | 863   |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 1.00  |
| Uniform Delay (d), s/veh   | 40.3  | 0.0   | 42.1  | 48.7  | 44.2  | 32.8  | 48.9  | 0.0   | 32.1  | 46.3  | 0.0   | 21.9  |
| Incr Delay (d2), s/veh   | 0.2   | 0.0   | 1.8   | 3.0   | 0.4   | 8.3   | 0.8   | 0.0   | 21.4  | 10.2  | 0.0   | 1.3   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 1.8   | 0.0   | 7.8   | 3.7   | 2.4   | 4.3   | 1.5   | 0.0   | 20.4  | 6.7   | 0.0   | 10.9  |
| Unsig. Movement Delay, s/veh   |   |   |   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 40.4  | 0.0   | 43.9  | 51.7  | 44.6  | 41.1  | 49.7  | 0.0   | 53.5  | 56.5  | 0.0   | 23.2  |
| LnGrp LOS  | D   |   | D   | D   | D   | D   | D   |   | D   | E   |   | C   |
| Approach Vol, veh/h  |   | 365   |   |   | 410   |   |   | 720   |   |   | 780   |   |
| Approach Delay, s/veh  |   | 43.2  |   |   | 45.4  |   |   | 53.2  |   |   | 32.8  |   |
| Approach LOS   |   | D   |   |   | D   |   |   | D   |   |   | C   |   |
| Timer - Assigned Phs   | 1   | 2   | 3   | 4   | 5   | 6   | 7   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s   | 22.8  | 18.9  | 11.8  | 57.1  | 14.6  | 27.0  | 19.9  | 49.0  |   |   |   |   |
| Change Period (Y+Rc), s  | * 4.6   | * 4.6   | 3.6   | * 4.6   | 3.8   | * 4.6   | 3.9   | * 4.6   |   |   |   |   |
| Max Green Setting (Gmax), s  | * 26  | * 45  | 24.4  | * 47  | 26.2  | * 45  | 24.1  | * 47  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s   | 6.0   | 13.0  | 5.3   | 27.5  | 10.3  | 19.6  | 15.8  | 43.1  |   |   |   |   |
| Green Ext Time (p_c), s  | 0.1   | 0.6   | 0.0   | 2.4   | 0.1   | 1.3   | 0.2   | 1.2   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   |   |   | 43.2  |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS  |   |   | D   |   |   |   |   |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| * HCM 7th computational engine requires equal clearance times for the phases crossing the barrier. |   |   |   |   |   |   |   |   |   |   |   |   |

# HCM 7th Signalized Intersection Summary

## 2: Norwood Avenue & Jessie Avenue

### Future AM Road Diet

|  |  |  |  |  |  |  |  |  |  |  |  |  |
|--|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL  | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |   |  |  |   |  |   |  |  |  |  |  |   |
| Traffic Volume (veh/h)   | 45  | 95  | 210   | 245   | 80  | 65  | 125  | 570   | 100   | 45  | 685   | 35  |
| Future Volume (veh/h)  | 45  | 95  | 210   | 245   | 80  | 65  | 125  | 570   | 100   | 45  | 685   | 35  |
| Initial Q (Qb), veh  | 0   | 0   | 0   | 0   | 0   | 0   | 0  | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 1.00  | 1.00  |   | 0.97  | 1.00   |   | 0.97  | 1.00  |   | 1.00  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   | No  |   |  | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1870  | 1870  | 1870  | 1856  | 1856  | 1856  | 1856   | 1856  | 1856  | 1856  | 1856  | 1856  |
| Adj Flow Rate, veh/h   | 45  | 95  | 210   | 245   | 80  | 65  | 125  | 570   | 100   | 45  | 685   | 35  |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 2   | 2   | 2   | 3   | 3   | 3   | 3  | 3   | 3   | 3   | 3   | 3   |
| Cap, veh/h   | 89  | 189   | 240   | 265   | 86  | 70  | 151  | 800   | 658   | 100   | 704   | 36  |
| Arrive On Green  | 0.15  | 0.15  | 0.15  | 0.24  | 0.24  | 0.24  | 0.09   | 0.43  | 0.43  | 0.06  | 0.40  | 0.40  |
| Sat Flow, veh/h  | 592   | 1249  | 1585  | 1092  | 357   | 290   | 1767   | 1856  | 1527  | 1767  | 1750  | 89  |
| Grp Volume(v), veh/h   | 140   | 0   | 210   | 390   | 0   | 0   | 125  | 570   | 100   | 45  | 0   | 720   |
| Grp Sat Flow(s),veh/h/ln   | 1841  | 0   | 1585  | 1739  | 0   | 0   | 1767   | 1856  | 1527  | 1767  | 0   | 1839  |
| Q Serve(g_s), s  | 8.9   | 0.0   | 16.4  | 27.8  | 0.0   | 0.0   | 8.8  | 32.0  | 5.1   | 3.1   | 0.0   | 48.8  |
| Cycle Q Clear(g_c), s  | 8.9   | 0.0   | 16.4  | 27.8  | 0.0   | 0.0   | 8.8  | 32.0  | 5.1   | 3.1   | 0.0   | 48.8  |
| Prop In Lane   | 0.32  |   | 1.00  | 0.63  |   | 0.17  | 1.00   |   | 1.00  | 1.00  |   | 0.05  |
| Lane Grp Cap(c), veh/h   | 278   | 0   | 240   | 421   | 0   | 0   | 151  | 800   | 658   | 100   | 0   | 740   |
| V/C Ratio(X)   | 0.50  | 0.00  | 0.88  | 0.93  | 0.00  | 0.00  | 0.83   | 0.71  | 0.15  | 0.45  | 0.00  | 0.97  |
| Avail Cap(c_a), veh/h  | 457   | 0   | 394   | 500   | 0   | 0   | 355  | 800   | 658   | 355   | 0   | 745   |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 0.00  | 1.00   | 1.00  | 1.00  | 1.00  | 0.00  | 1.00  |
| Uniform Delay (d), s/veh   | 49.5  | 0.0   | 52.7  | 47.0  | 0.0   | 0.0   | 57.1   | 29.6  | 22.0  | 58.0  | 0.0   | 37.2  |
| Incr Delay (d2), s/veh   | 0.5   | 0.0   | 6.8   | 19.9  | 0.0   | 0.0   | 4.4  | 2.6   | 0.0   | 1.2   | 0.0   | 26.1  |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0  | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 4.1   | 0.0   | 6.9   | 14.3  | 0.0   | 0.0   | 4.1  | 14.3  | 1.8   | 1.4   | 0.0   | 26.9  |
| Unsig. Movement Delay, s/veh   |   |   |   |   |   |   |  |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 50.0  | 0.0   | 59.4  | 66.8  | 0.0   | 0.0   | 61.5   | 32.2  | 22.0  | 59.1  | 0.0   | 63.4  |
| LnGrp LOS  | D   |   | E   | E   |   |   | E  | C   | C   | E   |   | E   |
| Approach Vol, veh/h  | 350   |   |   | 390   |   |   | 795  |   |   | 765   |   |   |
| Approach Delay, s/veh  | 55.7  |   |   | 66.8  |   |   | 35.5   |   |   | 63.1  |   |   |
| Approach LOS   | E   |   |   | E   |   |   | D  |   |   | E   |   |   |
| Timer - Assigned Phs   | 2   |   | 3   |   | 4   |   | 6  |   | 7   |   | 8   |   |
| Phs Duration (G+Y+Rc), s   | 34.2  |   | 14.3  |   | 55.6  |   | 22.7   |   | 10.7  |   | 59.3  |   |
| Change Period (Y+Rc), s  | 3.5   |   | 3.5   |   | * 4.6   |   | 3.5  |   | 3.5   |   | * 4.6   |   |
| Max Green Setting (Gmax), s  | 36.5  |   | 25.5  |   | * 51  |   | 31.5   |   | 25.5  |   | * 51  |   |
| Max Q Clear Time (g_c+I1), s   | 29.8  |   | 10.8  |   | 50.8  |   | 18.4   |   | 5.1   |   | 34.0  |   |
| Green Ext Time (p_c), s  | 0.9   |   | 0.1   |   | 0.2   |   | 0.7  |   | 0.0   |   | 2.2   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |  |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   | 53.1  |   |   |   |   |   |  |   |   |   |   |   |
| HCM 7th LOS  | D   |   |   |   |   |   |  |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |  |   |   |   |   |   |
| * HCM 7th computational engine requires equal clearance times for the phases crossing the barrier. |   |   |   |   |   |   |  |   |   |   |   |   |

# HCM 7th Signalized Intersection Summary

## 3: Norwood Avenue & WB 80 On-Ramp/WB 80 Off-Ramp

Future AM Road Diet

|   |  |  |  |  |  |  |  |  |  |  |  |  |
|---|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement  | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL  | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations   |   |   |   |  |  |  |  |  |  |   |  |  |
| Traffic Volume (veh/h)  | 0   | 0   | 0   | 285   | 5   | 205   | 300  | 735   | 0   | 0   | 695   | 560   |
| Future Volume (veh/h)   | 0   | 0   | 0   | 285   | 5   | 205   | 300  | 735   | 0   | 0   | 695   | 560   |
| Initial Q (Qb), veh   |   |   |   | 0   | 0   | 0   | 0  | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.   |   |   |   | 1.00  | 1.00  | 1.00  | 1.00   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)   |   |   |   | 1.00  |   | 1.00  | 1.00   |   | 1.00  | 1.00  |   | 1.00  |
| Parking Bus, Adj  |   |   |   | 1.00  | 1.00  | 1.00  | 1.00   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach   |   |   |   | No  |   |   | No   |   |   | No  |   |   |
| Adj Sat Flow, veh/h/ln  |   |   |   | 1841  | 1841  | 1841  | 1841   | 1841  | 0   | 0   | 1870  | 1870  |
| Adj Flow Rate, veh/h  |   |   |   | 289   | 0   | 0   | 300  | 735   | 0   | 0   | 695   | 0   |
| Peak Hour Factor  |   |   |   | 1.00  | 1.00  | 1.00  | 1.00   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %  |   |   |   | 4   | 4   | 4   | 4  | 4   | 0   | 0   | 2   | 2   |
| Cap, veh/h  |   |   |   | 643   | 0   |   | 378  | 2136  | 0   | 0   | 1114  |   |
| Arrive On Green   |   |   |   | 0.18  | 0.00  | 0.00  | 0.22   | 0.61  | 0.00  | 0.00  | 0.31  | 0.00  |
| Sat Flow, veh/h   |   |   |   | 3506  | 0   | 1560  | 1753   | 3589  | 0   | 0   | 3647  | 1585  |
| Grp Volume(v), veh/h  |   |   |   | 289   | 0   | 0   | 300  | 735   | 0   | 0   | 695   | 0   |
| Grp Sat Flow(s),veh/h/ln  |   |   |   | 1753  | 0   | 1560  | 1753   | 1749  | 0   | 0   | 1777  | 1585  |
| Q Serve(g_s), s   |   |   |   | 3.1   | 0.0   | 0.0   | 6.9  | 4.4   | 0.0   | 0.0   | 7.1   | 0.0   |
| Cycle Q Clear(g_c), s   |   |   |   | 3.1   | 0.0   | 0.0   | 6.9  | 4.4   | 0.0   | 0.0   | 7.1   | 0.0   |
| Prop In Lane  |   |   |   | 1.00  |   | 1.00  | 1.00   |   | 0.00  | 0.00  |   | 1.00  |
| Lane Grp Cap(c), veh/h  |   |   |   | 643   | 0   |   | 378  | 2136  | 0   | 0   | 1114  |   |
| V/C Ratio(X)  |   |   |   | 0.45  | 0.00  |   | 0.79   | 0.34  | 0.00  | 0.00  | 0.62  |   |
| Avail Cap(c_a), veh/h   |   |   |   | 2951  | 0   |   | 1086   | 2878  | 0   | 0   | 2924  |   |
| HCM Platoon Ratio   |   |   |   | 1.00  | 1.00  | 1.00  | 1.00   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)  |   |   |   | 1.00  | 0.00  | 0.00  | 1.00   | 1.00  | 0.00  | 0.00  | 1.00  | 0.00  |
| Uniform Delay (d), s/veh  |   |   |   | 15.5  | 0.0   | 0.0   | 15.9   | 4.1   | 0.0   | 0.0   | 12.5  | 0.0   |
| Incr Delay (d2), s/veh  |   |   |   | 0.2   | 0.0   | 0.0   | 2.8  | 0.1   | 0.0   | 0.0   | 0.4   | 0.0   |
| Initial Q Delay(d3), s/veh  |   |   |   | 0.0   | 0.0   | 0.0   | 0.0  | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln  |   |   |   | 1.1   | 0.0   | 0.0   | 2.5  | 0.6   | 0.0   | 0.0   | 2.3   | 0.0   |
| Unsig. Movement Delay, s/veh  |   |   |   |   |   | 23.10   |  |   |   |   |   | 20.20   |
| LnGrp Delay(d), s/veh   |   |   |   | 15.7  | 0.0   | 23.1  | 18.7   | 4.2   | 0.0   | 0.0   | 13.0  | 20.2  |
| LnGrp LOS   |   |   |   | B   |   | C   | B  | A   |   |   | B   | C   |
| Approach Vol, veh/h   |   |   |   |   | 394   |   |  | 1035  |   |   | 975   |   |
| Approach Delay, s/veh   |   |   |   |   | 17.7  |   |  | 8.4   |   |   | 15.0  |   |
| Approach LOS  |   |   |   |   | B   |   |  | A   |   |   | B   |   |
| Timer - Assigned Phs  | 1   | 2   |   | 4   |   | 6   |  |   |   |   |   |   |
| Phs Duration (G+Y+Rc), s  | 12.7  | 18.2  |   | 11.8  |   | 30.9  |  |   |   |   |   |   |
| Change Period (Y+Rc), s   | 3.5   | 4.8   |   | 4.0   |   | 4.8   |  |   |   |   |   |   |
| Max Green Setting (Gmax), s   | 26.5  | 35.2  |   | 36.0  |   | 35.2  |  |   |   |   |   |   |
| Max Q Clear Time (g_c+I1), s  | 8.9   | 9.1   |   | 5.1   |   | 6.4   |  |   |   |   |   |   |
| Green Ext Time (p_c), s   | 0.6   | 4.3   |   | 0.5   |   | 4.2   |  |   |   |   |   |   |
| <b>Intersection Summary</b>   |   |   |   |   |   |   |  |   |   |   |   |   |
| HCM 7th Control Delay, s/veh  |   |   |   | 12.6  |   |   |  |   |   |   |   |   |
| HCM 7th LOS   |   |   |   | B   |   |   |  |   |   |   |   |   |
| <b>Notes</b>  |   |   |   |   |   |   |  |   |   |   |   |   |
| User approved volume balancing among the lanes for turning movement.  |   |   |   |   |   |   |  |   |   |   |   |   |
| Unsignalized Delay for [WBR, SBR] is included in calculations of the approach delay and intersection delay. |   |   |   |   |   |   |  |   |   |   |   |   |

# HCM 7th Signalized Intersection Summary

## 4: Norwood Avenue & EB 80 Off-Ramp/EB 80 On-Ramp

Future AM Road Diet

|  |  |  |  |  |  |  |  |  |  |  |  |  |
|--|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |  |  |  |   |   |   |   |  |  |  |  |  |
| Traffic Volume (veh/h)   | 360   | 5   | 435   | 0   | 0   | 0   | 0   | 655   | 295   | 375   | 605   | 0   |
| Future Volume (veh/h)  | 360   | 5   | 435   | 0   | 0   | 0   | 0   | 655   | 295   | 375   | 605   | 0   |
| Initial Q (Qb), veh  | 0   | 0   | 0   |   |   |   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 1.00  |   |   |   | 1.00  |   | 1.00  | 1.00  |   | 1.00  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   |   |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1826  | 1826  | 1826  |   |   |   | 0   | 1841  | 1841  | 1841  | 1841  | 0   |
| Adj Flow Rate, veh/h   | 364   | 0   | 0   |   |   |   | 0   | 655   | 0   | 375   | 605   | 0   |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 5   | 5   | 5   |   |   |   | 0   | 4   | 4   | 4   | 4   | 0   |
| Cap, veh/h   | 672   | 0   |   |   |   |   | 0   | 995   |   | 454   | 2162  | 0   |
| Arrive On Green  | 0.19  | 0.00  | 0.00  |   |   |   | 0.00  | 0.28  | 0.00  | 0.26  | 0.62  | 0.00  |
| Sat Flow, veh/h  | 3478  | 0   | 1547  |   |   |   | 0   | 3589  | 1560  | 1753  | 3589  | 0   |
| Grp Volume(v), veh/h   | 364   | 0   | 0   |   |   |   | 0   | 655   | 0   | 375   | 605   | 0   |
| Grp Sat Flow(s),veh/h/ln   | 1739  | 0   | 1547  |   |   |   | 0   | 1749  | 1560  | 1753  | 1749  | 0   |
| Q Serve(g_s), s  | 4.4   | 0.0   | 0.0   |   |   |   | 0.0   | 7.7   | 0.0   | 9.4   | 3.7   | 0.0   |
| Cycle Q Clear(g_c), s  | 4.4   | 0.0   | 0.0   |   |   |   | 0.0   | 7.7   | 0.0   | 9.4   | 3.7   | 0.0   |
| Prop In Lane   | 1.00  |   | 1.00  |   |   |   | 0.00  |   | 1.00  | 1.00  |   | 0.00  |
| Lane Grp Cap(c), veh/h   | 672   | 0   |   |   |   |   | 0   | 995   |   | 454   | 2162  | 0   |
| V/C Ratio(X)   | 0.54  | 0.00  |   |   |   |   | 0.00  | 0.66  |   | 0.83  | 0.28  | 0.00  |
| Avail Cap(c_a), veh/h  | 2682  | 0   |   |   |   |   | 0   | 2637  |   | 995   | 2637  | 0   |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 0.00  |   |   |   | 0.00  | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  |
| Uniform Delay (d), s/veh   | 17.0  | 0.0   | 0.0   |   |   |   | 0.0   | 14.7  | 0.0   | 16.3  | 4.1   | 0.0   |
| Incr Delay (d2), s/veh   | 0.3   | 0.0   | 0.0   |   |   |   | 0.0   | 0.6   | 0.0   | 2.9   | 0.1   | 0.0   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   |   |   |   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 1.6   | 0.0   | 0.0   |   |   |   | 0.0   | 2.5   | 0.0   | 3.6   | 0.8   | 0.0   |
| Unsig. Movement Delay, s/veh   |   |   | 27.70   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 17.2  | 0.0   | 27.7  |   |   |   | 0.0   | 15.3  | 0.0   | 19.2  | 4.2   | 0.0   |
| LnGrp LOS  | B   |   | C   |   |   |   |   | B   |   | B   | A   |   |
| Approach Vol, veh/h  |   | 579   |   |   |   |   |   | 655   |   |   | 980   |   |
| Approach Delay, s/veh  |   | 21.1  |   |   |   |   |   | 15.3  |   |   | 9.9   |   |
| Approach LOS   |   | C   |   |   |   |   |   | B   |   |   | A   |   |
| Timer - Assigned Phs   |   | 2   |   |   | 5   | 6   |   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s   |   | 33.7  |   |   | 15.6  | 18.1  |   | 13.0  |   |   |   |   |
| Change Period (Y+Rc), s  |   | 4.8   |   |   | 3.5   | 4.8   |   | 4.0   |   |   |   |   |
| Max Green Setting (Gmax), s  |   | 35.2  |   |   | 26.5  | 35.2  |   | 36.0  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s   |   | 5.7   |   |   | 11.4  | 9.7   |   | 6.4   |   |   |   |   |
| Green Ext Time (p_c), s  |   | 3.7   |   |   | 0.8   | 3.6   |   | 0.7   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   |   |   | 14.4  |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS  |   |   | B   |   |   |   |   |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| User approved volume balancing among the lanes for turning movement.                                   |   |   |   |   |   |   |   |   |   |   |   |   |
| Unsignalized Delay for [EBR] is included in calculations of the approach delay and intersection delay. |   |   |   |   |   |   |   |   |   |   |   |   |

Unsignalized Delay for [NBR] is excluded from calculations of the approach delay and intersection delay.

# HCM 7th Signalized Intersection Summary

## 5: Norwood Avenue & Harris Avenue

Future AM Road Diet

|  |  |  |  |  |  |  |   |  |  |  |  |  |
|--|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |   |  |  |   |  |  |  |  |   |  |  |  |
| Traffic Volume (veh/h)   | 150   | 25  | 40  | 15  | 35  | 115   | 45  | 680   | 20  | 95  | 670   | 285   |
| Future Volume (veh/h)  | 150   | 25  | 40  | 15  | 35  | 115   | 45  | 680   | 20  | 95  | 670   | 285   |
| Initial Q (Qb), veh  | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 0.98  | 1.00  |   | 0.98  | 1.00  |   | 0.98  | 1.00  |   | 0.98  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   | No  |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1707  | 1707  | 1707  | 1826  | 1826  | 1826  | 1870  | 1870  | 1870  | 1841  | 1841  | 1841  |
| Adj Flow Rate, veh/h   | 150   | 25  | 40  | 15  | 35  | 115   | 45  | 680   | 20  | 95  | 670   | 285   |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 13  | 13  | 13  | 5   | 5   | 5   | 2   | 2   | 2   | 4   | 4   | 4   |
| Cap, veh/h   | 206   | 34  | 323   | 75  | 176   | 211   | 143   | 739   | 22  | 179   | 792   | 656   |
| Arrive On Green  | 0.15  | 0.15  | 0.15  | 0.14  | 0.14  | 0.14  | 0.08  | 0.41  | 0.41  | 0.10  | 0.43  | 0.43  |
| Sat Flow, veh/h  | 1403  | 234   | 1413  | 540   | 1259  | 1512  | 1781  | 1806  | 53  | 1753  | 1841  | 1524  |
| Grp Volume(v), veh/h   | 175   | 0   | 40  | 50  | 0   | 115   | 45  | 0   | 700   | 95  | 670   | 285   |
| Grp Sat Flow(s),veh/h/ln   | 1637  | 0   | 1413  | 1799  | 0   | 1512  | 1781  | 0   | 1859  | 1753  | 1841  | 1524  |
| Q Serve(g_s), s  | 7.8   | 0.0   | 1.7   | 1.9   | 0.0   | 5.4   | 1.8   | 0.0   | 27.3  | 3.9   | 24.9  | 10.0  |
| Cycle Q Clear(g_c), s  | 7.8   | 0.0   | 1.7   | 1.9   | 0.0   | 5.4   | 1.8   | 0.0   | 27.3  | 3.9   | 24.9  | 10.0  |
| Prop In Lane   | 0.86  |   | 1.00  | 0.30  |   | 1.00  | 1.00  |   | 0.03  | 1.00  |   | 1.00  |
| Lane Grp Cap(c), veh/h   | 240   | 0   | 323   | 251   | 0   | 211   | 143   | 0   | 760   | 179   | 792   | 656   |
| V/C Ratio(X)   | 0.73  | 0.00  | 0.12  | 0.20  | 0.00  | 0.54  | 0.31  | 0.00  | 0.92  | 0.53  | 0.85  | 0.43  |
| Avail Cap(c_a), veh/h  | 780   | 0   | 790   | 852   | 0   | 717   | 851   | 0   | 862   | 838   | 853   | 706   |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Uniform Delay (d), s/veh   | 31.2  | 0.0   | 23.5  | 29.1  | 0.0   | 30.6  | 33.1  | 0.0   | 21.4  | 32.6  | 19.5  | 15.2  |
| Incr Delay (d2), s/veh   | 1.6   | 0.0   | 0.1   | 0.1   | 0.0   | 0.8   | 0.5   | 0.0   | 13.6  | 0.9   | 7.2   | 0.3   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 3.1   | 0.0   | 0.5   | 0.8   | 0.0   | 1.9   | 0.8   | 0.0   | 13.2  | 1.7   | 11.3  | 3.3   |
| Unsig. Movement Delay, s/veh   |   |   |   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 32.8  | 0.0   | 23.6  | 29.2  | 0.0   | 31.4  | 33.6  | 0.0   | 35.0  | 33.5  | 26.7  | 15.6  |
| LnGrp LOS  | C   |   | C   | C   |   | C   | C   |   | D   | C   | C   | B   |
| Approach Vol, veh/h  |   | 215   |   |   | 165   |   |   | 745   |   |   | 1050  |   |
| Approach Delay, s/veh  |   | 31.1  |   |   | 30.8  |   |   | 34.9  |   |   | 24.3  |   |
| Approach LOS   |   | C   |   |   | C   |   |   | C   |   |   | C   |   |
| Timer - Assigned Phs   |   | 2   | 3   | 4   |   | 6   | 7   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s   |   | 14.5  | 9.7   | 37.5  |   | 14.8  | 11.3  | 35.8  |   |   |   |   |
| Change Period (Y+Rc), s  |   | 3.8   | 3.5   | * 4.6   |   | 3.6   | 3.5   | * 4.6   |   |   |   |   |
| Max Green Setting (Gmax), s  |   | 36.2  | 36.5  | * 35  |   | 36.4  | 36.5  | * 35  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s   |   | 7.4   | 3.8   | 26.9  |   | 9.8   | 5.9   | 29.3  |   |   |   |   |
| Green Ext Time (p_c), s  |   | 0.4   | 0.0   | 3.1   |   | 0.7   | 0.1   | 2.0   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   |   |   | 29.1  |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS  |   |   | C   |   |   |   |   |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| * HCM 7th computational engine requires equal clearance times for the phases crossing the barrier. |   |   |   |   |   |   |   |   |   |   |   |   |

HCM 7th Signalized Intersection Summary  
6: Norwood Avenue & Silver Eagle Road

Future AM Road Diet

|  |  |  |  |  |  |  |  |  |  |  |  |  |
|--|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |  |  |   |  |  |   |  |  |   |  |  |   |
| Traffic Volume (veh/h)   | 200   | 125   | 270   | 50  | 125   | 30  | 195   | 475   | 25  | 10  | 420   | 190   |
| Future Volume (veh/h)  | 200   | 125   | 270   | 50  | 125   | 30  | 195   | 475   | 25  | 10  | 420   | 190   |
| Initial Q (Qb), veh  | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 0.97  | 1.00  |   | 0.98  | 1.00  |   | 1.00  | 1.00  |   | 0.97  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   | No  |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1826  | 1826  | 1826  | 1856  | 1856  | 1856  | 1870  | 1870  | 1870  | 1856  | 1856  | 1856  |
| Adj Flow Rate, veh/h   | 200   | 125   | 270   | 50  | 125   | 30  | 195   | 475   | 25  | 10  | 420   | 190   |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 5   | 5   | 5   | 3   | 3   | 3   | 2   | 2   | 2   | 3   | 3   | 3   |
| Cap, veh/h   | 234   | 133   | 287   | 134   | 295   | 71  | 229   | 845   | 44  | 39  | 447   | 202   |
| Arrive On Green  | 0.13  | 0.26  | 0.26  | 0.08  | 0.21  | 0.21  | 0.13  | 0.48  | 0.48  | 0.02  | 0.37  | 0.37  |
| Sat Flow, veh/h  | 1739  | 505   | 1090  | 1767  | 1440  | 346   | 1781  | 1761  | 93  | 1767  | 1199  | 542   |
| Grp Volume(v), veh/h   | 200   | 0   | 395   | 50  | 0   | 155   | 195   | 0   | 500   | 10  | 0   | 610   |
| Grp Sat Flow(s),veh/h/ln   | 1739  | 0   | 1595  | 1767  | 0   | 1786  | 1781  | 0   | 1853  | 1767  | 0   | 1741  |
| Q Serve(g_s), s  | 11.0  | 0.0   | 23.7  | 2.6   | 0.0   | 7.4   | 10.5  | 0.0   | 18.8  | 0.5   | 0.0   | 33.1  |
| Cycle Q Clear(g_c), s  | 11.0  | 0.0   | 23.7  | 2.6   | 0.0   | 7.4   | 10.5  | 0.0   | 18.8  | 0.5   | 0.0   | 33.1  |
| Prop In Lane   | 1.00  |   | 0.68  | 1.00  |   | 0.19  | 1.00  |   | 0.05  | 1.00  |   | 0.31  |
| Lane Grp Cap(c), veh/h   | 234   | 0   | 421   | 134   | 0   | 366   | 229   | 0   | 889   | 39  | 0   | 650   |
| V/C Ratio(X)   | 0.85  | 0.00  | 0.94  | 0.37  | 0.00  | 0.42  | 0.85  | 0.00  | 0.56  | 0.26  | 0.00  | 0.94  |
| Avail Cap(c_a), veh/h  | 471   | 0   | 426   | 479   | 0   | 484   | 392   | 0   | 889   | 389   | 0   | 719   |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 1.00  |
| Uniform Delay (d), s/veh   | 41.4  | 0.0   | 35.2  | 43.0  | 0.0   | 33.8  | 41.7  | 0.0   | 18.1  | 47.0  | 0.0   | 29.6  |
| Incr Delay (d2), s/veh   | 3.4   | 0.0   | 28.2  | 0.6   | 0.0   | 0.3   | 3.4   | 0.0   | 0.5   | 1.3   | 0.0   | 18.4  |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 4.9   | 0.0   | 12.3  | 1.2   | 0.0   | 3.2   | 4.7   | 0.0   | 7.5   | 0.3   | 0.0   | 16.6  |
| Unsig. Movement Delay, s/veh   |   |   |   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 44.8  | 0.0   | 63.5  | 43.6  | 0.0   | 34.1  | 45.1  | 0.0   | 18.6  | 48.3  | 0.0   | 48.0  |
| LnGrp LOS  | D   |   | E   | D   |   | C   | D   |   | B   | D   |   | D   |
| Approach Vol, veh/h  |   | 595   |   |   | 205   |   |   | 695   |   |   | 620   |   |
| Approach Delay, s/veh  |   | 57.2  |   |   | 36.4  |   |   | 26.0  |   |   | 48.0  |   |
| Approach LOS   |   | E   |   |   | D   |   |   | C   |   |   | D   |   |
| Timer - Assigned Phs   | 1   | 2   | 3   | 4   | 5   | 6   | 7   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s   | 16.7  | 23.9  | 16.1  | 41.1  | 10.9  | 29.7  | 5.6   | 51.5  |   |   |   |   |
| Change Period (Y+Rc), s  | 3.5   | * 3.9   | 3.5   | * 4.6   | 3.5   | 3.9   | 3.5   | * 4.6   |   |   |   |   |
| Max Green Setting (Gmax), s  | 26.5  | * 27  | 21.5  | * 40  | 26.5  | 26.1  | 21.5  | * 40  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s   | 13.0  | 9.4   | 12.5  | 35.1  | 4.6   | 25.7  | 2.5   | 20.8  |   |   |   |   |
| Green Ext Time (p_c), s  | 0.2   | 0.5   | 0.2   | 1.4   | 0.0   | 0.1   | 0.0   | 1.8   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   |   |   | 42.2  |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS  |   |   | D   |   |   |   |   |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| * HCM 7th computational engine requires equal clearance times for the phases crossing the barrier. |   |   |   |   |   |   |   |   |   |   |   |   |

# HCM 7th Signalized Intersection Summary

## 33: Norwood Avenue & Morey Avenue

Future AM Road Diet

|                              |  |  |  |  |  |  |  |  |  |  |  |  |
|------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement                     | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations          |   |  |   |   |  |   |  |  |   |  |  |   |
| Traffic Volume (veh/h)       | 90  | 1   | 45  | 5   | 1   | 5   | 23  | 681   | 1   | 1   | 679   | 45  |
| Future Volume (veh/h)        | 90  | 1   | 45  | 5   | 1   | 5   | 23  | 681   | 1   | 1   | 679   | 45  |
| Initial Q (Qb), veh          | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.              | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)          | 1.00  |   | 1.00  | 1.00  |   | 1.00  | 1.00  |   | 1.00  | 1.00  |   | 1.00  |
| Parking Bus, Adj             | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach        |   | No  |   |   | No  |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln       | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  |
| Adj Flow Rate, veh/h         | 98  | 1   | 49  | 5   | 1   | 5   | 25  | 740   | 1   | 1   | 738   | 49  |
| Peak Hour Factor             | 0.92  | 0.92  | 0.92  | 0.92  | 0.92  | 0.92  | 0.92  | 0.92  | 0.92  | 0.92  | 0.92  | 0.92  |
| Percent Heavy Veh, %         | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   |
| Cap, veh/h                   | 135   | 1   | 67  | 11  | 2   | 11  | 51  | 1008  | 1   | 3   | 889   | 59  |
| Arrive On Green              | 0.12  | 0.12  | 0.12  | 0.01  | 0.01  | 0.01  | 0.03  | 0.54  | 0.54  | 0.00  | 0.51  | 0.51  |
| Sat Flow, veh/h              | 1133  | 12  | 567   | 770   | 154   | 770   | 1781  | 1867  | 3   | 1781  | 1734  | 115   |
| Grp Volume(v), veh/h         | 148   | 0   | 0   | 11  | 0   | 0   | 25  | 0   | 741   | 1   | 0   | 787   |
| Grp Sat Flow(s),veh/h/ln     | 1712  | 0   | 0   | 1693  | 0   | 0   | 1781  | 0   | 1870  | 1781  | 0   | 1850  |
| Q Serve(g_s), s              | 4.6   | 0.0   | 0.0   | 0.4   | 0.0   | 0.0   | 0.8   | 0.0   | 16.7  | 0.0   | 0.0   | 20.0  |
| Cycle Q Clear(g_c), s        | 4.6   | 0.0   | 0.0   | 0.4   | 0.0   | 0.0   | 0.8   | 0.0   | 16.7  | 0.0   | 0.0   | 20.0  |
| Prop In Lane                 | 0.66  |   | 0.33  | 0.45  |   | 0.45  | 1.00  |   | 0.00  | 1.00  |   | 0.06  |
| Lane Grp Cap(c), veh/h       | 204   | 0   | 0   | 24  | 0   | 0   | 51  | 0   | 1010  | 3   | 0   | 948   |
| V/C Ratio(X)                 | 0.73  | 0.00  | 0.00  | 0.46  | 0.00  | 0.00  | 0.49  | 0.00  | 0.73  | 0.31  | 0.00  | 0.83  |
| Avail Cap(c_a), veh/h        | 774   | 0   | 0   | 766   | 0   | 0   | 164   | 0   | 1590  | 161   | 0   | 1569  |
| HCM Platoon Ratio            | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)           | 1.00  | 0.00  | 0.00  | 1.00  | 0.00  | 0.00  | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 1.00  |
| Uniform Delay (d), s/veh     | 23.5  | 0.0   | 0.0   | 27.0  | 0.0   | 0.0   | 26.4  | 0.0   | 9.7   | 27.6  | 0.0   | 11.4  |
| Incr Delay (d2), s/veh       | 4.9   | 0.0   | 0.0   | 13.3  | 0.0   | 0.0   | 7.0   | 0.0   | 1.1   | 47.2  | 0.0   | 2.0   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln     | 2.0   | 0.0   | 0.0   | 0.2   | 0.0   | 0.0   | 0.4   | 0.0   | 4.9   | 0.1   | 0.0   | 6.8   |
| Unsig. Movement Delay, s/veh |   |   |   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh        | 28.4  | 0.0   | 0.0   | 40.4  | 0.0   | 0.0   | 33.4  | 0.0   | 10.7  | 74.7  | 0.0   | 13.4  |
| LnGrp LOS                    | C   |   |   | D   |   |   | C   |   | B   | E   |   | B   |
| Approach Vol, veh/h          |   | 148   |   |   | 11  |   |   | 766   |   |   |   | 788   |
| Approach Delay, s/veh        |   | 28.4  |   |   | 40.4  |   |   | 11.5  |   |   |   | 13.5  |
| Approach LOS                 |   | C   |   |   | D   |   |   | B   |   |   |   | B   |
| Timer - Assigned Phs         | 1   | 2   |   | 4   | 5   | 6   |   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s     | 4.6   | 34.4  |   | 11.1  | 6.1   | 32.8  |   | 5.3   |   |   |   |   |
| Change Period (Y+Rc), s      | 4.5   | 4.5   |   | 4.5   | 4.5   | 4.5   |   | 4.5   |   |   |   |   |
| Max Green Setting (Gmax), s  | 5.0   | 47.0  |   | 25.0  | 5.1   | 46.9  |   | 25.0  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s | 2.0   | 18.7  |   | 6.6   | 2.8   | 22.0  |   | 2.4   |   |   |   |   |
| Green Ext Time (p_c), s      | 0.0   | 5.4   |   | 0.7   | 0.0   | 6.4   |   | 0.0   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh |   |   | 14.0  |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS                  |   |   | B   |   |   |   |   |   |   |   |   |   |

Queues

1: Norwood Avenue & Bell Avenue

Future AM Road Diet



| Lane Group              | EBL  | EBT  | WBL  | WBT  | WBR  | NBL  | NBT  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 75   | 290  | 135  | 95   | 180  | 55   | 665  | 225  | 555  |
| v/c Ratio               | 0.21 | 0.82 | 0.65 | 0.37 | 0.49 | 0.37 | 0.99 | 0.79 | 0.62 |
| Control Delay (s/veh)   | 43.2 | 64.9 | 70.0 | 58.5 | 12.2 | 66.4 | 70.4 | 71.4 | 30.7 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 43.2 | 64.9 | 70.0 | 58.5 | 12.2 | 66.4 | 70.4 | 71.4 | 30.7 |
| Queue Length 50th (ft)  | 50   | 216  | 107  | 76   | 0    | 43   | ~530 | 174  | 329  |
| Queue Length 95th (ft)  | 104  | 342  | 194  | 140  | 70   | 98   | #989 | #332 | 601  |
| Internal Link Dist (ft) |      | 878  |      | 976  |      |      | 1238 |      | 453  |
| Turn Bay Length (ft)    | 150  |      | 195  |      | 200  | 75   |      | 95   |      |
| Base Capacity (vph)     | 423  | 648  | 368  | 671  | 671  | 346  | 675  | 341  | 890  |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.18 | 0.45 | 0.37 | 0.14 | 0.27 | 0.16 | 0.99 | 0.66 | 0.62 |

Intersection Summary

~ Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.

# 95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Queues

2: Norwood Avenue & Jessie Avenue

Future AM Road Diet



| Lane Group              | EBT  | EBR  | WBT  | NBL  | NBT  | NBR  | SBL  | SBT   |
|-------------------------|------|------|------|------|------|------|------|-------|
| Lane Group Flow (vph)   | 140  | 210  | 390  | 125  | 570  | 100  | 45   | 720   |
| v/c Ratio               | 0.66 | 0.57 | 0.84 | 0.68 | 0.69 | 0.14 | 0.35 | 1.00  |
| Control Delay (s/veh)   | 71.6 | 13.2 | 62.2 | 75.7 | 36.5 | 11.0 | 69.3 | 73.7  |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.8  | 0.0  | 0.0  | 0.0   |
| Total Delay (s/veh)     | 71.6 | 13.2 | 62.2 | 75.7 | 37.3 | 11.0 | 69.3 | 73.7  |
| Queue Length 50th (ft)  | 117  | 0    | 305  | 104  | 395  | 18   | 37   | ~609  |
| Queue Length 95th (ft)  | 196  | 74   | #555 | 183  | 619  | 60   | 86   | #1050 |
| Internal Link Dist (ft) | 758  |      | 547  |      | 632  |      |      | 1238  |
| Turn Bay Length (ft)    |      | 100  |      | 100  |      |      | 120  |       |
| Base Capacity (vph)     | 442  | 541  | 485  | 342  | 827  | 699  | 342  | 721   |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 76   | 0    | 0    | 0     |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0     |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0     |
| Reduced v/c Ratio       | 0.32 | 0.39 | 0.80 | 0.37 | 0.76 | 0.14 | 0.13 | 1.00  |

Intersection Summary

~ Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.

# 95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Queues

3: Norwood Avenue & WB 80 On-Ramp/WB 80 Off-Ramp

Future AM Road Diet



| Lane Group                  | WBL  | WBT  | WBR  | NBL  | NBT  | SBT  | SBR  |
|-----------------------------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)       | 145  | 145  | 205  | 300  | 735  | 695  | 560  |
| v/c Ratio                   | 0.47 | 0.46 | 0.45 | 0.68 | 0.31 | 0.54 | 0.75 |
| Control Delay (s/veh)       | 33.6 | 33.6 | 8.2  | 34.8 | 5.3  | 20.3 | 17.0 |
| Queue Delay                 | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)         | 33.6 | 33.6 | 8.2  | 34.8 | 5.3  | 20.3 | 17.0 |
| Queue Length 50th (ft)      | 57   | 57   | 0    | 109  | 47   | 111  | 83   |
| Queue Length 95th (ft)      | 137  | 137  | 54   | 260  | 124  | 240  | 293  |
| Internal Link Dist (ft)     |      | 874  |      |      | 446  | 632  |      |
| Turn Bay Length (ft)        |      |      | 50   | 175  |      |      | 75   |
| Base Capacity (vph)         | 933  | 937  | 956  | 723  | 3064 | 1959 | 984  |
| Starvation Cap Reductn      | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn       | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn         | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio           | 0.16 | 0.15 | 0.21 | 0.41 | 0.24 | 0.35 | 0.57 |
| <b>Intersection Summary</b> |      |      |      |      |      |      |      |

Queues

4: Norwood Avenue & EB 80 Off-Ramp/EB 80 On-Ramp

Future AM Road Diet



| Lane Group              | EBL  | EBT  | EBR  | NBT  | NBR  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 184  | 181  | 435  | 655  | 295  | 375  | 605  |
| v/c Ratio               | 0.49 | 0.48 | 0.77 | 0.65 | 0.45 | 0.72 | 0.27 |
| Control Delay (s/veh)   | 30.8 | 30.6 | 20.2 | 27.9 | 5.8  | 35.8 | 7.0  |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 30.8 | 30.6 | 20.2 | 27.9 | 5.8  | 35.8 | 7.0  |
| Queue Length 50th (ft)  | 76   | 75   | 61   | 135  | 0    | 142  | 50   |
| Queue Length 95th (ft)  | 165  | 162  | 195  | 255  | 59   | #402 | 127  |
| Internal Link Dist (ft) |      | 679  |      | 657  |      |      | 446  |
| Turn Bay Length (ft)    |      |      | 50   |      | 220  | 180  |      |
| Base Capacity (vph)     | 847  | 851  | 922  | 1762 | 915  | 663  | 2973 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.22 | 0.21 | 0.47 | 0.37 | 0.32 | 0.57 | 0.20 |

Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.  
 Queue shown is maximum after two cycles.

Queues

5: Norwood Avenue & Harris Avenue

Future AM Road Diet



| Lane Group              | EBT  | EBR  | WBT  | WBR  | NBL  | NBT  | SBL  | SBT  | SBR  |
|-------------------------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 175  | 40   | 50   | 115  | 45   | 700  | 95   | 670  | 285  |
| v/c Ratio               | 0.64 | 0.09 | 0.22 | 0.40 | 0.22 | 0.92 | 0.47 | 0.82 | 0.38 |
| Control Delay (s/veh)   | 44.9 | 7.1  | 39.8 | 12.4 | 40.9 | 45.8 | 45.6 | 34.3 | 11.6 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 44.9 | 7.1  | 39.8 | 12.4 | 40.9 | 45.8 | 45.6 | 34.3 | 11.6 |
| Queue Length 50th (ft)  | 90   | 0    | 25   | 0    | 22   | 339  | 49   | 325  | 51   |
| Queue Length 95th (ft)  | 160  | 21   | 67   | 51   | 62   | #726 | 107  | #642 | 135  |
| Internal Link Dist (ft) | 655  |      | 515  |      |      | 251  |      | 657  |      |
| Turn Bay Length (ft)    |      | 140  |      |      | 85   |      | 110  |      |      |
| Base Capacity (vph)     | 671  | 849  | 738  | 696  | 739  | 759  | 725  | 813  | 747  |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.26 | 0.05 | 0.07 | 0.17 | 0.06 | 0.92 | 0.13 | 0.82 | 0.38 |

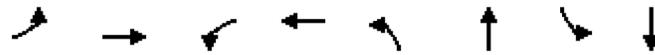
Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.  
 Queue shown is maximum after two cycles.

Queues

6: Norwood Avenue & Silver Eagle Road

Future AM Road Diet



| Lane Group              | EBL  | EBT  | WBL  | WBT  | NBL  | NBT  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 200  | 395  | 50   | 155  | 195  | 500  | 10   | 610  |
| v/c Ratio               | 0.74 | 0.83 | 0.30 | 0.49 | 0.76 | 0.50 | 0.07 | 0.91 |
| Control Delay (s/veh)   | 61.1 | 47.1 | 54.6 | 45.5 | 64.7 | 20.5 | 52.4 | 52.0 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 61.1 | 47.1 | 54.6 | 45.5 | 64.7 | 20.5 | 52.4 | 52.0 |
| Queue Length 50th (ft)  | 134  | 220  | 33   | 92   | 131  | 200  | 7    | 390  |
| Queue Length 95th (ft)  | 232  | 365  | 81   | 178  | 235  | 446  | 27   | #779 |
| Internal Link Dist (ft) |      | 710  |      | 228  |      | 480  |      | 903  |
| Turn Bay Length (ft)    | 110  |      |      |      | 95   |      | 55   |      |
| Base Capacity (vph)     | 428  | 478  | 436  | 449  | 357  | 993  | 353  | 671  |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.47 | 0.83 | 0.11 | 0.35 | 0.55 | 0.50 | 0.03 | 0.91 |

Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.  
 Queue shown is maximum after two cycles.

Queues

33: Norwood Avenue & Morey Avenue

Future AM Road Diet



| Lane Group              | EBT  | WBT  | NBL  | NBT  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 148  | 11   | 25   | 741  | 1    | 787  |
| v/c Ratio               | 0.56 | 0.08 | 0.22 | 0.57 | 0.01 | 0.64 |
| Control Delay (s/veh)   | 35.9 | 30.6 | 42.2 | 11.3 | 39.0 | 14.0 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 35.9 | 30.6 | 42.2 | 11.3 | 39.0 | 14.0 |
| Queue Length 50th (ft)  | 51   | 2    | 10   | 120  | 0    | 133  |
| Queue Length 95th (ft)  | 129  | 21   | 41   | 512  | 6    | #630 |
| Internal Link Dist (ft) | 329  | 438  |      | 256  |      | 304  |
| Turn Bay Length (ft)    |      |      | 100  |      | 50   |      |
| Base Capacity (vph)     | 565  | 552  | 116  | 1294 | 113  | 1238 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.26 | 0.02 | 0.22 | 0.57 | 0.01 | 0.64 |

Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.  
 Queue shown is maximum after two cycles.

# HCM 7th Signalized Intersection Summary

## 1: Norwood Avenue & Bell Avenue

## Future PM Road Diet

|  |  |  |  |  |  |  |  |  |  |  |  |  |
|--|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |  |  |   |  |  |  |  |  |   |  |  |  |
| Traffic Volume (veh/h)   | 20  | 115   | 85  | 205   | 145   | 170   | 95  | 320   | 250   | 195   | 495   | 30  |
| Future Volume (veh/h)  | 20  | 115   | 85  | 205   | 145   | 170   | 95  | 320   | 250   | 195   | 495   | 30  |
| Initial Q (Qb), veh  | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 0.98  | 1.00  |   | 0.95  | 1.00  |   | 0.98  | 1.00  |   | 0.98  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   | No  |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1885  | 1885  | 1885  | 1870  | 1870  | 1870  | 1885  | 1885  | 1885  | 1885  | 1885  | 1885  |
| Adj Flow Rate, veh/h   | 20  | 115   | 85  | 205   | 145   | 170   | 95  | 320   | 250   | 195   | 495   | 30  |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 1   | 1   | 1   | 2   | 2   | 2   | 1   | 1   | 1   | 1   | 1   | 1   |
| Cap, veh/h   | 286   | 154   | 114   | 246   | 232   | 187   | 195   | 354   | 277   | 240   | 692   | 42  |
| Arrive On Green  | 0.16  | 0.15  | 0.15  | 0.14  | 0.12  | 0.12  | 0.11  | 0.37  | 0.37  | 0.13  | 0.39  | 0.39  |
| Sat Flow, veh/h  | 1795  | 995   | 736   | 1781  | 1870  | 1511  | 1795  | 970   | 758   | 1795  | 1757  | 106   |
| Grp Volume(v), veh/h   | 20  | 0   | 200   | 205   | 145   | 170   | 95  | 0   | 570   | 195   | 0   | 525   |
| Grp Sat Flow(s),veh/h/ln   | 1795  | 0   | 1731  | 1781  | 1870  | 1511  | 1795  | 0   | 1728  | 1795  | 0   | 1863  |
| Q Serve(g_s), s  | 0.8   | 0.0   | 9.0   | 9.1   | 6.0   | 6.9   | 4.0   | 0.0   | 25.4  | 8.6   | 0.0   | 19.3  |
| Cycle Q Clear(g_c), s  | 0.8   | 0.0   | 9.0   | 9.1   | 6.0   | 6.9   | 4.0   | 0.0   | 25.4  | 8.6   | 0.0   | 19.3  |
| Prop In Lane   | 1.00  |   | 0.43  | 1.00  |   | 1.00  | 1.00  |   | 0.44  | 1.00  |   | 0.06  |
| Lane Grp Cap(c), veh/h   | 286   | 0   | 268   | 246   | 232   | 187   | 195   | 0   | 631   | 240   | 0   | 734   |
| V/C Ratio(X)   | 0.07  | 0.00  | 0.75  | 0.83  | 0.63  | 0.91  | 0.49  | 0.00  | 0.90  | 0.81  | 0.00  | 0.72  |
| Avail Cap(c_a), veh/h  | 579   | 0   | 968   | 575   | 1046  | 845   | 584   | 0   | 966   | 577   | 0   | 1042  |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 1.00  |
| Uniform Delay (d), s/veh   | 29.0  | 0.0   | 32.8  | 34.1  | 33.8  | 20.3  | 34.0  | 0.0   | 24.4  | 34.2  | 0.0   | 20.8  |
| Incr Delay (d2), s/veh   | 0.0   | 0.0   | 1.6   | 2.8   | 1.0   | 6.5   | 0.7   | 0.0   | 5.8   | 2.5   | 0.0   | 0.5   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 0.3   | 0.0   | 3.8   | 3.9   | 2.6   | 3.4   | 1.7   | 0.0   | 10.4  | 3.8   | 0.0   | 8.0   |
| Unsig. Movement Delay, s/veh   |   |   |   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 29.1  | 0.0   | 34.4  | 36.9  | 34.8  | 26.8  | 34.7  | 0.0   | 30.2  | 36.7  | 0.0   | 21.3  |
| LnGrp LOS  | C   |   | C   | D   | C   | C   | C   |   | C   | D   |   | C   |
| Approach Vol, veh/h  |   | 220   |   |   | 520   |   |   | 665   |   |   | 720   |   |
| Approach Delay, s/veh  |   | 33.9  |   |   | 33.0  |   |   | 30.9  |   |   | 25.5  |   |
| Approach LOS   |   | C   |   |   | C   |   |   | C   |   |   | C   |   |
| Timer - Assigned Phs   | 1   | 2   | 3   | 4   | 5   | 6   | 7   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s   | 17.5  | 14.7  | 12.4  | 36.6  | 15.0  | 17.2  | 14.8  | 34.2  |   |   |   |   |
| Change Period (Y+Rc), s  | * 4.6   | * 4.6   | 3.6   | * 4.6   | 3.8   | * 4.6   | 3.9   | * 4.6   |   |   |   |   |
| Max Green Setting (Gmax), s  | * 26  | * 45  | 26.4  | * 45  | 26.2  | * 45  | 26.1  | * 45  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s   | 2.8   | 8.9   | 6.0   | 21.3  | 11.1  | 11.0  | 10.6  | 27.4  |   |   |   |   |
| Green Ext Time (p_c), s  | 0.0   | 0.8   | 0.1   | 2.3   | 0.2   | 0.9   | 0.2   | 2.3   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   |   |   | 29.9  |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS  |   |   | C   |   |   |   |   |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| * HCM 7th computational engine requires equal clearance times for the phases crossing the barrier. |   |   |   |   |   |   |   |   |   |   |   |   |

# HCM 7th Signalized Intersection Summary

## 2: Norwood Avenue & Jessie Avenue

## Future PM Road Diet

|  |  |  |  |  |  |  |  |  |  |  |  |  |
|--|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |   |  |  |   |  |   |   |  |  |  |  |   |
| Traffic Volume (veh/h)   | 25  | 65  | 155   | 240   | 95  | 40  | 215   | 615   | 200   | 95  | 640   | 20  |
| Future Volume (veh/h)  | 25  | 65  | 155   | 240   | 95  | 40  | 215   | 615   | 200   | 95  | 640   | 20  |
| Initial Q (Qb), veh  | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 0.96  | 1.00  |   | 0.97  | 1.00  |   | 0.98  | 1.00  |   | 0.97  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   | No  |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1885  | 1885  | 1885  | 1885  | 1885  | 1885  | 1885  | 1885  | 1885  | 1885  | 1885  | 1885  |
| Adj Flow Rate, veh/h   | 25  | 65  | 155   | 240   | 95  | 40  | 215   | 615   | 200   | 95  | 640   | 20  |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 1   | 1   | 1   | 1   | 1   | 1   | 1   | 1   | 1   | 1   | 1   | 1   |
| Cap, veh/h   | 66  | 171   | 194   | 265   | 105   | 44  | 245   | 825   | 682   | 133   | 682   | 21  |
| Arrive On Green  | 0.13  | 0.13  | 0.13  | 0.23  | 0.23  | 0.23  | 0.14  | 0.44  | 0.44  | 0.07  | 0.38  | 0.38  |
| Sat Flow, veh/h  | 516   | 1343  | 1530  | 1144  | 453   | 191   | 1795  | 1885  | 1558  | 1795  | 1816  | 57  |
| Grp Volume(v), veh/h   | 90  | 0   | 155   | 375   | 0   | 0   | 215   | 615   | 200   | 95  | 0   | 660   |
| Grp Sat Flow(s),veh/h/ln   | 1859  | 0   | 1530  | 1788  | 0   | 0   | 1795  | 1885  | 1558  | 1795  | 0   | 1873  |
| Q Serve(g_s), s  | 5.2   | 0.0   | 11.4  | 23.7  | 0.0   | 0.0   | 13.7  | 31.6  | 9.6   | 6.0   | 0.0   | 39.5  |
| Cycle Q Clear(g_c), s  | 5.2   | 0.0   | 11.4  | 23.7  | 0.0   | 0.0   | 13.7  | 31.6  | 9.6   | 6.0   | 0.0   | 39.5  |
| Prop In Lane   | 0.28  |   | 1.00  | 0.64  |   | 0.11  | 1.00  |   | 1.00  | 1.00  |   | 0.03  |
| Lane Grp Cap(c), veh/h   | 236   | 0   | 194   | 414   | 0   | 0   | 245   | 825   | 682   | 133   | 0   | 703   |
| V/C Ratio(X)   | 0.38  | 0.00  | 0.80  | 0.91  | 0.00  | 0.00  | 0.88  | 0.75  | 0.29  | 0.72  | 0.00  | 0.94  |
| Avail Cap(c_a), veh/h  | 504   | 0   | 415   | 562   | 0   | 0   | 409   | 825   | 682   | 409   | 0   | 812   |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 0.00  | 1.00  | 1.00  | 1.00  | 1.00  | 0.00  | 1.00  |
| Uniform Delay (d), s/veh   | 46.5  | 0.0   | 49.3  | 43.4  | 0.0   | 0.0   | 49.2  | 27.3  | 21.1  | 52.6  | 0.0   | 35.0  |
| Incr Delay (d2), s/veh   | 0.4   | 0.0   | 2.8   | 12.6  | 0.0   | 0.0   | 6.0   | 3.3   | 0.1   | 2.7   | 0.0   | 16.2  |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 2.4   | 0.0   | 4.4   | 11.9  | 0.0   | 0.0   | 6.4   | 14.3  | 3.4   | 2.8   | 0.0   | 20.8  |
| Unsig. Movement Delay, s/veh   |   |   |   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 46.9  | 0.0   | 52.1  | 56.1  | 0.0   | 0.0   | 55.2  | 30.5  | 21.2  | 55.3  | 0.0   | 51.2  |
| LnGrp LOS  | D   |   | D   | E   |   |   | E   | C   | C   | E   |   | D   |
| Approach Vol, veh/h  | 245   |   |   | 375   |   |   | 1030  |   |   | 755   |   |   |
| Approach Delay, s/veh  | 50.2  |   |   | 56.1  |   |   | 33.9  |   |   | 51.7  |   |   |
| Approach LOS   | D   |   |   | E   |   |   | C   |   |   | D   |   |   |
| Timer - Assigned Phs   | 2   |   | 3   |   | 4   |   | 6   |   | 7   |   | 8   |   |
| Phs Duration (G+Y+Rc), s   | 30.4  |   | 19.4  |   | 48.2  |   | 18.3  |   | 12.1  |   | 55.5  |   |
| Change Period (Y+Rc), s  | 3.5   |   | 3.5   |   | * 4.6   |   | 3.5   |   | 3.5   |   | * 4.6   |   |
| Max Green Setting (Gmax), s  | 36.5  |   | 26.5  |   | * 50  |   | 31.5  |   | 26.5  |   | * 50  |   |
| Max Q Clear Time (g_c+I1), s   | 25.7  |   | 15.7  |   | 41.5  |   | 13.4  |   | 8.0   |   | 33.6  |   |
| Green Ext Time (p_c), s  | 1.2   |   | 0.2   |   | 2.1   |   | 0.5   |   | 0.1   |   | 2.6   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   | 44.6  |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS  | D   |   |   |   |   |   |   |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| * HCM 7th computational engine requires equal clearance times for the phases crossing the barrier. |   |   |   |   |   |   |   |   |   |   |   |   |

# HCM 7th Signalized Intersection Summary

## 3: Norwood Avenue & WB 80 On-Ramp/WB 80 Off-Ramp

Future PM Road Diet

|   |  |  |  |  |  |  |  |  |  |  |  |  |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement  | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations   |   |   |   |  |  |  |  |  |  |   |  |  |
| Traffic Volume (veh/h)  | 0   | 0   | 0   | 285   | 0   | 325   | 415   | 855   | 0   | 0   | 630   | 505   |
| Future Volume (veh/h)   | 0   | 0   | 0   | 285   | 0   | 325   | 415   | 855   | 0   | 0   | 630   | 505   |
| Initial Q (Qb), veh   |   |   |   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.   |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)   |   |   |   | 1.00  |   | 1.00  | 1.00  |   | 1.00  | 1.00  |   | 1.00  |
| Parking Bus, Adj  |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach   |   |   |   | No  |   |   | No  |   |   | No  |   |   |
| Adj Sat Flow, veh/h/ln  |   |   |   | 1885  | 1885  | 1885  | 1885  | 1885  | 0   | 0   | 1885  | 1885  |
| Adj Flow Rate, veh/h  |   |   |   | 285   | 0   | 0   | 415   | 855   | 0   | 0   | 630   | 0   |
| Peak Hour Factor  |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %  |   |   |   | 1   | 1   | 1   | 1   | 1   | 0   | 0   | 1   | 1   |
| Cap, veh/h  |   |   |   | 634   | 0   |   | 497   | 2265  | 0   | 0   | 1001  |   |
| Arrive On Green   |   |   |   | 0.18  | 0.00  | 0.00  | 0.28  | 0.63  | 0.00  | 0.00  | 0.28  | 0.00  |
| Sat Flow, veh/h   |   |   |   | 3591  | 0   | 1598  | 1795  | 3676  | 0   | 0   | 3676  | 1598  |
| Grp Volume(v), veh/h  |   |   |   | 285   | 0   | 0   | 415   | 855   | 0   | 0   | 630   | 0   |
| Grp Sat Flow(s),veh/h/ln  |   |   |   | 1795  | 0   | 1598  | 1795  | 1791  | 0   | 0   | 1791  | 1598  |
| Q Serve(g_s), s   |   |   |   | 3.3   | 0.0   | 0.0   | 10.0  | 5.3   | 0.0   | 0.0   | 7.1   | 0.0   |
| Cycle Q Clear(g_c), s   |   |   |   | 3.3   | 0.0   | 0.0   | 10.0  | 5.3   | 0.0   | 0.0   | 7.1   | 0.0   |
| Prop In Lane  |   |   |   | 1.00  |   | 1.00  | 1.00  |   | 0.00  | 0.00  |   | 1.00  |
| Lane Grp Cap(c), veh/h  |   |   |   | 634   | 0   |   | 497   | 2265  | 0   | 0   | 1001  |   |
| V/C Ratio(X)  |   |   |   | 0.45  | 0.00  |   | 0.84  | 0.38  | 0.00  | 0.00  | 0.63  |   |
| Avail Cap(c_a), veh/h   |   |   |   | 2808  | 0   |   | 1033  | 2738  | 0   | 0   | 2738  |   |
| HCM Platoon Ratio   |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)  |   |   |   | 1.00  | 0.00  | 0.00  | 1.00  | 1.00  | 0.00  | 0.00  | 1.00  | 0.00  |
| Uniform Delay (d), s/veh  |   |   |   | 17.0  | 0.0   | 0.0   | 15.7  | 4.1   | 0.0   | 0.0   | 14.5  | 0.0   |
| Incr Delay (d2), s/veh  |   |   |   | 0.2   | 0.0   | 0.0   | 2.8   | 0.1   | 0.0   | 0.0   | 0.5   | 0.0   |
| Initial Q Delay(d3), s/veh  |   |   |   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln  |   |   |   | 1.2   | 0.0   | 0.0   | 3.6   | 0.8   | 0.0   | 0.0   | 2.5   | 0.0   |
| Unsig. Movement Delay, s/veh  |   |   |   |   |   | 30.70   |   |   |   |   |   | 25.10   |
| LnGrp Delay(d), s/veh   |   |   |   | 17.1  | 0.0   | 30.7  | 18.5  | 4.2   | 0.0   | 0.0   | 15.0  | 25.1  |
| LnGrp LOS   |   |   |   | B   |   | C   | B   | A   |   |   | B   | C   |
| Approach Vol, veh/h   |   |   |   |   | 450   |   |   | 1270  |   |   | 885   |   |
| Approach Delay, s/veh   |   |   |   |   | 22.1  |   |   | 8.8   |   |   | 17.9  |   |
| Approach LOS  |   |   |   |   | C   |   |   | A   |   |   | B   |   |
| Timer - Assigned Phs  | 1   | 2   |   | 4   |   | 6   |   |   |   |   |   |   |
| Phs Duration (G+Y+Rc), s  | 16.2  | 17.7  |   | 12.1  |   | 33.9  |   |   |   |   |   |   |
| Change Period (Y+Rc), s   | 3.5   | 4.8   |   | 4.0   |   | 4.8   |   |   |   |   |   |   |
| Max Green Setting (Gmax), s   | 26.5  | 35.2  |   | 36.0  |   | 35.2  |   |   |   |   |   |   |
| Max Q Clear Time (g_c+I1), s  | 12.0  | 9.1   |   | 5.3   |   | 7.3   |   |   |   |   |   |   |
| Green Ext Time (p_c), s   | 0.8   | 3.8   |   | 0.5   |   | 5.0   |   |   |   |   |   |   |
| <b>Intersection Summary</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh  |   |   |   | 14.2  |   |   |   |   |   |   |   |   |
| HCM 7th LOS   |   |   |   | B   |   |   |   |   |   |   |   |   |
| <b>Notes</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| User approved volume balancing among the lanes for turning movement.  |   |   |   |   |   |   |   |   |   |   |   |   |
| Unsignalized Delay for [WBR, SBR] is included in calculations of the approach delay and intersection delay. |   |   |   |   |   |   |   |   |   |   |   |   |

# HCM 7th Signalized Intersection Summary

## 4: Norwood Avenue & EB 80 Off-Ramp/EB 80 On-Ramp

Future PM Road Diet

|  |  |  |  |  |  |  |  |  |  |  |  |  |
|--|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |  |  |  |   |   |   |   |  |  |  |  |  |
| Traffic Volume (veh/h)   | 515   | 15  | 420   | 0   | 0   | 0   | 0   | 750   | 285   | 305   | 610   | 0   |
| Future Volume (veh/h)  | 515   | 15  | 420   | 0   | 0   | 0   | 0   | 750   | 285   | 305   | 610   | 0   |
| Initial Q (Qb), veh  | 0   | 0   | 0   |   |   |   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 1.00  |   |   |   | 1.00  |   | 1.00  | 1.00  |   | 1.00  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   |   |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1856  | 1856  | 1856  |   |   |   | 0   | 1870  | 1870  | 1885  | 1885  | 0   |
| Adj Flow Rate, veh/h   | 526   | 0   | 0   |   |   |   | 0   | 750   | 0   | 305   | 610   | 0   |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 3   | 3   | 3   |   |   |   | 0   | 2   | 2   | 1   | 1   | 0   |
| Cap, veh/h   | 728   | 0   |   |   |   |   | 0   | 1123  |   | 382   | 2164  | 0   |
| Arrive On Green  | 0.21  | 0.00  | 0.00  |   |   |   | 0.00  | 0.32  | 0.00  | 0.21  | 0.60  | 0.00  |
| Sat Flow, veh/h  | 3534  | 0   | 1572  |   |   |   | 0   | 3647  | 1585  | 1795  | 3676  | 0   |
| Grp Volume(v), veh/h   | 526   | 0   | 0   |   |   |   | 0   | 750   | 0   | 305   | 610   | 0   |
| Grp Sat Flow(s),veh/h/ln   | 1767  | 0   | 1572  |   |   |   | 0   | 1777  | 1585  | 1795  | 1791  | 0   |
| Q Serve(g_s), s  | 6.4   | 0.0   | 0.0   |   |   |   | 0.0   | 8.5   | 0.0   | 7.5   | 3.8   | 0.0   |
| Cycle Q Clear(g_c), s  | 6.4   | 0.0   | 0.0   |   |   |   | 0.0   | 8.5   | 0.0   | 7.5   | 3.8   | 0.0   |
| Prop In Lane   | 1.00  |   | 1.00  |   |   |   | 0.00  |   | 1.00  | 1.00  |   | 0.00  |
| Lane Grp Cap(c), veh/h   | 728   | 0   |   |   |   |   | 0   | 1123  |   | 382   | 2164  | 0   |
| V/C Ratio(X)   | 0.72  | 0.00  |   |   |   |   | 0.00  | 0.67  |   | 0.80  | 0.28  | 0.00  |
| Avail Cap(c_a), veh/h  | 2742  | 0   |   |   |   |   | 0   | 2695  |   | 1025  | 2717  | 0   |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  |   |   |   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 0.00  |   |   |   | 0.00  | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  |
| Uniform Delay (d), s/veh   | 17.2  | 0.0   | 0.0   |   |   |   | 0.0   | 13.8  | 0.0   | 17.3  | 4.4   | 0.0   |
| Incr Delay (d2), s/veh   | 0.5   | 0.0   | 0.0   |   |   |   | 0.0   | 0.5   | 0.0   | 2.9   | 0.1   | 0.0   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   |   |   |   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 2.3   | 0.0   | 0.0   |   |   |   | 0.0   | 2.7   | 0.0   | 3.0   | 0.8   | 0.0   |
| Unsig. Movement Delay, s/veh   |   |   | 25.00   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 17.7  | 0.0   | 25.0  |   |   |   | 0.0   | 14.3  | 0.0   | 20.2  | 4.4   | 0.0   |
| LnGrp LOS  | B   |   | C   |   |   |   |   | B   |   | C   | A   |   |
| Approach Vol, veh/h  |   | 736   |   |   |   |   |   | 750   |   |   | 915   |   |
| Approach Delay, s/veh  |   | 19.8  |   |   |   |   |   | 14.3  |   |   | 9.7   |   |
| Approach LOS   |   | B   |   |   |   |   |   | B   |   |   | A   |   |
| Timer - Assigned Phs   |   | 2   |   |   | 5   | 6   |   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s   |   | 32.8  |   |   | 13.4  | 19.5  |   | 13.6  |   |   |   |   |
| Change Period (Y+Rc), s  |   | 4.8   |   |   | 3.5   | 4.8   |   | 4.0   |   |   |   |   |
| Max Green Setting (Gmax), s  |   | 35.2  |   |   | 26.5  | 35.2  |   | 36.0  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s   |   | 5.8   |   |   | 9.5   | 10.5  |   | 8.4   |   |   |   |   |
| Green Ext Time (p_c), s  |   | 3.7   |   |   | 0.6   | 4.2   |   | 1.0   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   |   |   | 14.2  |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS  |   |   | B   |   |   |   |   |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| User approved volume balancing among the lanes for turning movement.                                   |   |   |   |   |   |   |   |   |   |   |   |   |
| Unsignalized Delay for [EBR] is included in calculations of the approach delay and intersection delay. |   |   |   |   |   |   |   |   |   |   |   |   |

Unsignalized Delay for [NBR] is excluded from calculations of the approach delay and intersection delay.

# HCM 7th Signalized Intersection Summary

## 5: Norwood Avenue & Harris Avenue

Future PM Road Diet

|  |  |  |  |  |  |  |  |  |  |  |  |  |
|--|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |   |  |  |   |  |  |  |  |   |  |  |  |
| Traffic Volume (veh/h)   | 230   | 25  | 50  | 40  | 15  | 155   | 30  | 715   | 30  | 85  | 815   | 130   |
| Future Volume (veh/h)  | 230   | 25  | 50  | 40  | 15  | 155   | 30  | 715   | 30  | 85  | 815   | 130   |
| Initial Q (Qb), veh  | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 0.98  | 1.00  |   | 0.97  | 1.00  |   | 0.97  | 1.00  |   | 0.97  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   | No  |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1856  | 1856  | 1856  | 1856  | 1856  | 1856  | 1885  | 1885  | 1885  | 1856  | 1856  | 1856  |
| Adj Flow Rate, veh/h   | 230   | 25  | 50  | 40  | 15  | 155   | 30  | 715   | 30  | 85  | 815   | 130   |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 3   | 3   | 3   | 3   | 3   | 3   | 1   | 1   | 1   | 3   | 3   | 3   |
| Cap, veh/h   | 285   | 31  | 365   | 162   | 61  | 191   | 105   | 787   | 33  | 155   | 868   | 713   |
| Arrive On Green  | 0.18  | 0.18  | 0.18  | 0.12  | 0.12  | 0.12  | 0.06  | 0.44  | 0.44  | 0.09  | 0.47  | 0.47  |
| Sat Flow, veh/h  | 1601  | 174   | 1537  | 1302  | 488   | 1532  | 1795  | 1794  | 75  | 1767  | 1856  | 1525  |
| Grp Volume(v), veh/h   | 255   | 0   | 50  | 55  | 0   | 155   | 30  | 0   | 745   | 85  | 815   | 130   |
| Grp Sat Flow(s),veh/h/ln   | 1775  | 0   | 1537  | 1790  | 0   | 1532  | 1795  | 0   | 1869  | 1767  | 1856  | 1525  |
| Q Serve(g_s), s  | 12.5  | 0.0   | 2.3   | 2.5   | 0.0   | 8.9   | 1.4   | 0.0   | 33.7  | 4.2   | 37.8  | 4.5   |
| Cycle Q Clear(g_c), s  | 12.5  | 0.0   | 2.3   | 2.5   | 0.0   | 8.9   | 1.4   | 0.0   | 33.7  | 4.2   | 37.8  | 4.5   |
| Prop In Lane   | 0.90  |   | 1.00  | 0.73  |   | 1.00  | 1.00  |   | 0.04  | 1.00  |   | 1.00  |
| Lane Grp Cap(c), veh/h   | 316   | 0   | 365   | 223   | 0   | 191   | 105   | 0   | 820   | 155   | 868   | 713   |
| V/C Ratio(X)   | 0.81  | 0.00  | 0.14  | 0.25  | 0.00  | 0.81  | 0.29  | 0.00  | 0.91  | 0.55  | 0.94  | 0.18  |
| Avail Cap(c_a), veh/h  | 714   | 0   | 710   | 617   | 0   | 528   | 625   | 0   | 937   | 615   | 930   | 765   |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Uniform Delay (d), s/veh   | 35.7  | 0.0   | 27.3  | 35.8  | 0.0   | 38.6  | 40.8  | 0.0   | 23.7  | 39.6  | 22.9  | 14.0  |
| Incr Delay (d2), s/veh   | 1.9   | 0.0   | 0.1   | 0.2   | 0.0   | 3.1   | 0.5   | 0.0   | 11.3  | 1.1   | 16.0  | 0.1   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 5.5   | 0.0   | 0.8   | 1.1   | 0.0   | 3.4   | 0.6   | 0.0   | 15.9  | 1.8   | 19.1  | 1.5   |
| Unsig. Movement Delay, s/veh   |   |   |   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 37.6  | 0.0   | 27.4  | 36.0  | 0.0   | 41.7  | 41.4  | 0.0   | 35.0  | 40.7  | 38.9  | 14.1  |
| LnGrp LOS  | D   |   | C   | D   |   | D   | D   |   | D   | D   | D   | B   |
| Approach Vol, veh/h  |   | 305   |   |   | 210   |   |   | 775   |   |   | 1030  |   |
| Approach Delay, s/veh  |   | 35.9  |   |   | 40.2  |   |   | 35.3  |   |   | 35.9  |   |
| Approach LOS   |   | D   |   |   | D   |   |   | D   |   |   | D   |   |
| Timer - Assigned Phs   |   | 2   | 3   | 4   |   | 6   | 7   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s   |   | 15.1  | 8.8   | 47.0  |   | 19.7  | 11.4  | 44.3  |   |   |   |   |
| Change Period (Y+Rc), s  |   | 3.8   | 3.5   | * 4.6   |   | 3.6   | 3.5   | * 4.6   |   |   |   |   |
| Max Green Setting (Gmax), s  |   | 31.2  | 31.5  | * 45  |   | 36.4  | 31.5  | * 45  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s   |   | 10.9  | 3.4   | 39.8  |   | 14.5  | 6.2   | 35.7  |   |   |   |   |
| Green Ext Time (p_c), s  |   | 0.4   | 0.0   | 2.6   |   | 1.0   | 0.1   | 2.9   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   |   |   | 36.1  |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS  |   |   | D   |   |   |   |   |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| * HCM 7th computational engine requires equal clearance times for the phases crossing the barrier. |   |   |   |   |   |   |   |   |   |   |   |   |

HCM 7th Signalized Intersection Summary  
6: Norwood Avenue & Silver Eagle Road

Future PM Road Diet

|  |  |  |  |  |  |  |   |  |  |  |  |  |
|--|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement   | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations  |  |  |   |  |  |   |  |  |   |  |  |  |
| Traffic Volume (veh/h)   | 205   | 185   | 260   | 20  | 140   | 40  | 210   | 455   | 30  | 45  | 480   | 180   |
| Future Volume (veh/h)  | 205   | 185   | 260   | 20  | 140   | 40  | 210   | 455   | 30  | 45  | 480   | 180   |
| Initial Q (Qb), veh  | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)  | 1.00  |   | 0.98  | 1.00  |   | 0.99  | 1.00  |   | 0.97  | 1.00  |   | 0.97  |
| Parking Bus, Adj   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach  |   | No  |   |   | No  |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln   | 1885  | 1885  | 1885  | 1885  | 1885  | 1885  | 1870  | 1870  | 1870  | 1885  | 1885  | 1885  |
| Adj Flow Rate, veh/h   | 205   | 185   | 260   | 20  | 140   | 40  | 210   | 455   | 30  | 45  | 480   | 180   |
| Peak Hour Factor   | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %   | 1   | 1   | 1   | 1   | 1   | 1   | 2   | 2   | 2   | 1   | 1   | 1   |
| Cap, veh/h   | 241   | 188   | 264   | 77  | 250   | 71  | 245   | 802   | 53  | 117   | 507   | 190   |
| Arrive On Green  | 0.13  | 0.27  | 0.27  | 0.04  | 0.18  | 0.18  | 0.14  | 0.46  | 0.46  | 0.07  | 0.39  | 0.39  |
| Sat Flow, veh/h  | 1795  | 699   | 982   | 1795  | 1405  | 401   | 1781  | 1732  | 114   | 1795  | 1296  | 486   |
| Grp Volume(v), veh/h   | 205   | 0   | 445   | 20  | 0   | 180   | 210   | 0   | 485   | 45  | 0   | 660   |
| Grp Sat Flow(s),veh/h/ln   | 1795  | 0   | 1681  | 1795  | 0   | 1807  | 1781  | 0   | 1846  | 1795  | 0   | 1782  |
| Q Serve(g_s), s  | 10.8  | 0.0   | 25.5  | 1.0   | 0.0   | 8.8   | 11.2  | 0.0   | 18.6  | 2.3   | 0.0   | 34.7  |
| Cycle Q Clear(g_c), s  | 10.8  | 0.0   | 25.5  | 1.0   | 0.0   | 8.8   | 11.2  | 0.0   | 18.6  | 2.3   | 0.0   | 34.7  |
| Prop In Lane   | 1.00  |   | 0.58  | 1.00  |   | 0.22  | 1.00  |   | 0.06  | 1.00  |   | 0.27  |
| Lane Grp Cap(c), veh/h   | 241   | 0   | 452   | 77  | 0   | 321   | 245   | 0   | 854   | 117   | 0   | 697   |
| V/C Ratio(X)   | 0.85  | 0.00  | 0.98  | 0.26  | 0.00  | 0.56  | 0.86  | 0.00  | 0.57  | 0.38  | 0.00  | 0.95  |
| Avail Cap(c_a), veh/h  | 491   | 0   | 452   | 491   | 0   | 494   | 395   | 0   | 854   | 398   | 0   | 742   |
| HCM Platoon Ratio  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)   | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 1.00  |
| Uniform Delay (d), s/veh   | 41.0  | 0.0   | 35.2  | 44.9  | 0.0   | 36.4  | 40.9  | 0.0   | 19.0  | 43.5  | 0.0   | 28.6  |
| Incr Delay (d2), s/veh   | 3.3   | 0.0   | 37.8  | 0.7   | 0.0   | 0.6   | 5.7   | 0.0   | 0.6   | 0.8   | 0.0   | 20.0  |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln   | 4.9   | 0.0   | 14.9  | 0.5   | 0.0   | 3.9   | 5.1   | 0.0   | 7.4   | 1.1   | 0.0   | 18.1  |
| Unsig. Movement Delay, s/veh   |   |   |   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh  | 44.3  | 0.0   | 73.0  | 45.6  | 0.0   | 37.0  | 46.6  | 0.0   | 19.5  | 44.2  | 0.0   | 48.6  |
| LnGrp LOS  | D   |   | E   | D   |   | D   | D   |   | B   | D   |   | D   |
| Approach Vol, veh/h  |   | 650   |   |   | 200   |   |   | 695   |   |   | 705   |   |
| Approach Delay, s/veh  |   | 64.0  |   |   | 37.8  |   |   | 27.7  |   |   | 48.3  |   |
| Approach LOS   |   | E   |   |   | D   |   |   | C   |   |   | D   |   |
| Timer - Assigned Phs   | 1   | 2   | 3   | 4   | 5   | 6   | 7   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s   | 16.5  | 21.2  | 16.8  | 42.5  | 7.7   | 30.0  | 9.8   | 49.5  |   |   |   |   |
| Change Period (Y+Rc), s  | 3.5   | * 3.9   | 3.5   | * 4.6   | 3.5   | 3.9   | 3.5   | * 4.6   |   |   |   |   |
| Max Green Setting (Gmax), s  | 26.5  | * 27  | 21.5  | * 40  | 26.5  | 26.1  | 21.5  | * 40  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s   | 12.8  | 10.8  | 13.2  | 36.7  | 3.0   | 27.5  | 4.3   | 20.6  |   |   |   |   |
| Green Ext Time (p_c), s  | 0.2   | 0.5   | 0.2   | 1.2   | 0.0   | 0.0   | 0.0   | 1.7   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh   |   |   | 45.6  |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS  |   |   | D   |   |   |   |   |   |   |   |   |   |
| <b>Notes</b>   |   |   |   |   |   |   |   |   |   |   |   |   |
| * HCM 7th computational engine requires equal clearance times for the phases crossing the barrier. |   |   |   |   |   |   |   |   |   |   |   |   |

# HCM 7th Signalized Intersection Summary

## 33: Norwood Avenue & Morey Avenue

Future PM Road Diet

|                              |  |  |  |  |  |  |   |  |  |  |  |  |
|------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement                     | EBL   | EBT   | EBR   | WBL   | WBT   | WBR   | NBL   | NBT   | NBR   | SBL   | SBT   | SBR   |
| Lane Configurations          |   |  |   |   |  |   |  |  |   |  |  |   |
| Traffic Volume (veh/h)       | 45  | 1   | 23  | 5   | 1   | 5   | 45  | 654   | 1   | 1   | 814   | 90  |
| Future Volume (veh/h)        | 45  | 1   | 23  | 5   | 1   | 5   | 45  | 654   | 1   | 1   | 814   | 90  |
| Initial Q (Qb), veh          | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   |
| Lane Width Adj.              | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Ped-Bike Adj(A_pbT)          | 1.00  |   | 1.00  | 1.00  |   | 1.00  | 1.00  |   | 1.00  | 1.00  |   | 1.00  |
| Parking Bus, Adj             | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Work Zone On Approach        |   | No  |   |   | No  |   |   | No  |   |   | No  |   |
| Adj Sat Flow, veh/h/ln       | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  | 1870  |
| Adj Flow Rate, veh/h         | 45  | 1   | 23  | 5   | 1   | 5   | 45  | 654   | 1   | 1   | 814   | 90  |
| Peak Hour Factor             | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Percent Heavy Veh, %         | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   |
| Cap, veh/h                   | 64  | 1   | 33  | 11  | 2   | 11  | 79  | 1153  | 2   | 3   | 950   | 105   |
| Arrive On Green              | 0.06  | 0.06  | 0.06  | 0.01  | 0.01  | 0.01  | 0.04  | 0.62  | 0.62  | 0.00  | 0.57  | 0.57  |
| Sat Flow, veh/h              | 1116  | 25  | 571   | 770   | 154   | 770   | 1781  | 1867  | 3   | 1781  | 1655  | 183   |
| Grp Volume(v), veh/h         | 69  | 0   | 0   | 11  | 0   | 0   | 45  | 0   | 655   | 1   | 0   | 904   |
| Grp Sat Flow(s),veh/h/ln     | 1712  | 0   | 0   | 1693  | 0   | 0   | 1781  | 0   | 1870  | 1781  | 0   | 1837  |
| Q Serve(g_s), s              | 2.3   | 0.0   | 0.0   | 0.4   | 0.0   | 0.0   | 1.4   | 0.0   | 12.0  | 0.0   | 0.0   | 24.0  |
| Cycle Q Clear(g_c), s        | 2.3   | 0.0   | 0.0   | 0.4   | 0.0   | 0.0   | 1.4   | 0.0   | 12.0  | 0.0   | 0.0   | 24.0  |
| Prop In Lane                 | 0.65  |   | 0.33  | 0.45  |   | 0.45  | 1.00  |   | 0.00  | 1.00  |   | 0.10  |
| Lane Grp Cap(c), veh/h       | 99  | 0   | 0   | 24  | 0   | 0   | 79  | 0   | 1154  | 3   | 0   | 1055  |
| V/C Ratio(X)                 | 0.70  | 0.00  | 0.00  | 0.46  | 0.00  | 0.00  | 0.57  | 0.00  | 0.57  | 0.33  | 0.00  | 0.86  |
| Avail Cap(c_a), veh/h        | 736   | 0   | 0   | 728   | 0   | 0   | 153   | 0   | 1511  | 153   | 0   | 1485  |
| HCM Platoon Ratio            | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  | 1.00  |
| Upstream Filter(I)           | 1.00  | 0.00  | 0.00  | 1.00  | 0.00  | 0.00  | 1.00  | 0.00  | 1.00  | 1.00  | 0.00  | 1.00  |
| Uniform Delay (d), s/veh     | 26.9  | 0.0   | 0.0   | 28.5  | 0.0   | 0.0   | 27.2  | 0.0   | 6.6   | 29.0  | 0.0   | 10.4  |
| Incr Delay (d2), s/veh       | 8.5   | 0.0   | 0.0   | 13.5  | 0.0   | 0.0   | 6.3   | 0.0   | 0.4   | 52.5  | 0.0   | 3.7   |
| Initial Q Delay(d3), s/veh   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| %ile BackOfQ(50%),veh/ln     | 1.1   | 0.0   | 0.0   | 0.2   | 0.0   | 0.0   | 0.7   | 0.0   | 3.0   | 0.1   | 0.0   | 8.2   |
| Unsig. Movement Delay, s/veh |   |   |   |   |   |   |   |   |   |   |   |   |
| LnGrp Delay(d), s/veh        | 35.4  | 0.0   | 0.0   | 41.9  | 0.0   | 0.0   | 33.5  | 0.0   | 7.0   | 81.5  | 0.0   | 14.1  |
| LnGrp LOS                    | D   |   |   | D   |   |   | C   |   | A   | F   |   | B   |
| Approach Vol, veh/h          |   | 69  |   |   | 11  |   |   | 700   |   |   |   | 905   |
| Approach Delay, s/veh        |   | 35.4  |   |   | 41.9  |   |   | 8.7   |   |   |   | 14.2  |
| Approach LOS                 |   | D   |   |   | D   |   |   | A   |   |   |   | B   |
| Timer - Assigned Phs         | 1   | 2   |   | 4   | 5   | 6   |   | 8   |   |   |   |   |
| Phs Duration (G+Y+Rc), s     | 4.6   | 40.4  |   | 7.9   | 7.1   | 37.9  |   | 5.3   |   |   |   |   |
| Change Period (Y+Rc), s      | 4.5   | 4.5   |   | 4.5   | 4.5   | 4.5   |   | 4.5   |   |   |   |   |
| Max Green Setting (Gmax), s  | 5.0   | 47.0  |   | 25.0  | 5.0   | 47.0  |   | 25.0  |   |   |   |   |
| Max Q Clear Time (g_c+I1), s | 2.0   | 14.0  |   | 4.3   | 3.4   | 26.0  |   | 2.4   |   |   |   |   |
| Green Ext Time (p_c), s      | 0.0   | 4.6   |   | 0.3   | 0.0   | 7.4   |   | 0.0   |   |   |   |   |
| <b>Intersection Summary</b>  |   |   |   |   |   |   |   |   |   |   |   |   |
| HCM 7th Control Delay, s/veh |   |   | 13.0  |   |   |   |   |   |   |   |   |   |
| HCM 7th LOS                  |   |   | B   |   |   |   |   |   |   |   |   |   |

Queues

1: Norwood Avenue & Bell Avenue

Future PM Road Diet



| Lane Group              | EBL  | EBT  | WBL  | WBT  | WBR  | NBL  | NBT  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 20   | 200  | 205  | 145  | 170  | 95   | 570  | 195  | 525  |
| v/c Ratio               | 0.08 | 0.73 | 0.75 | 0.32 | 0.34 | 0.52 | 0.81 | 0.72 | 0.63 |
| Control Delay (s/veh)   | 44.5 | 58.8 | 65.9 | 44.6 | 9.4  | 63.4 | 42.7 | 64.6 | 31.2 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 44.5 | 58.8 | 65.9 | 44.6 | 9.4  | 63.4 | 42.7 | 64.6 | 31.2 |
| Queue Length 50th (ft)  | 14   | 126  | 146  | 76   | 0    | 68   | 355  | 139  | 287  |
| Queue Length 95th (ft)  | 38   | 235  | 266  | 196  | 66   | 143  | #758 | 253  | 547  |
| Internal Link Dist (ft) |      | 878  |      | 976  |      |      | 1238 |      | 453  |
| Turn Bay Length (ft)    | 150  |      | 195  |      | 200  | 75   |      | 95   |      |
| Base Capacity (vph)     | 421  | 704  | 407  | 742  | 719  | 414  | 708  | 409  | 835  |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.05 | 0.28 | 0.50 | 0.20 | 0.24 | 0.23 | 0.81 | 0.48 | 0.63 |

Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.  
 Queue shown is maximum after two cycles.

Queues

2: Norwood Avenue & Jessie Avenue

Future PM Road Diet



| Lane Group              | EBT  | EBR  | WBT  | NBL  | NBT  | NBR  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 90   | 155  | 375  | 215  | 615  | 200  | 95   | 660  |
| v/c Ratio               | 0.48 | 0.52 | 0.86 | 0.80 | 0.73 | 0.26 | 0.58 | 0.91 |
| Control Delay (s/veh)   | 66.5 | 14.9 | 67.4 | 76.4 | 38.2 | 11.9 | 74.2 | 57.6 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 1.7  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 66.5 | 14.9 | 67.4 | 76.4 | 39.9 | 11.9 | 74.2 | 57.6 |
| Queue Length 50th (ft)  | 76   | 0    | 297  | 179  | 423  | 40   | 80   | 535  |
| Queue Length 95th (ft)  | 138  | 67   | #539 | 299  | 724  | 115  | 153  | #973 |
| Internal Link Dist (ft) | 758  |      | 547  |      | 632  |      |      | 1238 |
| Turn Bay Length (ft)    |      | 100  |      | 100  |      |      | 120  |      |
| Base Capacity (vph)     | 449  | 495  | 504  | 364  | 841  | 756  | 364  | 725  |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 102  | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.20 | 0.31 | 0.74 | 0.59 | 0.83 | 0.26 | 0.26 | 0.91 |

Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.  
 Queue shown is maximum after two cycles.

Queues

3: Norwood Avenue & WB 80 On-Ramp/WB 80 Off-Ramp

Future PM Road Diet



| Lane Group              | WBL  | WBT  | WBR  | NBL  | NBT  | SBT  | SBR  |
|-------------------------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 142  | 143  | 325  | 415  | 855  | 630  | 505  |
| v/c Ratio               | 0.42 | 0.42 | 0.74 | 0.71 | 0.35 | 0.58 | 0.76 |
| Control Delay (s/veh)   | 32.3 | 32.4 | 26.7 | 34.0 | 6.2  | 25.4 | 18.7 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.1  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 32.3 | 32.4 | 26.7 | 34.0 | 6.2  | 25.4 | 18.7 |
| Queue Length 50th (ft)  | 62   | 63   | 73   | 162  | 71   | 132  | 86   |
| Queue Length 95th (ft)  | 134  | 134  | 186  | #431 | 157  | 221  | 240  |
| Internal Link Dist (ft) |      | 874  |      |      | 446  | 632  |      |
| Turn Bay Length (ft)    |      |      | 50   | 175  |      |      | 75   |
| Base Capacity (vph)     | 848  | 848  | 865  | 657  | 3044 | 1746 | 894  |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 685  | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.17 | 0.17 | 0.38 | 0.63 | 0.36 | 0.36 | 0.56 |

Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.  
 Queue shown is maximum after two cycles.

Queues

4: Norwood Avenue & EB 80 Off-Ramp/EB 80 On-Ramp

Future PM Road Diet



| Lane Group              | EBL  | EBT  | EBR  | NBT  | NBR  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 263  | 267  | 420  | 750  | 285  | 305  | 610  |
| v/c Ratio               | 0.59 | 0.60 | 0.72 | 0.69 | 0.27 | 0.70 | 0.28 |
| Control Delay (s/veh)   | 31.6 | 31.7 | 20.1 | 28.1 | 1.9  | 38.3 | 8.1  |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 31.6 | 31.7 | 20.1 | 28.1 | 1.9  | 38.3 | 8.1  |
| Queue Length 50th (ft)  | 105  | 106  | 70   | 148  | 0    | 119  | 57   |
| Queue Length 95th (ft)  | 240  | 244  | 222  | 306  | 34   | 298  | 136  |
| Internal Link Dist (ft) |      | 679  |      | 657  |      |      | 446  |
| Turn Bay Length (ft)    |      |      | 50   |      | 220  | 180  |      |
| Base Capacity (vph)     | 890  | 895  | 934  | 1850 | 1355 | 703  | 3049 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.30 | 0.30 | 0.45 | 0.41 | 0.21 | 0.43 | 0.20 |

Intersection Summary

Queues

5: Norwood Avenue & Harris Avenue

Future PM Road Diet



| Lane Group              | EBT  | EBR  | WBT  | WBR  | NBL  | NBT  | SBL  | SBT  | SBR  |
|-------------------------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 255  | 50   | 55   | 155  | 30   | 745  | 85   | 815  | 130  |
| v/c Ratio               | 0.77 | 0.11 | 0.28 | 0.51 | 0.17 | 0.89 | 0.47 | 0.92 | 0.17 |
| Control Delay (s/veh)   | 55.7 | 7.4  | 48.6 | 13.9 | 47.7 | 41.7 | 53.6 | 43.4 | 11.3 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.7  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 55.7 | 7.4  | 48.6 | 13.9 | 47.7 | 42.4 | 53.6 | 43.4 | 11.3 |
| Queue Length 50th (ft)  | 157  | 0    | 33   | 0    | 18   | 422  | 53   | 501  | 27   |
| Queue Length 95th (ft)  | 255  | 26   | 80   | 63   | 52   | #804 | 109  | #867 | 71   |
| Internal Link Dist (ft) | 655  |      | 515  |      |      | 251  |      | 657  |      |
| Turn Bay Length (ft)    |      | 140  |      |      | 85   |      | 110  |      |      |
| Base Capacity (vph)     | 631  | 794  | 545  | 581  | 553  | 837  | 542  | 890  | 743  |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 13   | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.40 | 0.06 | 0.10 | 0.27 | 0.05 | 0.90 | 0.16 | 0.92 | 0.17 |

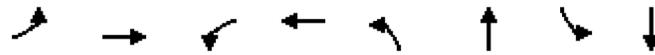
Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.  
 Queue shown is maximum after two cycles.

Queues

6: Norwood Avenue & Silver Eagle Road

Future PM Road Diet



| Lane Group              | EBL  | EBT  | WBL  | WBT  | NBL  | NBT  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 205  | 445  | 20   | 180  | 210  | 485  | 45   | 660  |
| v/c Ratio               | 0.73 | 0.83 | 0.12 | 0.64 | 0.76 | 0.52 | 0.28 | 0.93 |
| Control Delay (s/veh)   | 58.5 | 47.3 | 51.3 | 52.4 | 62.3 | 23.1 | 54.4 | 54.4 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 58.5 | 47.3 | 51.3 | 52.4 | 62.3 | 23.1 | 54.4 | 54.4 |
| Queue Length 50th (ft)  | 130  | 234  | 12   | 109  | 133  | 223  | 28   | 405  |
| Queue Length 95th (ft)  | 236  | #446 | 42   | 203  | #254 | 438  | 76   | #858 |
| Internal Link Dist (ft) |      | 710  |      | 228  |      | 480  |      | 903  |
| Turn Bay Length (ft)    | 110  |      |      |      | 95   |      | 55   |      |
| Base Capacity (vph)     | 456  | 534  | 456  | 470  | 367  | 941  | 370  | 706  |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.45 | 0.83 | 0.04 | 0.38 | 0.57 | 0.52 | 0.12 | 0.93 |

Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.  
 Queue shown is maximum after two cycles.

Queues

33: Norwood Avenue & Morey Avenue

Future PM Road Diet



| Lane Group              | EBT  | WBT  | NBL  | NBT  | SBL  | SBT  |
|-------------------------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 69   | 11   | 45   | 655  | 1    | 904  |
| v/c Ratio               | 0.37 | 0.08 | 0.39 | 0.45 | 0.01 | 0.70 |
| Control Delay (s/veh)   | 31.8 | 29.2 | 47.4 | 7.4  | 37.0 | 15.1 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay (s/veh)     | 31.8 | 29.2 | 47.4 | 7.4  | 37.0 | 15.1 |
| Queue Length 50th (ft)  | 22   | 3    | 21   | 75   | 0    | 247  |
| Queue Length 95th (ft)  | 65   | 19   | #61  | 364  | 6    | #707 |
| Internal Link Dist (ft) | 329  | 438  |      | 256  |      | 304  |
| Turn Bay Length (ft)    |      |      | 100  |      | 50   |      |
| Base Capacity (vph)     | 569  | 556  | 114  | 1453 | 114  | 1300 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.12 | 0.02 | 0.39 | 0.45 | 0.01 | 0.70 |

Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.  
 Queue shown is maximum after two cycles.

## **Section 2. Sidra Intersection Analysis Results**

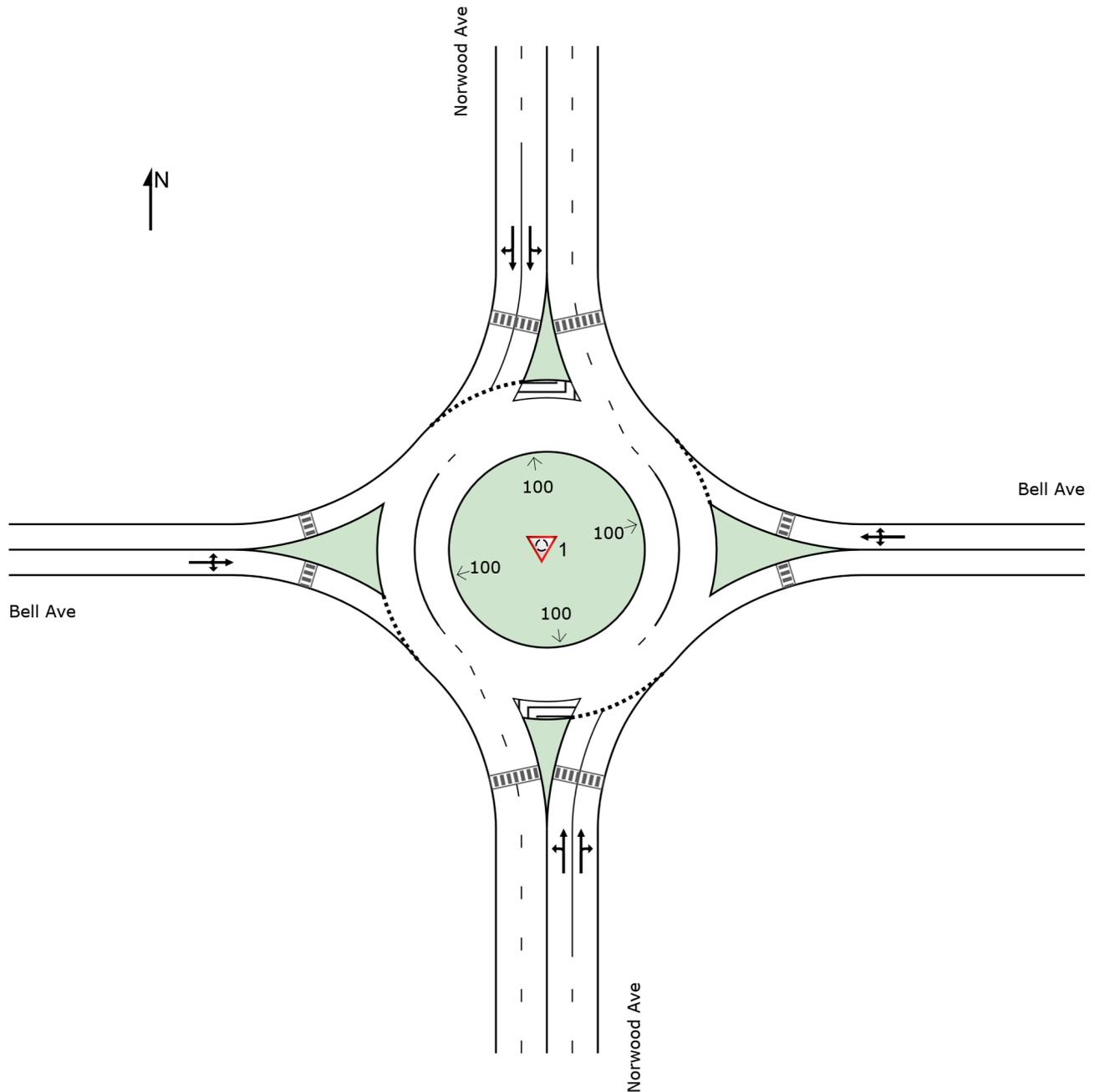
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# SITE LAYOUT

## Site: 1 [Norwood/Bell - AM No Build (Site Folder: General)]

Norwood/Bell - AM No Build  
Site Category: Future Conditions 1  
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.

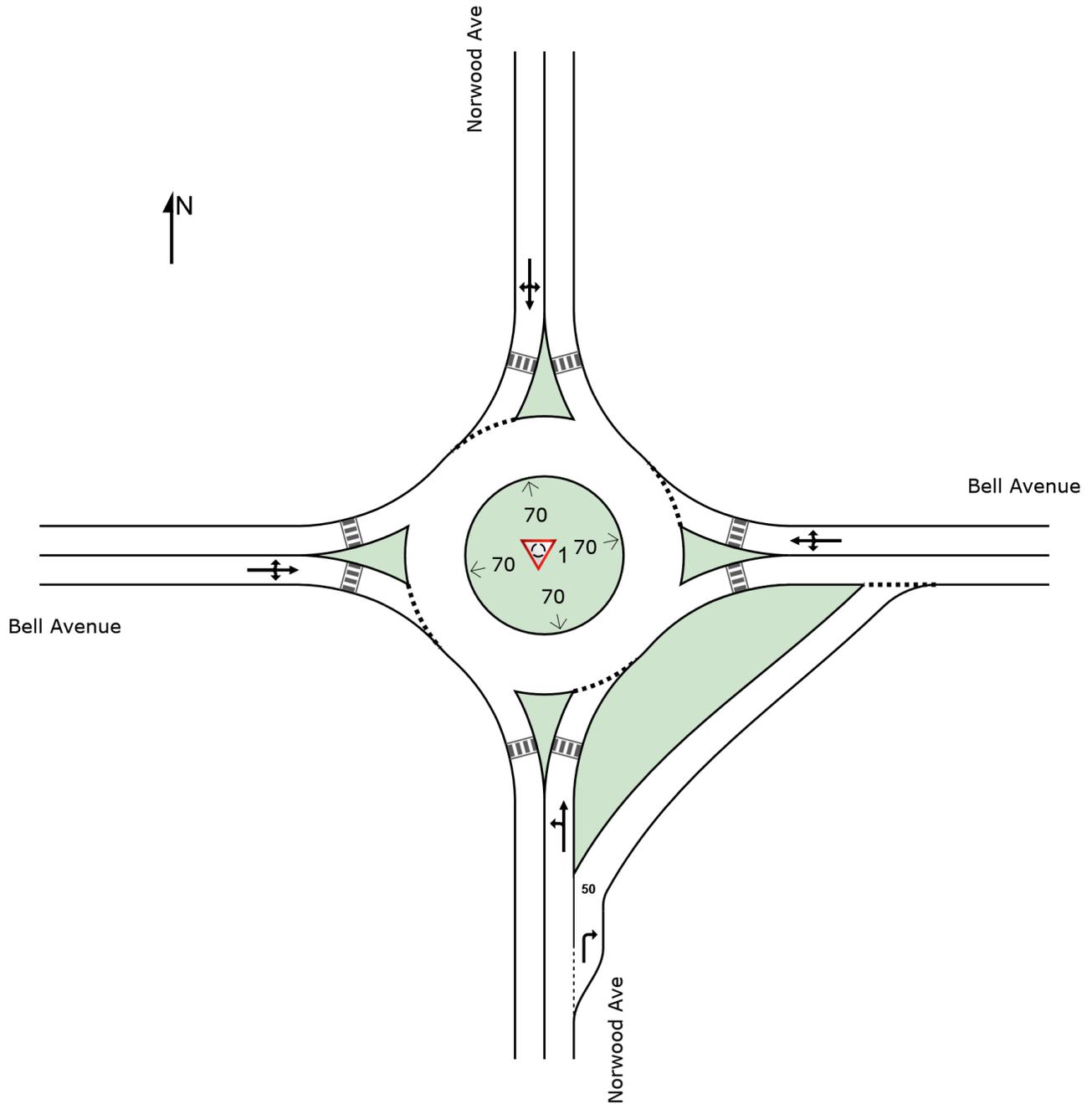


# SITE LAYOUT

## Site: 1 [Norwood/Bell - AM Road Diet (Site Folder: General)]

Norwood/Bell - AM Road Diet  
Site Category: Future Conditions 2  
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.

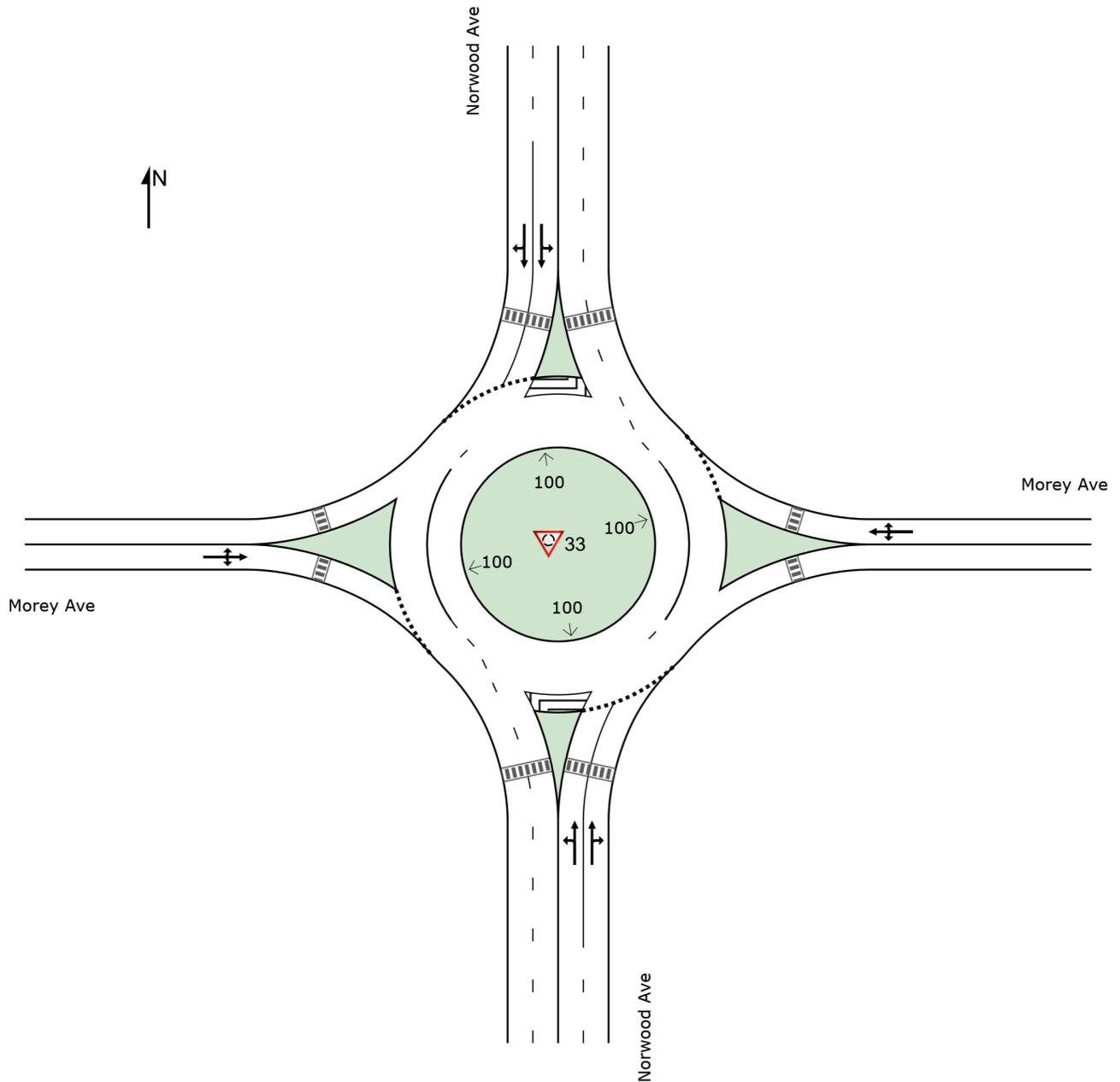


# SITE LAYOUT

## Site: 33 [Norwood/Morey - AM No Build (Site Folder: General)]

Norwood/Morey - AM No Build  
Site Category: Future Conditions 1  
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.

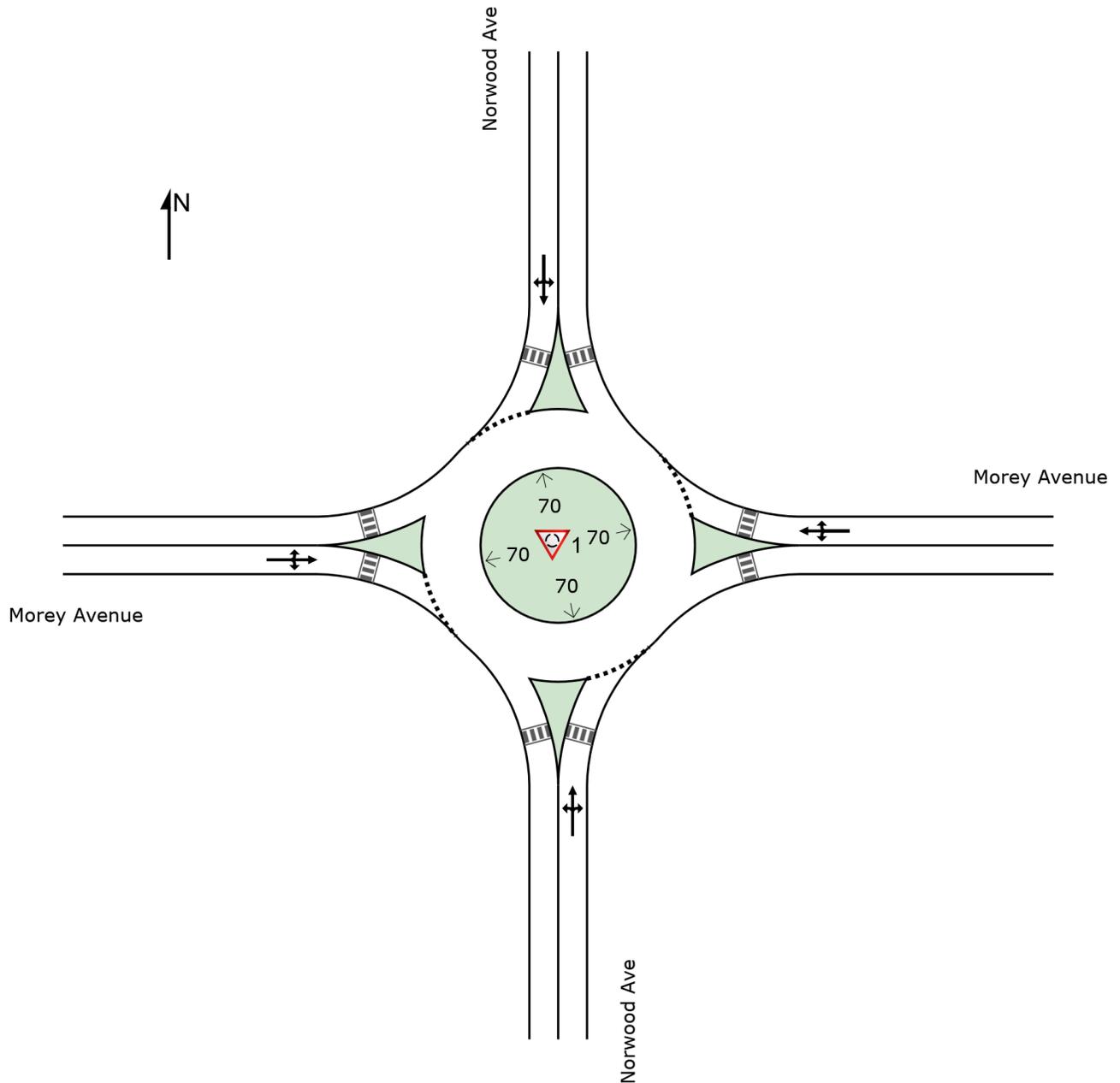


# SITE LAYOUT

## Site: 1 [Norwood/Morey - AM Road Diet (Site Folder: General)]

Norwood/Morey - AM Road Diet  
Site Category: Future Conditions 2  
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.

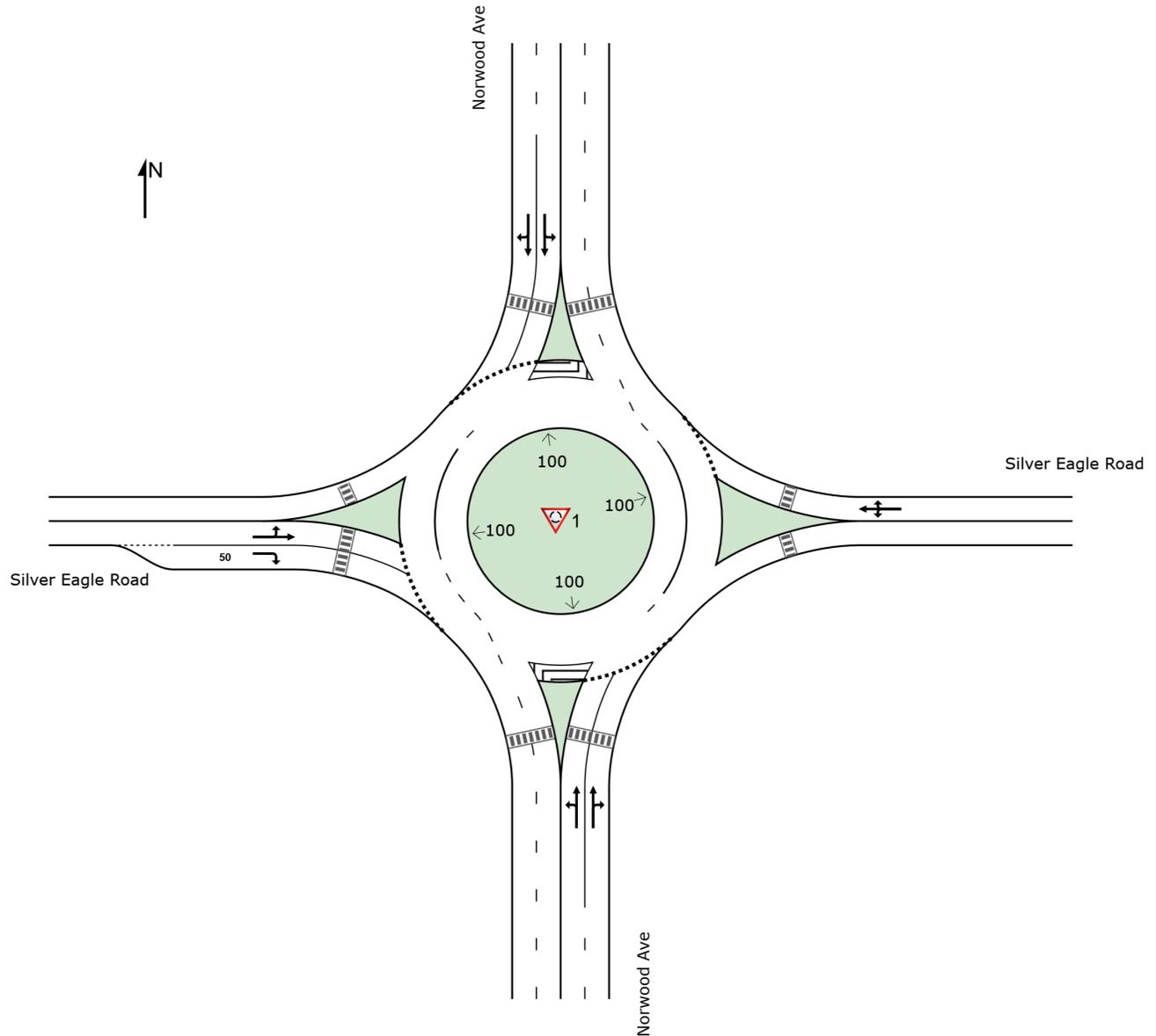


# SITE LAYOUT

Site: 1 [Norwood/Silver Eagle Road - AM No Build (Site Folder: General)]

Norwood/Silver Eagle Road - AM No Build  
Site Category: Future Conditions 1  
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



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Organisation: DKS ASSOCIATES | Licence: NETWORK / FLOATING | Created: Thursday, February 20, 2025 6:48:51 PM

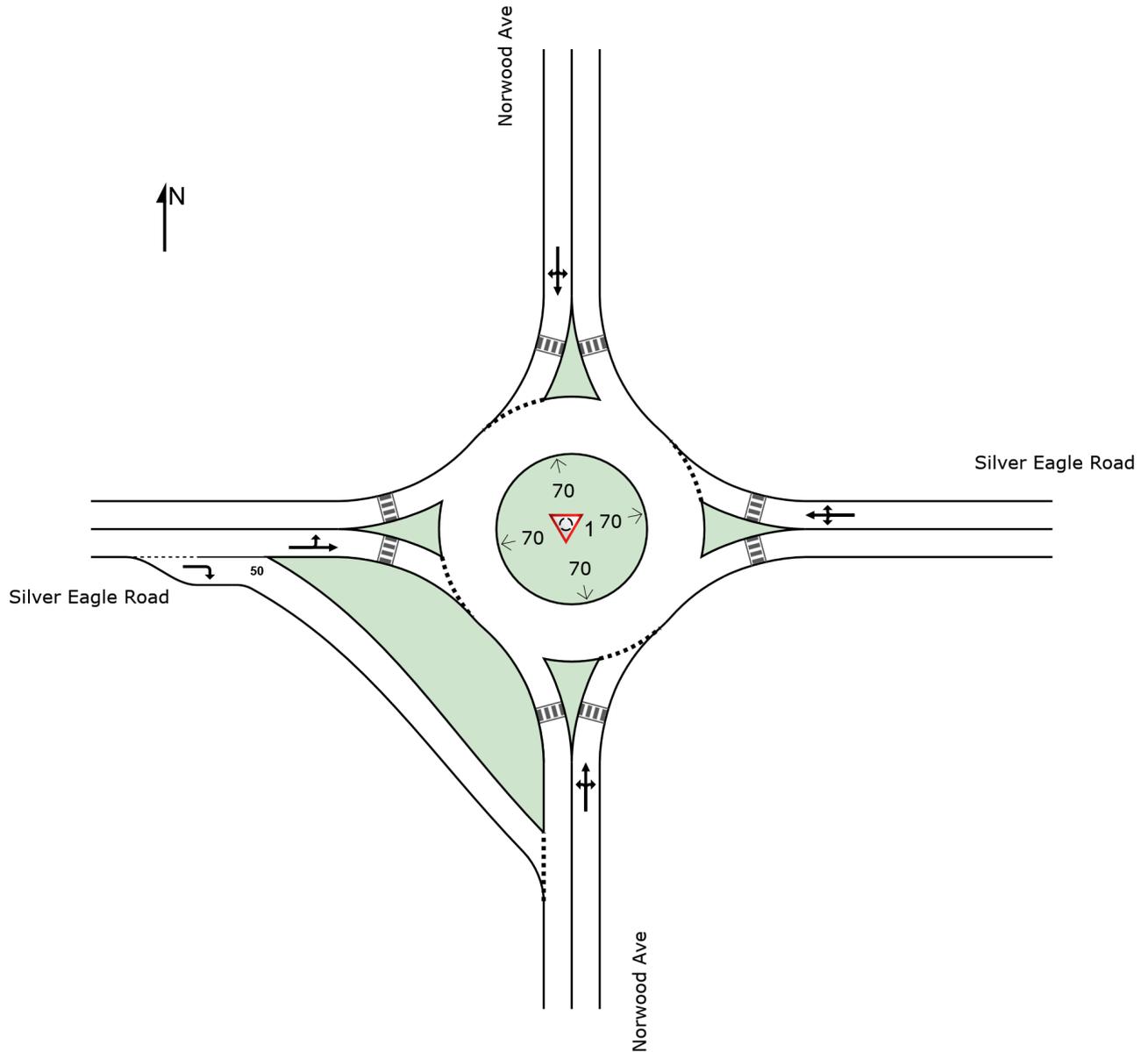
Project: L:\All-DKS\SAC\IP\24000\700s\IP24795-000 Norwood Avenue Complete Streets Transportation Plan\06 Analysis\Sidra\Future Conditions Alternatives.sip9

# SITE LAYOUT

Site: 1 [Norwood/Silver Eagle Road - AM Road Diet (Site Folder: General)]

Norwood/Silver Eagle Road - AM Road Diet  
Site Category: Future Conditions 2  
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



# MOVEMENT SUMMARY

Site: 1 [Norwood/Bell - AM No Build (Site Folder: General)]

Output produced by SIDRA INTERSECTION Version: 9.1.6.228

Norwood/Bell - AM No Build  
 Site Category: Future Conditions 1  
 Roundabout

| Vehicle Movement Performance |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
|------------------------------|------|-----------|--------------|-----|---------------|-----|-----------|-------------|------------------|-------------------|----------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows |     | Arrival Flows |     | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |          | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ] | %   | [ Total HV ]  | %   |           |             |                  | [ Veh. ]          | [ Dist ] |           |                |                     |             |
|                              |      |           | veh/h        |     | veh/h         |     | v/c       | sec         |                  | veh               | ft       |           |                |                     | mph         |
| South: Norwood Ave           |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
| 3                            | L2   | All MCs   | 70           | 3.0 | 70            | 3.0 | 0.428     | 8.5         | LOS A            | 2.2               | 55.9     | 0.57      | 0.40           | 0.57                | 25.9        |
| 8                            | T1   | All MCs   | 515          | 3.0 | 515           | 3.0 | 0.428     | 8.5         | LOS A            | 2.2               | 55.9     | 0.57      | 0.40           | 0.57                | 26.2        |
| 18                           | R2   | All MCs   | 250          | 3.0 | 250           | 3.0 | 0.428     | 8.5         | LOS A            | 2.2               | 55.9     | 0.57      | 0.40           | 0.57                | 26.1        |
| Approach                     |      |           | 835          | 3.0 | 835           | 3.0 | 0.428     | 8.5         | LOS A            | 2.2               | 55.9     | 0.57      | 0.40           | 0.57                | 26.1        |
| East: Bell Ave               |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
| 1                            | L2   | All MCs   | 220          | 4.0 | 220           | 4.0 | 0.624     | 15.4        | LOS B            | 4.7               | 121.8    | 0.77      | 0.90           | 1.31                | 23.6        |
| 6                            | T1   | All MCs   | 90           | 4.0 | 90            | 4.0 | 0.624     | 15.4        | LOS B            | 4.7               | 121.8    | 0.77      | 0.90           | 1.31                | 23.8        |
| 16                           | R2   | All MCs   | 155          | 4.0 | 155           | 4.0 | 0.624     | 15.4        | LOS B            | 4.7               | 121.8    | 0.77      | 0.90           | 1.31                | 23.7        |
| Approach                     |      |           | 465          | 4.0 | 465           | 4.0 | 0.624     | 15.4        | LOS B            | 4.7               | 121.8    | 0.77      | 0.90           | 1.31                | 23.7        |
| North: Norwood Ave           |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
| 7                            | L2   | All MCs   | 145          | 3.0 | 145           | 3.0 | 0.436     | 8.8         | LOS A            | 2.4               | 61.4     | 0.59      | 0.46           | 0.65                | 25.5        |
| 4                            | T1   | All MCs   | 635          | 3.0 | 635           | 3.0 | 0.436     | 8.8         | LOS A            | 2.4               | 61.4     | 0.59      | 0.46           | 0.65                | 26.1        |
| 14                           | R2   | All MCs   | 45           | 3.0 | 45            | 3.0 | 0.436     | 8.8         | LOS A            | 2.4               | 61.4     | 0.59      | 0.46           | 0.65                | 26.2        |
| Approach                     |      |           | 825          | 3.0 | 825           | 3.0 | 0.436     | 8.8         | LOS A            | 2.4               | 61.4     | 0.59      | 0.46           | 0.65                | 26.0        |
| West: Bell Ave               |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
| 5                            | L2   | All MCs   | 60           | 1.0 | 60            | 1.0 | 0.636     | 19.6        | LOS B            | 3.9               | 98.7     | 0.80      | 1.01           | 1.38                | 22.9        |
| 2                            | T1   | All MCs   | 150          | 1.0 | 150           | 1.0 | 0.636     | 19.6        | LOS B            | 3.9               | 98.7     | 0.80      | 1.01           | 1.38                | 23.1        |
| 12                           | R2   | All MCs   | 155          | 1.0 | 155           | 1.0 | 0.636     | 19.6        | LOS B            | 3.9               | 98.7     | 0.80      | 1.01           | 1.38                | 23.1        |
| Approach                     |      |           | 365          | 1.0 | 365           | 1.0 | 0.636     | 19.6        | LOS B            | 3.9               | 98.7     | 0.80      | 1.01           | 1.38                | 23.1        |
| All Vehicles                 |      |           | 2490         | 2.9 | 2490          | 2.9 | 0.636     | 11.5        | LOS B            | 4.7               | 121.8    | 0.65      | 0.61           | 0.85                | 25.1        |

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab).  
 Roundabout LOS Method: Same as Signalised Intersections.  
 Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.  
 LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).  
 Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).  
 Roundabout Capacity Model: US HCM 6.  
 Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).  
 Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.  
 Gap-Acceptance Capacity Formula: Sieglloch M1 implied by US HCM 6 Roundabout Capacity Model.  
 HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.  
 Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

# MOVEMENT SUMMARY

Site: 1 [Norwood/Bell - PM No Build (Site Folder: General)]

Output produced by SIDRA INTERSECTION Version: 9.1.6.228

Norwood/Bell - PM No Build  
 Site Category: Future Conditions 1  
 Roundabout

| Vehicle Movement Performance |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
|------------------------------|------|-----------|--------------|-----|---------------|-----|-----------|-------------|------------------|-------------------|--------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows |     | Arrival Flows |     | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |        | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ] | %   | [ Total HV ]  | %   |           |             |                  | [ Veh. ]          | Dist ] |           |                |                     |             |
|                              |      |           | veh/h        |     | veh/h         |     | v/c       | sec         |                  |                   | ft     |           |                |                     | mph         |
| South: Norwood Ave           |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 3                            | L2   | All MCs   | 130          | 1.0 | 130           | 1.0 | 0.403     | 7.3         | LOS A            | 2.2               | 55.7   | 0.47      | 0.29           | 0.47                | 26.1        |
| 8                            | T1   | All MCs   | 445          | 1.0 | 445           | 1.0 | 0.403     | 7.3         | LOS A            | 2.2               | 55.7   | 0.47      | 0.29           | 0.47                | 26.4        |
| 18                           | R2   | All MCs   | 335          | 1.0 | 335           | 1.0 | 0.403     | 7.3         | LOS A            | 2.2               | 55.7   | 0.47      | 0.29           | 0.47                | 26.5        |
| Approach                     |      |           | 910          | 1.0 | 910           | 1.0 | 0.403     | 7.3         | LOS A            | 2.2               | 55.7   | 0.47      | 0.29           | 0.47                | 26.4        |
| East: Bell Ave               |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 1                            | L2   | All MCs   | 300          | 2.0 | 300           | 2.0 | 0.662     | 15.6        | LOS B            | 6.1               | 155.0  | 0.79      | 0.93           | 1.39                | 23.5        |
| 6                            | T1   | All MCs   | 115          | 2.0 | 115           | 2.0 | 0.662     | 15.6        | LOS B            | 6.1               | 155.0  | 0.79      | 0.93           | 1.39                | 23.7        |
| 16                           | R2   | All MCs   | 130          | 2.0 | 130           | 2.0 | 0.662     | 15.6        | LOS B            | 6.1               | 155.0  | 0.79      | 0.93           | 1.39                | 23.6        |
| Approach                     |      |           | 545          | 2.0 | 545           | 2.0 | 0.662     | 15.6        | LOS B            | 6.1               | 155.0  | 0.79      | 0.93           | 1.39                | 23.5        |
| North: Norwood Ave           |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 7                            | L2   | All MCs   | 130          | 1.0 | 130           | 1.0 | 0.452     | 9.9         | LOS A            | 2.7               | 67.2   | 0.66      | 0.62           | 0.84                | 25.2        |
| 4                            | T1   | All MCs   | 610          | 1.0 | 610           | 1.0 | 0.452     | 9.9         | LOS A            | 2.7               | 67.2   | 0.66      | 0.62           | 0.84                | 25.8        |
| 14                           | R2   | All MCs   | 20           | 1.0 | 20            | 1.0 | 0.452     | 9.9         | LOS A            | 2.7               | 67.2   | 0.66      | 0.62           | 0.84                | 25.9        |
| Approach                     |      |           | 760          | 1.0 | 760           | 1.0 | 0.452     | 9.9         | LOS A            | 2.7               | 67.2   | 0.66      | 0.62           | 0.84                | 25.7        |
| West: Bell Ave               |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 5                            | L2   | All MCs   | 15           | 1.0 | 15            | 1.0 | 0.391     | 12.3        | LOS B            | 1.7               | 42.2   | 0.70      | 0.78           | 0.91                | 24.8        |
| 2                            | T1   | All MCs   | 90           | 1.0 | 90            | 1.0 | 0.391     | 12.3        | LOS B            | 1.7               | 42.2   | 0.70      | 0.78           | 0.91                | 25.1        |
| 12                           | R2   | All MCs   | 115          | 1.0 | 115           | 1.0 | 0.391     | 12.3        | LOS B            | 1.7               | 42.2   | 0.70      | 0.78           | 0.91                | 25.0        |
| Approach                     |      |           | 220          | 1.0 | 220           | 1.0 | 0.391     | 12.3        | LOS B            | 1.7               | 42.2   | 0.70      | 0.78           | 0.91                | 25.0        |
| All Vehicles                 |      |           | 2435         | 1.2 | 2435          | 1.2 | 0.662     | 10.4        | LOS B            | 6.1               | 155.0  | 0.62      | 0.58           | 0.83                | 25.3        |

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: Sieglach M1 implied by US HCM 6 Roundabout Capacity Model.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

# MOVEMENT SUMMARY

Site: 1 [Norwood/Bell - AM Road Diet (Site Folder: General)]

Output produced by SIDRA INTERSECTION Version: 9.1.6.228

Norwood/Bell - AM Road Diet  
 Site Category: Future Conditions 2  
 Roundabout

| Vehicle Movement Performance |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
|------------------------------|------|-----------|--------------|-----|---------------|-----|-----------|-------------|------------------|-------------------|--------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows |     | Arrival Flows |     | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |        | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ] | %   | [ Total HV ]  | %   |           |             |                  | [ Veh. veh        | Dist ] |           |                |                     |             |
| South: Norwood Ave           |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 3                            | L2   | All MCs   | 55           | 3.0 | 55            | 3.0 | 0.584     | 12.7        | LOS B            | 4.8               | 123.9  | 0.73      | 0.77           | 1.13                | 24.5        |
| 8                            | T1   | All MCs   | 445          | 3.0 | 445           | 3.0 | 0.584     | 12.7        | LOS B            | 4.8               | 123.9  | 0.73      | 0.77           | 1.13                | 24.7        |
| 18                           | R2   | All MCs   | 220          | 3.0 | 220           | 3.0 | 0.256     | 6.9         | LOS A            | 1.2               | 29.7   | 0.56      | 0.42           | 0.56                | 26.4        |
| Approach                     |      |           | 720          | 3.0 | 720           | 3.0 | 0.584     | 10.9        | LOS B            | 4.8               | 123.9  | 0.68      | 0.66           | 0.95                | 25.2        |
| East: Bell Avenue            |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 1                            | L2   | All MCs   | 135          | 4.0 | 135           | 4.0 | 0.578     | 14.5        | LOS B            | 4.3               | 111.2  | 0.78      | 0.84           | 1.19                | 23.7        |
| 6                            | T1   | All MCs   | 95           | 4.0 | 95            | 4.0 | 0.578     | 14.5        | LOS B            | 4.3               | 111.2  | 0.78      | 0.84           | 1.19                | 23.9        |
| 16                           | R2   | All MCs   | 180          | 4.0 | 180           | 4.0 | 0.578     | 14.5        | LOS B            | 4.3               | 111.2  | 0.78      | 0.84           | 1.19                | 23.9        |
| Approach                     |      |           | 410          | 4.0 | 410           | 4.0 | 0.578     | 14.5        | LOS B            | 4.3               | 111.2  | 0.78      | 0.84           | 1.19                | 23.8        |
| North: Norwood Ave           |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 7                            | L2   | All MCs   | 225          | 3.0 | 225           | 3.0 | 0.793     | 19.3        | LOS B            | 16.4              | 418.9  | 0.95      | 1.08           | 1.73                | 22.6        |
| 4                            | T1   | All MCs   | 500          | 3.0 | 500           | 3.0 | 0.793     | 19.3        | LOS B            | 16.4              | 418.9  | 0.95      | 1.08           | 1.73                | 22.9        |
| 14                           | R2   | All MCs   | 55           | 3.0 | 55            | 3.0 | 0.793     | 19.3        | LOS B            | 16.4              | 418.9  | 0.95      | 1.08           | 1.73                | 22.8        |
| Approach                     |      |           | 780          | 3.0 | 780           | 3.0 | 0.793     | 19.3        | LOS B            | 16.4              | 418.9  | 0.95      | 1.08           | 1.73                | 22.8        |
| West: Bell Avenue            |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 5                            | L2   | All MCs   | 75           | 1.0 | 75            | 1.0 | 0.667     | 21.8        | LOS C            | 4.6               | 115.5  | 0.85      | 1.03           | 1.40                | 22.1        |
| 2                            | T1   | All MCs   | 190          | 1.0 | 190           | 1.0 | 0.667     | 21.8        | LOS C            | 4.6               | 115.5  | 0.85      | 1.03           | 1.40                | 22.4        |
| 12                           | R2   | All MCs   | 100          | 1.0 | 100           | 1.0 | 0.667     | 21.8        | LOS C            | 4.6               | 115.5  | 0.85      | 1.03           | 1.40                | 22.3        |
| Approach                     |      |           | 365          | 1.0 | 365           | 1.0 | 0.667     | 21.8        | LOS C            | 4.6               | 115.5  | 0.85      | 1.03           | 1.40                | 22.3        |
| All Vehicles                 |      |           | 2275         | 2.9 | 2275          | 2.9 | 0.793     | 16.2        | LOS B            | 16.4              | 418.9  | 0.82      | 0.90           | 1.33                | 23.6        |

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab).  
 Roundabout LOS Method: Same as Signalised Intersections.  
 Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.  
 LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).  
 Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).  
 Roundabout Capacity Model: US HCM 6.  
 Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).  
 Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.  
 Gap-Acceptance Capacity Formula: Sieglloch M1 implied by US HCM 6 Roundabout Capacity Model.  
 HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.  
 Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

# MOVEMENT SUMMARY

**Site: 1 [Norwood/Bell - PM Road Diet (Site Folder: General)]**

**Output produced by SIDRA INTERSECTION Version: 9.1.6.228**

Norwood/Bell - PM Road Diet  
 Site Category: Future Conditions 2  
 Roundabout

| Vehicle Movement Performance |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
|------------------------------|------|-----------|--------------|-----|---------------|-----|-----------|-------------|------------------|-------------------|--------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows |     | Arrival Flows |     | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |        | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ] | %   | [ Total HV ]  | %   |           |             |                  | [ Veh. veh        | Dist ] |           |                |                     |             |
| South: Norwood Ave           |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 3                            | L2   | All MCs   | 95           | 1.0 | 95            | 1.0 | 0.402     | 7.7         | LOS A            | 2.1               | 52.7   | 0.54      | 0.37           | 0.54                | 25.7        |
| 8                            | T1   | All MCs   | 320          | 1.0 | 320           | 1.0 | 0.402     | 7.7         | LOS A            | 2.1               | 52.7   | 0.54      | 0.37           | 0.54                | 26.0        |
| 18                           | R2   | All MCs   | 250          | 1.0 | 250           | 1.0 | 0.253     | 6.1         | LOS A            | 1.2               | 30.8   | 0.49      | 0.33           | 0.49                | 26.6        |
| Approach                     |      |           | 665          | 1.0 | 665           | 1.0 | 0.402     | 7.1         | LOS A            | 2.1               | 52.7   | 0.52      | 0.36           | 0.52                | 26.2        |
| East: Bell Avenue            |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 1                            | L2   | All MCs   | 205          | 2.0 | 205           | 2.0 | 0.607     | 13.3        | LOS B            | 5.8               | 147.0  | 0.77      | 0.79           | 1.17                | 23.9        |
| 6                            | T1   | All MCs   | 145          | 2.0 | 145           | 2.0 | 0.607     | 13.3        | LOS B            | 5.8               | 147.0  | 0.77      | 0.79           | 1.17                | 24.2        |
| 16                           | R2   | All MCs   | 170          | 2.0 | 170           | 2.0 | 0.607     | 13.3        | LOS B            | 5.8               | 147.0  | 0.77      | 0.79           | 1.17                | 24.1        |
| Approach                     |      |           | 520          | 2.0 | 520           | 2.0 | 0.607     | 13.3        | LOS B            | 5.8               | 147.0  | 0.77      | 0.79           | 1.17                | 24.1        |
| North: Norwood Ave           |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 7                            | L2   | All MCs   | 195          | 1.0 | 195           | 1.0 | 0.840     | 25.3        | LOS C            | 15.9              | 401.1  | 1.00      | 1.36           | 2.18                | 21.4        |
| 4                            | T1   | All MCs   | 495          | 1.0 | 495           | 1.0 | 0.840     | 25.3        | LOS C            | 15.9              | 401.1  | 1.00      | 1.36           | 2.18                | 21.6        |
| 14                           | R2   | All MCs   | 30           | 1.0 | 30            | 1.0 | 0.840     | 25.3        | LOS C            | 15.9              | 401.1  | 1.00      | 1.36           | 2.18                | 21.5        |
| Approach                     |      |           | 720          | 1.0 | 720           | 1.0 | 0.840     | 25.3        | LOS C            | 15.9              | 401.1  | 1.00      | 1.36           | 2.18                | 21.5        |
| West: Bell Avenue            |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 5                            | L2   | All MCs   | 20           | 1.0 | 20            | 1.0 | 0.410     | 13.3        | LOS B            | 2.0               | 49.4   | 0.74      | 0.79           | 0.93                | 24.3        |
| 2                            | T1   | All MCs   | 115          | 1.0 | 115           | 1.0 | 0.410     | 13.3        | LOS B            | 2.0               | 49.4   | 0.74      | 0.79           | 0.93                | 24.6        |
| 12                           | R2   | All MCs   | 85           | 1.0 | 85            | 1.0 | 0.410     | 13.3        | LOS B            | 2.0               | 49.4   | 0.74      | 0.79           | 0.93                | 24.5        |
| Approach                     |      |           | 220          | 1.0 | 220           | 1.0 | 0.410     | 13.3        | LOS B            | 2.0               | 49.4   | 0.74      | 0.79           | 0.93                | 24.5        |
| All Vehicles                 |      |           | 2125         | 1.2 | 2125          | 1.2 | 0.840     | 15.4        | LOS B            | 15.9              | 401.1  | 0.77      | 0.85           | 1.29                | 23.8        |

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: Sieglloch M1 implied by US HCM 6 Roundabout Capacity Model.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

# MOVEMENT SUMMARY

**Site: 33 [Norwood/Morey - AM No Build (Site Folder: General)]**

**Output produced by SIDRA INTERSECTION Version: 9.1.6.228**

Norwood/Morey - AM No Build  
 Site Category: Future Conditions 1  
 Roundabout

| Vehicle Movement Performance |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
|------------------------------|------|-----------|--------------|-----|---------------|-----|-----------|-------------|------------------|-------------------|--------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows |     | Arrival Flows |     | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |        | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ] | %   | [ Total HV ]  | %   |           |             |                  | [ Veh. veh        | Dist ] |           |                |                     |             |
| South: Norwood Ave           |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 3                            | L2   | All MCs   | 23           | 3.0 | 23            | 3.0 | 0.360     | 6.1         | LOS A            | 2.0               | 50.6   | 0.29      | 0.12           | 0.29                | 26.8        |
| 8                            | T1   | All MCs   | 881          | 3.0 | 881           | 3.0 | 0.360     | 6.1         | LOS A            | 2.0               | 50.6   | 0.29      | 0.12           | 0.29                | 27.1        |
| 18                           | R2   | All MCs   | 1            | 3.0 | 1             | 3.0 | 0.360     | 6.1         | LOS A            | 2.0               | 50.6   | 0.29      | 0.12           | 0.29                | 27.0        |
| Approach                     |      |           | 905          | 3.0 | 905           | 3.0 | 0.360     | 6.1         | LOS A            | 2.0               | 50.6   | 0.29      | 0.12           | 0.29                | 27.1        |
| East: Morey Ave              |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 1                            | L2   | All MCs   | 5            | 1.0 | 5             | 1.0 | 0.019     | 6.4         | LOS A            | 0.1               | 1.5    | 0.59      | 0.53           | 0.59                | 26.0        |
| 6                            | T1   | All MCs   | 1            | 1.0 | 1             | 1.0 | 0.019     | 6.4         | LOS A            | 0.1               | 1.5    | 0.59      | 0.53           | 0.59                | 26.2        |
| 16                           | R2   | All MCs   | 5            | 1.0 | 5             | 1.0 | 0.019     | 6.4         | LOS A            | 0.1               | 1.5    | 0.59      | 0.53           | 0.59                | 26.2        |
| Approach                     |      |           | 11           | 1.0 | 11            | 1.0 | 0.019     | 6.4         | LOS A            | 0.1               | 1.5    | 0.59      | 0.53           | 0.59                | 26.1        |
| North: Norwood Ave           |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 7                            | L2   | All MCs   | 1            | 3.0 | 1             | 3.0 | 0.394     | 5.9         | LOS A            | 2.4               | 60.6   | 0.16      | 0.04           | 0.16                | 26.9        |
| 4                            | T1   | All MCs   | 1004         | 3.0 | 1004          | 3.0 | 0.394     | 5.9         | LOS A            | 2.4               | 60.6   | 0.16      | 0.04           | 0.16                | 27.2        |
| 14                           | R2   | All MCs   | 45           | 3.0 | 45            | 3.0 | 0.394     | 5.9         | LOS A            | 2.4               | 60.6   | 0.16      | 0.04           | 0.16                | 27.1        |
| Approach                     |      |           | 1050         | 3.0 | 1050          | 3.0 | 0.394     | 5.9         | LOS A            | 2.4               | 60.6   | 0.16      | 0.04           | 0.16                | 27.2        |
| West: Morey Ave              |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 5                            | L2   | All MCs   | 90           | 1.0 | 90            | 1.0 | 0.239     | 9.5         | LOS A            | 0.8               | 21.2   | 0.65      | 0.65           | 0.65                | 24.8        |
| 2                            | T1   | All MCs   | 1            | 1.0 | 1             | 1.0 | 0.239     | 9.5         | LOS A            | 0.8               | 21.2   | 0.65      | 0.65           | 0.65                | 25.1        |
| 12                           | R2   | All MCs   | 45           | 1.0 | 45            | 1.0 | 0.239     | 9.5         | LOS A            | 0.8               | 21.2   | 0.65      | 0.65           | 0.65                | 25.0        |
| Approach                     |      |           | 136          | 1.0 | 136           | 1.0 | 0.239     | 9.5         | LOS A            | 0.8               | 21.2   | 0.65      | 0.65           | 0.65                | 24.9        |
| All Vehicles                 |      |           | 2102         | 2.9 | 2102          | 2.9 | 0.394     | 6.2         | LOS A            | 2.4               | 60.6   | 0.25      | 0.12           | 0.25                | 27.0        |

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab).  
 Roundabout LOS Method: Same as Signalised Intersections.  
 Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.  
 LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).  
 Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).  
 Roundabout Capacity Model: US HCM 6.  
 Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).  
 Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.  
 Gap-Acceptance Capacity Formula: Sieglloch M1 implied by US HCM 6 Roundabout Capacity Model.  
 HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.  
 Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

# MOVEMENT SUMMARY

Site: 33 [Norwood/Morey - PM No Build (Site Folder: General)]

Output produced by SIDRA INTERSECTION Version: 9.1.6.228

Norwood/Morey - PM No Build  
 Site Category: Future Conditions 1  
 Roundabout

| Vehicle Movement Performance |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
|------------------------------|------|-----------|--------------|-----|---------------|-----|-----------|-------------|------------------|-------------------|--------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows |     | Arrival Flows |     | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |        | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ] | %   | [ Total HV ]  | %   |           |             |                  | [ Veh. veh        | Dist ] |           |                |                     |             |
| South: Norwood Ave           |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 3                            | L2   | All MCs   | 45           | 3.0 | 45            | 3.0 | 0.360     | 5.8         | LOS A            | 2.0               | 52.1   | 0.20      | 0.06           | 0.20                | 26.8        |
| 8                            | T1   | All MCs   | 899          | 3.0 | 899           | 3.0 | 0.360     | 5.8         | LOS A            | 2.0               | 52.1   | 0.20      | 0.06           | 0.20                | 27.2        |
| 18                           | R2   | All MCs   | 1            | 3.0 | 1             | 3.0 | 0.360     | 5.8         | LOS A            | 2.0               | 52.1   | 0.20      | 0.06           | 0.20                | 27.1        |
| Approach                     |      |           | 945          | 3.0 | 945           | 3.0 | 0.360     | 5.8         | LOS A            | 2.0               | 52.1   | 0.20      | 0.06           | 0.20                | 27.2        |
| East: Morey Ave              |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 1                            | L2   | All MCs   | 5            | 1.0 | 5             | 1.0 | 0.019     | 6.4         | LOS A            | 0.1               | 1.5    | 0.59      | 0.53           | 0.59                | 26.0        |
| 6                            | T1   | All MCs   | 1            | 1.0 | 1             | 1.0 | 0.019     | 6.4         | LOS A            | 0.1               | 1.5    | 0.59      | 0.53           | 0.59                | 26.2        |
| 16                           | R2   | All MCs   | 5            | 1.0 | 5             | 1.0 | 0.019     | 6.4         | LOS A            | 0.1               | 1.5    | 0.59      | 0.53           | 0.59                | 26.2        |
| Approach                     |      |           | 11           | 1.0 | 11            | 1.0 | 0.019     | 6.4         | LOS A            | 0.1               | 1.5    | 0.59      | 0.53           | 0.59                | 26.1        |
| North: Norwood Ave           |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 7                            | L2   | All MCs   | 1            | 3.0 | 1             | 3.0 | 0.421     | 6.5         | LOS A            | 2.6               | 66.6   | 0.23      | 0.08           | 0.23                | 26.7        |
| 4                            | T1   | All MCs   | 1009         | 3.0 | 1009          | 3.0 | 0.421     | 6.5         | LOS A            | 2.6               | 66.6   | 0.23      | 0.08           | 0.23                | 27.0        |
| 14                           | R2   | All MCs   | 90           | 3.0 | 90            | 3.0 | 0.421     | 6.5         | LOS A            | 2.6               | 66.6   | 0.23      | 0.08           | 0.23                | 26.9        |
| Approach                     |      |           | 1100         | 3.0 | 1100          | 3.0 | 0.421     | 6.5         | LOS A            | 2.6               | 66.6   | 0.23      | 0.08           | 0.23                | 27.0        |
| West: Morey Ave              |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 5                            | L2   | All MCs   | 45           | 1.0 | 45            | 1.0 | 0.122     | 7.8         | LOS A            | 0.4               | 10.2   | 0.62      | 0.62           | 0.62                | 25.3        |
| 2                            | T1   | All MCs   | 1            | 1.0 | 1             | 1.0 | 0.122     | 7.8         | LOS A            | 0.4               | 10.2   | 0.62      | 0.62           | 0.62                | 25.6        |
| 12                           | R2   | All MCs   | 23           | 1.0 | 23            | 1.0 | 0.122     | 7.8         | LOS A            | 0.4               | 10.2   | 0.62      | 0.62           | 0.62                | 25.5        |
| Approach                     |      |           | 69           | 1.0 | 69            | 1.0 | 0.122     | 7.8         | LOS A            | 0.4               | 10.2   | 0.62      | 0.62           | 0.62                | 25.4        |
| All Vehicles                 |      |           | 2125         | 2.9 | 2125          | 2.9 | 0.421     | 6.2         | LOS A            | 2.6               | 66.6   | 0.23      | 0.09           | 0.23                | 27.0        |

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: Sieglach M1 implied by US HCM 6 Roundabout Capacity Model.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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Project: L:\AI-DKS\SAC\IP\24000\700s\IP24795-000 Norwood Avenue Complete Streets Transportation Plan\06 Analysis\Sidra\Future Conditions Alternatives.sip9

# MOVEMENT SUMMARY

 Site: 1 [Norwood/Morey - AM Road Diet (Site Folder: General)]

Output produced by SIDRA INTERSECTION Version: 9.1.6.228

Norwood/Morey - AM Road Diet  
 Site Category: Future Conditions 2  
 Roundabout

| Vehicle Movement Performance |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
|------------------------------|------|-----------|--------------|-----|---------------|-----|-----------|-------------|------------------|-------------------|--------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows |     | Arrival Flows |     | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |        | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ] | %   | [ Total HV ]  | %   |           |             |                  | [ Veh. veh        | Dist ] |           |                |                     |             |
| South: Norwood Ave           |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 3                            | L2   | All MCs   | 23           | 3.0 | 23            | 3.0 | 0.579     | 9.4         | LOS A            | 4.9               | 125.7  | 0.44      | 0.19           | 0.44                | 25.5        |
| 8                            | T1   | All MCs   | 681          | 3.0 | 681           | 3.0 | 0.579     | 9.4         | LOS A            | 4.9               | 125.7  | 0.44      | 0.19           | 0.44                | 25.8        |
| 18                           | R2   | All MCs   | 1            | 3.0 | 1             | 3.0 | 0.579     | 9.4         | LOS A            | 4.9               | 125.7  | 0.44      | 0.19           | 0.44                | 25.6        |
| Approach                     |      |           | 705          | 3.0 | 705           | 3.0 | 0.579     | 9.4         | LOS A            | 4.9               | 125.7  | 0.44      | 0.19           | 0.44                | 25.7        |
| East: Morey Avenue           |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 1                            | L2   | All MCs   | 5            | 1.0 | 5             | 1.0 | 0.019     | 6.3         | LOS A            | 0.1               | 1.7    | 0.61      | 0.51           | 0.61                | 25.8        |
| 6                            | T1   | All MCs   | 1            | 1.0 | 1             | 1.0 | 0.019     | 6.3         | LOS A            | 0.1               | 1.7    | 0.61      | 0.51           | 0.61                | 26.1        |
| 16                           | R2   | All MCs   | 5            | 1.0 | 5             | 1.0 | 0.019     | 6.3         | LOS A            | 0.1               | 1.7    | 0.61      | 0.51           | 0.61                | 26.0        |
| Approach                     |      |           | 11           | 1.0 | 11            | 1.0 | 0.019     | 6.3         | LOS A            | 0.1               | 1.7    | 0.61      | 0.51           | 0.61                | 25.9        |
| North: Norwood Ave           |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 7                            | L2   | All MCs   | 1            | 3.0 | 1             | 3.0 | 0.557     | 7.8         | LOS A            | 4.9               | 126.1  | 0.24      | 0.07           | 0.24                | 25.9        |
| 4                            | T1   | All MCs   | 679          | 3.0 | 679           | 3.0 | 0.557     | 7.8         | LOS A            | 4.9               | 126.1  | 0.24      | 0.07           | 0.24                | 26.2        |
| 14                           | R2   | All MCs   | 45           | 3.0 | 45            | 3.0 | 0.557     | 7.8         | LOS A            | 4.9               | 126.1  | 0.24      | 0.07           | 0.24                | 26.1        |
| Approach                     |      |           | 725          | 3.0 | 725           | 3.0 | 0.557     | 7.8         | LOS A            | 4.9               | 126.1  | 0.24      | 0.07           | 0.24                | 26.2        |
| West: Morey Avenue           |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 5                            | L2   | All MCs   | 90           | 1.0 | 90            | 1.0 | 0.206     | 7.9         | LOS A            | 0.8               | 21.3   | 0.64      | 0.57           | 0.64                | 25.1        |
| 2                            | T1   | All MCs   | 1            | 1.0 | 1             | 1.0 | 0.206     | 7.9         | LOS A            | 0.8               | 21.3   | 0.64      | 0.57           | 0.64                | 25.4        |
| 12                           | R2   | All MCs   | 45           | 1.0 | 45            | 1.0 | 0.206     | 7.9         | LOS A            | 0.8               | 21.3   | 0.64      | 0.57           | 0.64                | 25.3        |
| Approach                     |      |           | 136          | 1.0 | 136           | 1.0 | 0.206     | 7.9         | LOS A            | 0.8               | 21.3   | 0.64      | 0.57           | 0.64                | 25.1        |
| All Vehicles                 |      |           | 1577         | 2.8 | 1577          | 2.8 | 0.579     | 8.5         | LOS A            | 4.9               | 126.1  | 0.37      | 0.17           | 0.37                | 25.9        |

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: Sieglloch M1 implied by US HCM 6 Roundabout Capacity Model.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

# MOVEMENT SUMMARY

 Site: 1 [Norwood/Morey - PM Road Diet (Site Folder: General)]

Output produced by SIDRA INTERSECTION Version: 9.1.6.228

Norwood/Morey - PM Road Diet  
 Site Category: Future Conditions 2  
 Roundabout

| Vehicle Movement Performance |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
|------------------------------|------|-----------|--------------|-----|---------------|-----|-----------|-------------|------------------|-------------------|--------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows |     | Arrival Flows |     | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |        | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ] | %   | [ Total HV ]  | %   |           |             |                  | [ Veh. veh        | Dist ] |           |                |                     |             |
| South: Norwood Ave           |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 3                            | L2   | All MCs   | 45           | 3.0 | 45            | 3.0 | 0.548     | 8.2         | LOS A            | 4.6               | 118.9  | 0.30      | 0.10           | 0.30                | 25.8        |
| 8                            | T1   | All MCs   | 654          | 3.0 | 654           | 3.0 | 0.548     | 8.2         | LOS A            | 4.6               | 118.9  | 0.30      | 0.10           | 0.30                | 26.1        |
| 18                           | R2   | All MCs   | 1            | 3.0 | 1             | 3.0 | 0.548     | 8.2         | LOS A            | 4.6               | 118.9  | 0.30      | 0.10           | 0.30                | 26.0        |
| Approach                     |      |           | 700          | 3.0 | 700           | 3.0 | 0.548     | 8.2         | LOS A            | 4.6               | 118.9  | 0.30      | 0.10           | 0.30                | 26.0        |
| East: Morey Avenue           |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 1                            | L2   | All MCs   | 5            | 1.0 | 5             | 1.0 | 0.018     | 6.0         | LOS A            | 0.1               | 1.6    | 0.59      | 0.49           | 0.59                | 25.9        |
| 6                            | T1   | All MCs   | 1            | 1.0 | 1             | 1.0 | 0.018     | 6.0         | LOS A            | 0.1               | 1.6    | 0.59      | 0.49           | 0.59                | 26.2        |
| 16                           | R2   | All MCs   | 5            | 1.0 | 5             | 1.0 | 0.018     | 6.0         | LOS A            | 0.1               | 1.6    | 0.59      | 0.49           | 0.59                | 26.1        |
| Approach                     |      |           | 11           | 1.0 | 11            | 1.0 | 0.018     | 6.0         | LOS A            | 0.1               | 1.6    | 0.59      | 0.49           | 0.59                | 26.0        |
| North: Norwood Ave           |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 7                            | L2   | All MCs   | 1            | 3.0 | 1             | 3.0 | 0.712     | 11.4        | LOS B            | 8.9               | 227.2  | 0.47      | 0.16           | 0.47                | 24.9        |
| 4                            | T1   | All MCs   | 814          | 3.0 | 814           | 3.0 | 0.712     | 11.4        | LOS B            | 8.9               | 227.2  | 0.47      | 0.16           | 0.47                | 25.2        |
| 14                           | R2   | All MCs   | 90           | 3.0 | 90            | 3.0 | 0.712     | 11.4        | LOS B            | 8.9               | 227.2  | 0.47      | 0.16           | 0.47                | 25.1        |
| Approach                     |      |           | 905          | 3.0 | 905           | 3.0 | 0.712     | 11.4        | LOS B            | 8.9               | 227.2  | 0.47      | 0.16           | 0.47                | 25.2        |
| West: Morey Avenue           |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 5                            | L2   | All MCs   | 45           | 1.0 | 45            | 1.0 | 0.121     | 7.8         | LOS A            | 0.5               | 11.5   | 0.64      | 0.61           | 0.64                | 25.1        |
| 2                            | T1   | All MCs   | 1            | 1.0 | 1             | 1.0 | 0.121     | 7.8         | LOS A            | 0.5               | 11.5   | 0.64      | 0.61           | 0.64                | 25.4        |
| 12                           | R2   | All MCs   | 23           | 1.0 | 23            | 1.0 | 0.121     | 7.8         | LOS A            | 0.5               | 11.5   | 0.64      | 0.61           | 0.64                | 25.3        |
| Approach                     |      |           | 69           | 1.0 | 69            | 1.0 | 0.121     | 7.8         | LOS A            | 0.5               | 11.5   | 0.64      | 0.61           | 0.64                | 25.2        |
| All Vehicles                 |      |           | 1685         | 2.9 | 1685          | 2.9 | 0.712     | 9.9         | LOS A            | 8.9               | 227.2  | 0.40      | 0.16           | 0.40                | 25.5        |

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: Sieglloch M1 implied by US HCM 6 Roundabout Capacity Model.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

# MOVEMENT SUMMARY

**Site: 1 [Norwood/Silver Eagle Road - AM No Build (Site Folder: General)]**

**Output produced by SIDRA INTERSECTION Version: 9.1.6.228**

Norwood/Silver Eagle Road - AM No Build  
 Site Category: Future Conditions 1  
 Roundabout

| Vehicle Movement Performance |      |           |   |     |  |     |                  |                    |                  |   |           |                |                     |                    |      |
|------------------------------|------|-----------|---|-----|--|-----|------------------|--------------------|------------------|---|-----------|----------------|---------------------|--------------------|------|
| Mov ID                       | Turn | Mov Class | Demand Flows<br>[ Total HV ]<br>veh/h % |     | Arrival Flows<br>[ Total HV ]<br>veh/h % |     | Deg. Satn<br>v/c | Aver. Delay<br>sec | Level of Service | 95% Back Of Queue<br>[ Veh. veh ]<br>[ Dist ]<br>ft | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed<br>mph |      |
| South: Norwood Ave           |      |           |   |     |  |     |                  |                    |                  |   |           |                |                     |                    |      |
| 3                            | L2   | All MCs   | 135                                     | 2.0 | 135                                      | 2.0 | 0.401            | 8.3                | LOS A            | 2.0   | 49.9      | 0.58           | 0.43                | 0.58               | 25.7 |
| 8                            | T1   | All MCs   | 600                                     | 2.0 | 600                                      | 2.0 | 0.401            | 8.3                | LOS A            | 2.0   | 49.9      | 0.58           | 0.43                | 0.58               | 26.2 |
| 18                           | R2   | All MCs   | 20                                      | 2.0 | 20                                       | 2.0 | 0.401            | 8.3                | LOS A            | 2.0   | 49.9      | 0.58           | 0.43                | 0.58               | 26.3 |
| Approach                     |      |           | 755                                     | 2.0 | 755                                      | 2.0 | 0.401            | 8.3                | LOS A            | 2.0   | 49.9      | 0.58           | 0.43                | 0.58               | 26.1 |
| East: Silver Eagle Road      |      |           |   |     |  |     |                  |                    |                  |   |           |                |                     |                    |      |
| 1                            | L2   | All MCs   | 45                                      | 3.0 | 45                                       | 3.0 | 0.375            | 12.3               | LOS B            | 1.5   | 38.7      | 0.69           | 0.76                | 0.89               | 24.7 |
| 6                            | T1   | All MCs   | 115                                     | 3.0 | 115                                      | 3.0 | 0.375            | 12.3               | LOS B            | 1.5   | 38.7      | 0.69           | 0.76                | 0.89               | 25.0 |
| 16                           | R2   | All MCs   | 45                                      | 3.0 | 45                                       | 3.0 | 0.375            | 12.3               | LOS B            | 1.5   | 38.7      | 0.69           | 0.76                | 0.89               | 24.9 |
| Approach                     |      |           | 205                                     | 3.0 | 205                                      | 3.0 | 0.375            | 12.3               | LOS B            | 1.5   | 38.7      | 0.69           | 0.76                | 0.89               | 24.9 |
| North: Norwood Ave           |      |           |   |     |  |     |                  |                    |                  |   |           |                |                     |                    |      |
| 7                            | L2   | All MCs   | 25                                      | 3.0 | 25                                       | 3.0 | 0.426            | 8.1                | LOS A            | 2.2   | 57.6      | 0.54           | 0.36                | 0.54               | 26.1 |
| 4                            | T1   | All MCs   | 665                                     | 3.0 | 665                                      | 3.0 | 0.426            | 8.1                | LOS A            | 2.2   | 57.6      | 0.54           | 0.36                | 0.54               | 26.4 |
| 14                           | R2   | All MCs   | 190                                     | 3.0 | 190                                      | 3.0 | 0.426            | 8.1                | LOS A            | 2.2   | 57.6      | 0.54           | 0.36                | 0.54               | 26.3 |
| Approach                     |      |           | 880                                     | 3.0 | 880                                      | 3.0 | 0.426            | 8.1                | LOS A            | 2.2   | 57.6      | 0.54           | 0.36                | 0.54               | 26.4 |
| West: Silver Eagle Road      |      |           |   |     |  |     |                  |                    |                  |   |           |                |                     |                    |      |
| 5                            | L2   | All MCs   | 260                                     | 5.0 | 260                                      | 5.0 | 0.553            | 14.5               | LOS B            | 3.3   | 85.3      | 0.74           | 0.85                | 1.17               | 23.6 |
| 2                            | T1   | All MCs   | 110                                     | 5.0 | 110                                      | 5.0 | 0.553            | 14.5               | LOS B            | 3.3   | 85.3      | 0.74           | 0.85                | 1.17               | 23.8 |
| 12                           | R2   | All MCs   | 195                                     | 5.0 | 195                                      | 5.0 | 0.319            | 10.2               | LOS B            | 1.2   | 32.4      | 0.65           | 0.63                | 0.72               | 25.5 |
| Approach                     |      |           | 565                                     | 5.0 | 565                                      | 5.0 | 0.553            | 13.0               | LOS B            | 3.3   | 85.3      | 0.71           | 0.77                | 1.01               | 24.3 |
| All Vehicles                 |      |           | 2405                                    | 3.2 | 2405                                     | 3.2 | 0.553            | 9.7                | LOS A            | 3.3   | 85.3      | 0.60           | 0.51                | 0.69               | 25.6 |

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: Sieglösch M1 implied by US HCM 6 Roundabout Capacity Model.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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Project: L:\All-DKS\SAC\IP\24000\700s\IP24795-000 Norwood Avenue Complete Streets Transportation Plan\06 Analysis\Sidra\Future Conditions Alternatives.sip9

# MOVEMENT SUMMARY

**Site: 1 [Norwood/Silver Eagle Road - PM No Build (Site Folder: General)]**

**Output produced by SIDRA INTERSECTION Version: 9.1.6.228**

Norwood/Silver Eagle Road - PM No Build  
 Site Category: Future Conditions 1  
 Roundabout

| Vehicle Movement Performance |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
|------------------------------|------|-----------|--------------|-----|---------------|-----|-----------|-------------|------------------|-------------------|--------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows |     | Arrival Flows |     | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |        | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ] | %   | [ Total HV ]  | %   |           |             |                  | [ Veh. veh        | Dist ] |           |                |                     |             |
| South: Norwood Ave           |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 3                            | L2   | All MCs   | 190          | 2.0 | 190           | 2.0 | 0.480     | 10.2        | LOS B            | 3.1               | 77.7   | 0.66      | 0.61           | 0.85                | 25.0        |
| 8                            | T1   | All MCs   | 625          | 2.0 | 625           | 2.0 | 0.480     | 10.2        | LOS B            | 3.1               | 77.7   | 0.66      | 0.61           | 0.85                | 25.7        |
| 18                           | R2   | All MCs   | 25           | 2.0 | 25            | 2.0 | 0.480     | 10.2        | LOS B            | 3.1               | 77.7   | 0.66      | 0.61           | 0.85                | 25.8        |
| Approach                     |      |           | 840          | 2.0 | 840           | 2.0 | 0.480     | 10.2        | LOS B            | 3.1               | 77.7   | 0.66      | 0.61           | 0.85                | 25.5        |
| East: Silver Eagle Road      |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 1                            | L2   | All MCs   | 15           | 1.0 | 15            | 1.0 | 0.328     | 11.6        | LOS B            | 1.3               | 32.0   | 0.70      | 0.75           | 0.83                | 25.1        |
| 6                            | T1   | All MCs   | 120          | 1.0 | 120           | 1.0 | 0.328     | 11.6        | LOS B            | 1.3               | 32.0   | 0.70      | 0.75           | 0.83                | 25.3        |
| 16                           | R2   | All MCs   | 40           | 1.0 | 40            | 1.0 | 0.328     | 11.6        | LOS B            | 1.3               | 32.0   | 0.70      | 0.75           | 0.83                | 25.3        |
| Approach                     |      |           | 175          | 1.0 | 175           | 1.0 | 0.328     | 11.6        | LOS B            | 1.3               | 32.0   | 0.70      | 0.75           | 0.83                | 25.3        |
| North: Norwood Ave           |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 7                            | L2   | All MCs   | 45           | 1.0 | 45            | 1.0 | 0.430     | 8.1         | LOS A            | 2.3               | 58.1   | 0.56      | 0.38           | 0.56                | 26.1        |
| 4                            | T1   | All MCs   | 610          | 1.0 | 610           | 1.0 | 0.430     | 8.1         | LOS A            | 2.3               | 58.1   | 0.56      | 0.38           | 0.56                | 26.4        |
| 14                           | R2   | All MCs   | 235          | 1.0 | 235           | 1.0 | 0.430     | 8.1         | LOS A            | 2.3               | 58.1   | 0.56      | 0.38           | 0.56                | 26.3        |
| Approach                     |      |           | 890          | 1.0 | 890           | 1.0 | 0.430     | 8.1         | LOS A            | 2.3               | 58.1   | 0.56      | 0.38           | 0.56                | 26.3        |
| West: Silver Eagle Road      |      |           |              |     |               |     |           |             |                  |                   |        |           |                |                     |             |
| 5                            | L2   | All MCs   | 280          | 1.0 | 280           | 1.0 | 0.563     | 13.1        | LOS B            | 3.9               | 98.2   | 0.73      | 0.81           | 1.14                | 24.0        |
| 2                            | T1   | All MCs   | 160          | 1.0 | 160           | 1.0 | 0.563     | 13.1        | LOS B            | 3.9               | 98.2   | 0.73      | 0.81           | 1.14                | 24.3        |
| 12                           | R2   | All MCs   | 230          | 1.0 | 230           | 1.0 | 0.323     | 9.0         | LOS A            | 1.4               | 34.3   | 0.63      | 0.57           | 0.66                | 25.9        |
| Approach                     |      |           | 670          | 1.0 | 670           | 1.0 | 0.563     | 11.7        | LOS B            | 3.9               | 98.2   | 0.70      | 0.73           | 0.97                | 24.7        |
| All Vehicles                 |      |           | 2575         | 1.3 | 2575          | 1.3 | 0.563     | 10.0        | LOS A            | 3.9               | 98.2   | 0.64      | 0.57           | 0.78                | 25.5        |

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: Sieglösch M1 implied by US HCM 6 Roundabout Capacity Model.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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Project: L:\All-DKS\SAC\IP\24000\700s\IP24795-000 Norwood Avenue Complete Streets Transportation Plan\06 Analysis\Sidra\Future Conditions Alternatives.sip9

# MOVEMENT SUMMARY

Site: 1 [Norwood/Silver Eagle Road - AM Road Diet (Site Folder: General)]

Output produced by SIDRA INTERSECTION Version: 9.1.6.228

Norwood/Silver Eagle Road - AM Road Diet  
 Site Category: Future Conditions 2  
 Roundabout

| Vehicle Movement Performance |      |           |   |     |  |     |                  |                    |                  |   |           |                |                     |                    |      |
|------------------------------|------|-----------|---|-----|--|-----|------------------|--------------------|------------------|---|-----------|----------------|---------------------|--------------------|------|
| Mov ID                       | Turn | Mov Class | Demand Flows<br>[ Total HV ]<br>veh/h % |     | Arrival Flows<br>[ Total HV ]<br>veh/h % |     | Deg. Satn<br>v/c | Aver. Delay<br>sec | Level of Service | 95% Back Of Queue<br>[ Veh. veh ]<br>[ Dist ]<br>ft | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed<br>mph |      |
| South: Norwood Ave           |      |           |   |     |  |     |                  |                    |                  |   |           |                |                     |                    |      |
| 3                            | L2   | All MCs   | 195                                     | 2.0 | 195                                      | 2.0 | 0.740            | 17.1               | LOS B            | 11.7  | 296.8     | 0.88           | 0.98                | 1.55               | 23.2 |
| 8                            | T1   | All MCs   | 475                                     | 2.0 | 475                                      | 2.0 | 0.740            | 17.1               | LOS B            | 11.7  | 296.8     | 0.88           | 0.98                | 1.55               | 23.4 |
| 18                           | R2   | All MCs   | 25                                      | 2.0 | 25                                       | 2.0 | 0.740            | 17.1               | LOS B            | 11.7  | 296.8     | 0.88           | 0.98                | 1.55               | 23.3 |
| Approach                     |      |           | 695                                     | 2.0 | 695                                      | 2.0 | 0.740            | 17.1               | LOS B            | 11.7  | 296.8     | 0.88           | 0.98                | 1.55               | 23.3 |
| East: Silver Eagle Road      |      |           |   |     |  |     |                  |                    |                  |   |           |                |                     |                    |      |
| 1                            | L2   | All MCs   | 50                                      | 3.0 | 50                                       | 3.0 | 0.392            | 13.1               | LOS B            | 1.8   | 45.8      | 0.74           | 0.78                | 0.91               | 24.2 |
| 6                            | T1   | All MCs   | 125                                     | 3.0 | 125                                      | 3.0 | 0.392            | 13.1               | LOS B            | 1.8   | 45.8      | 0.74           | 0.78                | 0.91               | 24.4 |
| 16                           | R2   | All MCs   | 30                                      | 3.0 | 30                                       | 3.0 | 0.392            | 13.1               | LOS B            | 1.8   | 45.8      | 0.74           | 0.78                | 0.91               | 24.3 |
| Approach                     |      |           | 205                                     | 3.0 | 205                                      | 3.0 | 0.392            | 13.1               | LOS B            | 1.8   | 45.8      | 0.74           | 0.78                | 0.91               | 24.4 |
| North: Norwood Ave           |      |           |   |     |  |     |                  |                    |                  |   |           |                |                     |                    |      |
| 7                            | L2   | All MCs   | 10                                      | 3.0 | 10                                       | 3.0 | 0.688            | 15.4               | LOS B            | 8.8   | 225.5     | 0.83           | 0.89                | 1.38               | 23.8 |
| 4                            | T1   | All MCs   | 420                                     | 3.0 | 420                                      | 3.0 | 0.688            | 15.4               | LOS B            | 8.8   | 225.5     | 0.83           | 0.89                | 1.38               | 24.1 |
| 14                           | R2   | All MCs   | 190                                     | 3.0 | 190                                      | 3.0 | 0.688            | 15.4               | LOS B            | 8.8   | 225.5     | 0.83           | 0.89                | 1.38               | 24.0 |
| Approach                     |      |           | 620                                     | 3.0 | 620                                      | 3.0 | 0.688            | 15.4               | LOS B            | 8.8   | 225.5     | 0.83           | 0.89                | 1.38               | 24.0 |
| West: Silver Eagle Road      |      |           |   |     |  |     |                  |                    |                  |   |           |                |                     |                    |      |
| 5                            | L2   | All MCs   | 200                                     | 5.0 | 200                                      | 5.0 | 0.390            | 8.9                | LOS A            | 1.9   | 48.8      | 0.61           | 0.51                | 0.67               | 24.9 |
| 2                            | T1   | All MCs   | 125                                     | 5.0 | 125                                      | 5.0 | 0.390            | 8.9                | LOS A            | 1.9   | 48.8      | 0.61           | 0.51                | 0.67               | 25.2 |
| 12                           | R2   | All MCs   | 270                                     | 5.0 | 270                                      | 5.0 | 0.344            | 8.7                | LOS A            | 1.6   | 41.1      | 0.62           | 0.49                | 0.62               | 25.8 |
| Approach                     |      |           | 595                                     | 5.0 | 595                                      | 5.0 | 0.390            | 8.8                | LOS A            | 1.9   | 48.8      | 0.62           | 0.50                | 0.65               | 25.3 |
| All Vehicles                 |      |           | 2115                                    | 3.2 | 2115                                     | 3.2 | 0.740            | 13.9               | LOS B            | 11.7  | 296.8     | 0.78           | 0.80                | 1.18               | 24.2 |

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: Sieglösch M1 implied by US HCM 6 Roundabout Capacity Model.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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Project: L:\All-DKS\SAC\IP\24000\700s\IP24795-000 Norwood Avenue Complete Streets Transportation Plan\06 Analysis\Sidra\Future Conditions Alternatives.sip9

# MOVEMENT SUMMARY

Site: 1 [Norwood/Silver Eagle Road - PM Road Diet (Site Folder: General)]

Output produced by SIDRA INTERSECTION Version: 9.1.6.228

Norwood/Silver Eagle Road - PM Road Diet  
 Site Category: Future Conditions 2  
 Roundabout

| Vehicle Movement Performance |      |           |   |     |  |     |                  |                    |                  |                                   |            |           |                |                     |                    |
|------------------------------|------|-----------|---|-----|--|-----|------------------|--------------------|------------------|-----------------------------------|------------|-----------|----------------|---------------------|--------------------|
| Mov ID                       | Turn | Mov Class | Demand Flows<br>[ Total HV ]<br>veh/h % |     | Arrival Flows<br>[ Total HV ]<br>veh/h % |     | Deg. Satn<br>v/c | Aver. Delay<br>sec | Level of Service | 95% Back Of Queue<br>[ Veh. veh ] | Dist<br>ft | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed<br>mph |
| South: Norwood Ave           |      |           |   |     |  |     |                  |                    |                  |                                   |            |           |                |                     |                    |
| 3                            | L2   | All MCs   | 210                                     | 2.0 | 210                                      | 2.0 | 0.811            | 22.9               | LOS C            | 14.0                              | 354.7      | 0.98      | 1.25           | 1.99                | 21.9               |
| 8                            | T1   | All MCs   | 455                                     | 2.0 | 455                                      | 2.0 | 0.811            | 22.9               | LOS C            | 14.0                              | 354.7      | 0.98      | 1.25           | 1.99                | 22.1               |
| 18                           | R2   | All MCs   | 30                                      | 2.0 | 30                                       | 2.0 | 0.811            | 22.9               | LOS C            | 14.0                              | 354.7      | 0.98      | 1.25           | 1.99                | 22.0               |
| Approach                     |      |           | 695                                     | 2.0 | 695                                      | 2.0 | 0.811            | 22.9               | LOS C            | 14.0                              | 354.7      | 0.98      | 1.25           | 1.99                | 22.0               |
| East: Silver Eagle Road      |      |           |   |     |  |     |                  |                    |                  |                                   |            |           |                |                     |                    |
| 1                            | L2   | All MCs   | 20                                      | 1.0 | 20                                       | 1.0 | 0.365            | 12.0               | LOS B            | 1.7                               | 41.9       | 0.73      | 0.75           | 0.86                | 24.6               |
| 6                            | T1   | All MCs   | 140                                     | 1.0 | 140                                      | 1.0 | 0.365            | 12.0               | LOS B            | 1.7                               | 41.9       | 0.73      | 0.75           | 0.86                | 24.9               |
| 16                           | R2   | All MCs   | 40                                      | 1.0 | 40                                       | 1.0 | 0.365            | 12.0               | LOS B            | 1.7                               | 41.9       | 0.73      | 0.75           | 0.86                | 24.8               |
| Approach                     |      |           | 200                                     | 1.0 | 200                                      | 1.0 | 0.365            | 12.0               | LOS B            | 1.7                               | 41.9       | 0.73      | 0.75           | 0.86                | 24.8               |
| North: Norwood Ave           |      |           |   |     |  |     |                  |                    |                  |                                   |            |           |                |                     |                    |
| 7                            | L2   | All MCs   | 45                                      | 1.0 | 45                                       | 1.0 | 0.760            | 18.3               | LOS B            | 12.5                              | 314.7      | 0.91      | 1.05           | 1.66                | 23.1               |
| 4                            | T1   | All MCs   | 480                                     | 1.0 | 480                                      | 1.0 | 0.760            | 18.3               | LOS B            | 12.5                              | 314.7      | 0.91      | 1.05           | 1.66                | 23.3               |
| 14                           | R2   | All MCs   | 180                                     | 1.0 | 180                                      | 1.0 | 0.760            | 18.3               | LOS B            | 12.5                              | 314.7      | 0.91      | 1.05           | 1.66                | 23.2               |
| Approach                     |      |           | 705                                     | 1.0 | 705                                      | 1.0 | 0.760            | 18.3               | LOS B            | 12.5                              | 314.7      | 0.91      | 1.05           | 1.66                | 23.3               |
| West: Silver Eagle Road      |      |           |   |     |  |     |                  |                    |                  |                                   |            |           |                |                     |                    |
| 5                            | L2   | All MCs   | 205                                     | 1.0 | 205                                      | 1.0 | 0.662            | 15.2               | LOS B            | 6.4                               | 160.9      | 0.81      | 0.90           | 1.34                | 23.5               |
| 2                            | T1   | All MCs   | 185                                     | 1.0 | 185                                      | 1.0 | 0.662            | 15.2               | LOS B            | 6.4                               | 160.9      | 0.81      | 0.90           | 1.34                | 23.7               |
| 12                           | R2   | All MCs   | 260                                     | 1.0 | 260                                      | 1.0 | 0.662            | 12.5               | LOS B            | 6.4                               | 160.9      | 0.74      | 0.78           | 1.09                | 24.5               |
| Approach                     |      |           | 650                                     | 1.0 | 650                                      | 1.0 | 0.662            | 14.1               | LOS B            | 6.4                               | 160.9      | 0.78      | 0.85           | 1.24                | 24.0               |
| All Vehicles                 |      |           | 2250                                    | 1.3 | 2250                                     | 1.3 | 0.811            | 18.0               | LOS B            | 14.0                              | 354.7      | 0.88      | 1.03           | 1.57                | 23.2               |

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: Sieglösch M1 implied by US HCM 6 Roundabout Capacity Model.

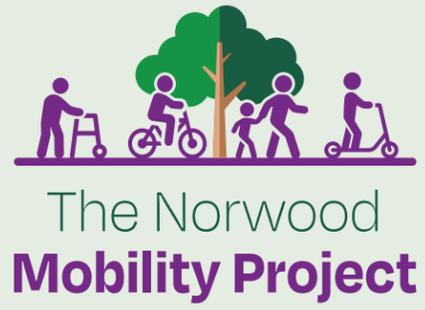
HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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Project: L:\All-DKS\SAC\IP\24000\700s\IP24795-000 Norwood Avenue Complete Streets Transportation Plan\06 Analysis\Sidra\Future Conditions Alternatives.sip9



## **C - Engagement Summaries**



# Phase 1 Engagement Materials



# The Norwood Mobility Project

## Help us develop a plan to improve safety and access on Norwood Avenue whether you are walking, biking, driving, or taking the bus!

*¡Ayúdenos a desarrollar un plan para mejorar la seguridad y el acceso en Norwood Avenue ya sea que esté caminando, en bicicleta, conduciendo o tomando el autobús!*

### Join us for a workshop to share your ideas!

*Únase a nosotros para un taller para compartir sus ideas!*

#### IN-PERSON EN PERSONA

November 18, 2024 | 18 de noviembre de 2024

6:30 PM - 8:00 PM

Robertson Community Center  
3525 Norwood Ave Sacramento

#### VIRTUAL VIRTUAL

December 9, 2024 | 9 de diciembre de 2024

6:30 PM - 7:30 PM

Via Zoom Meeting | Vía reunión de Zoom

Register at | Regístrese en: [bit.ly/norwood-register](https://bit.ly/norwood-register)

Meeting ID | ID de reunión: 899 0189 8092

Passcode | Código de acceso: Norwood

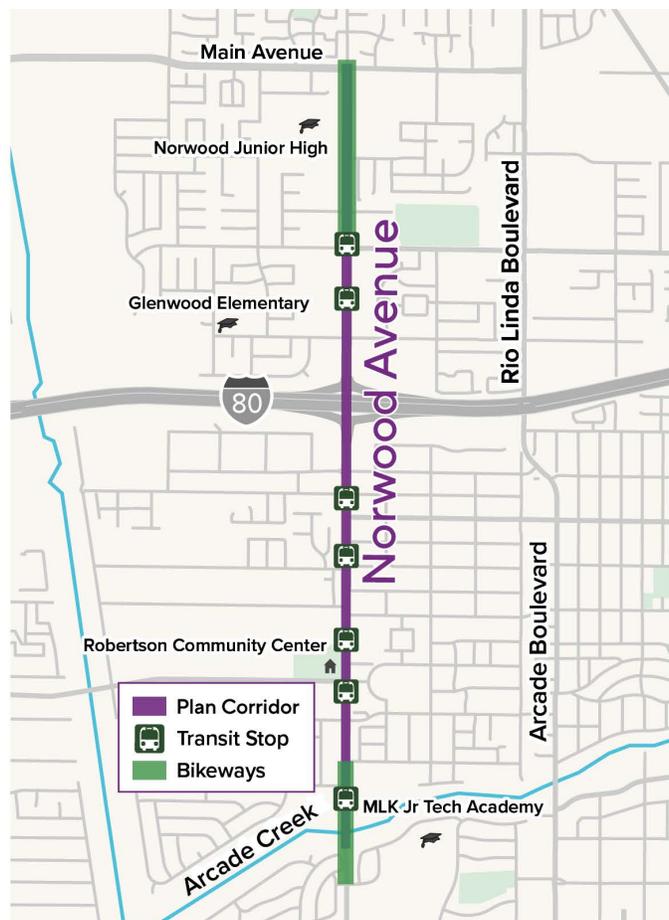
Registration is required to attend

*Es necesario registrarse para asistir*

For more information, visit our website at:

*Para más información visite nuestro sitio web en:*

[www.NorwoodMobility.org](http://www.NorwoodMobility.org)



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City of  
SACRAMENTO



The Norwood

Mobility Project

City of SACRAMENTO

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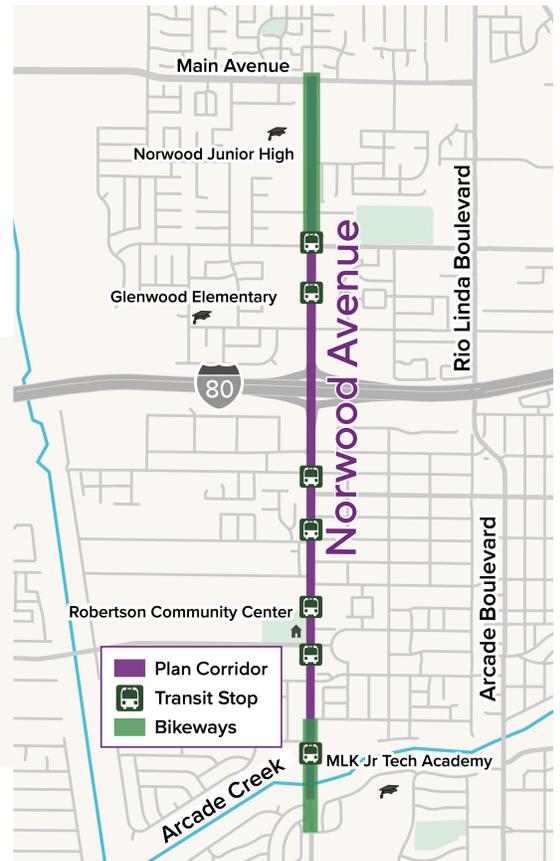
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The Norwood

Mobility Project

City of  
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**¡Ayúdenos a desarrollar un plan para mejorar la seguridad y el acceso en Norwood Avenue ya sea que esté caminando, en bicicleta, conduciendo o tomando el autobús!**

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**Vía reunión de Zoom**

Regístrese en: [bit.ly/norwood-register](https://bit.ly/norwood-register)

ID de reunión: 899 0189 8092

Código de acceso: Norwood

*Es necesario registrarse para asistir*

Para más información visite nuestro sitio web en:

**[www.NorwoodMobility.org](http://www.NorwoodMobility.org)**



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## The Norwood Mobility Project

The City of Sacramento is developing a vision for the Norwood Avenue corridor that provides a safer & more multimodal-friendly roadway for the community.

Open

Embed

### Community Survey

Please take the following brief survey. Your input is extremely valuable, and it will help the project team select the preferred future options and potential physical changes to Norwood Avenue.

What is your zip code?

How often do you typically travel on Norwood Avenue?

Daily

- Some Days (e.g., work commute, shopping, and errands)
- Weekly
- Every Couple of Weeks
- Monthly
- Rarely

**How do you typically travel on Norwood Avenue? Select all that apply.**

- Driving in a Personal Vehicle
- Riding in a Personal Vehicle
- Public Transit
- Paratransit
- Walking/Rolling
- Bicycling (including using e-bikes)
- Scooting
- Ride-Sharing (Uber, Lyft), Taxi
- Other (please specify)

For the next questions, please rate your interest in each potential change to Norwood Avenue on a scale from 1 (least interested) to 5 (most interested).

**Improved public transit stop conditions and access.**

1 = least interested, 5 = most interested.

- 1
- 2
- 3
- 4
- 5



**Improved walking conditions such as wider sidewalks and street trees.**

1 = least interested, 5 = most interested.

- 1
- 2
- 3
- 4
- 5

**Improved walking and bicycling crossing of Norwood Ave.**

1 = least interested, 5 = most interested.

- 1
- 2
- 3
- 4
- 5

**Improved bikeways on Norwood (buffer bike lanes or separated bikeways with a post or curb).**

1 = least interested, 5 = most interested.

- 1
- 2
- 3
- 4
- 5

**Reduced driver speed.**

1 = least interested, 5 = most interested.

- 1

---

**Improved driving safety.**

1 = least interested, 5 = most interested.

- 1
- 2
- 3
- 4
- 5

**Other transportation safety-related improvements (please specify and rate your interest in the change from 1 to 5).**

The following optional three demographic questions help us know if we are getting a broad and representative range of community perspectives. Please still submit this survey even if you decide to not answer these three optional questions.

**What best describes your race or ethnicity? Select all that apply.**

(Optional).

- Asian
- Black or African American
- Hispanic or Latino/a/e
- Middle Eastern or North African
- Native American or Alaska Native
- Native Hawaiian or other Pacific Islander

- White
- Prefer not to say
- Other (please specify)

**What is your age?**

(Optional).

- Under 18
- 18 to 24 years
- 25 to 34 years
- 35 to 44 years
- 45 to 64 years
- 65 to 84 years
- 85 to 99 years
- 100 years and older

**Do you identify as someone with a mobility or related disability that impacts how you travel?**

(Optional).

- Yes
- No
- Prefer not to say

**Do you have any other comments related to accessibility and safety on Norwood Ave?**



The Norwood  
**Mobility Project**

# Phase 1 Engagement Summary

## Phase 1 Public Engagement Summary

The following section summarizes engagement methods and feedback received during the first round of public engagement.

### Public Engagement Events

#### In-Person Events

The project team attended the Harvest Festival on Saturday, October 26, 2024. The Harvest Festival is a family friendly event that is highly attended and includes vendors, local organizations, and public agencies to promote their services and goods while providing a space for families to “trick or treat”. This event was attended by the City to promote awareness of the Norwood Mobility Project, gather public input about current issues along the corridor, and encourage community members to complete a project survey. The project team interacted with over 50 people at the Harvest Festival.



A public workshop was held on Monday, November 18, 2024, from 6:30 to 8:00 pm. The workshop provided residents, employees, business owners, school district officials, parents, and other interested parties an opportunity to learn about the study and the City’s efforts to improve corridor conditions. Attendees were introduced to the project’s purpose, need, and goals, provided an opportunity to complete a community survey, and/or leave



comments on the social pinpoint interactive map. Four comment boards were also provided to gather public input with each board denoting a transportation mode (i.e., walking, biking, driving, or transit). Approximately 10 people from the public attended the workshop. Attendees were engaged and receptive to the project and provided feedback regarding areas of concern on Norwood Avenue and potential improvements they would support.

On December 19, 2024, City staff attended a public workshop hosted by the Neighborhood Development Action Team (NDAT). The NDAT workshop was held at Bella’s Boba, east of Norwood Avenue on Eleanor Avenue. This event was attended by approximately 20

members of the community and provided attendees with project information and the opportunity to complete a community survey, provide input on a map board, or discuss corridor issues with project staff.

### **Virtual Meeting**

On Monday, December 9, 2024, a virtual community meeting was held. This virtual meeting served the same purpose as the in-person workshop to raise project awareness, gather public comment, and concerns. The event was held via Zoom from 6:30pm to 7:30pm in an effort to ensure community members could participate in project discussion and provide input. The virtual workshop consisted of a brief presentation to introduce the project purpose, need, and overall goals. During the virtual meeting, attendees were given the opportunity to provide comments, questions, or raise concerns to project staff. Participants were also given the project website information to complete the survey and/or interactive map on their own time.

## **Engagement Media Methods**

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### **Project Website**

Integrated into the City of Sacramento website, a project specific webpage was created for the Norwood Mobility Project<sup>17</sup>. As shown in **Figure 27**, information such as project background, corridor extents, project schedule, and input methods are provided. The project webpage offers two forms of public input such as a community survey and interactive Social Pinpoint map (**Figure 28**). The community survey was provided at the in-person workshop in English and Spanish, the online version allows for translation (**Figure 29**).

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<sup>17</sup> [Norwood Mobility Project](#)

# The Norwood Mobility Project

## Project overview

Norwood Avenue between Main Avenue and Arcade Creek is a critical corridor serving local neighborhoods, as well as students and businesses. However, it is part of the City’s High Injury Network, corridors with a high number of transportation related severe injuries and fatalities, and identified as a high priority project in the City’s Transportation Priorities Plan.

The City was awarded a competitive planning grant to review data and work with the community to develop a plan to address safety and mobility on the corridor.

The goal of the plan is to identify a data driven, community supported vision for a future Norwood Avenue, inclusive of all users and reflective of the needs of the community it serves, eliminating barriers to jobs, housing, and services.

Having a Council adopted plan ensures the City is eligible for competitive grant funding for any next phases such as Preliminary Engineering Design, Environmental Clearance, Final Design and Construction.



## Project schedule

- Fall 2024:** Existing conditions analysis
- Fall-Winter 2024/2025:** Community engagement phase 1, including in-person and virtual workshops and pop-ins
- Fall 2024 – Spring 2025:** Alternatives analysis
- Winter 2025:** Community engagement phase 2, including community survey, virtual open house and focus groups
- Spring -Fall 2025:** Draft plan development and community engagement
- Winter 2025:** Final Plan



The Norwood Mobility Project Schedule

## Share your input

Explore [The Norwood Mobility Project interactive map](#) where you can share your comments.

There will be a variety of opportunities for you to get involved and provide your input, including community pop-ins where we will meet with the community where they are, as well as in-person and virtual workshops.

### In-Person Workshop

Monday, November 18, 2024 (completed!)

### Virtual Workshop

Monday, December 9, 2024

6:30-7:30pm

[Registration link](#)

\*Registration required

You can review our [Norwood Mobility Project Phase 1 presentation here](#).



Figure 27. Norwood Mobility Project Web Page

# We need your input!

Use the interactive map to provide comments about locations in the study area.

Follow these instructions to use the map:

- To add a comment > Select the 'Add Marker' button in the lower right corner of the map and click the specific location where you want to leave your comment. Fill out the details of the input form as required and select the 'Submit' button.



- To view the map legend and/or turn map layer on/off > Select the icon in the upper left corner of the map that looks like a stack of papers. The display box will show the maps layers. Click next to the circle to the right of each layer label to toggle that layer on/off.



- To select an a different base map > Select the icon in the upper left corner of the map that looks like an unfolded map. The display box will show several base map options to choose from.



- To view additional map instructions > Select the question mark icon just above the map in the upper left corner. The display box will include more instruction information.

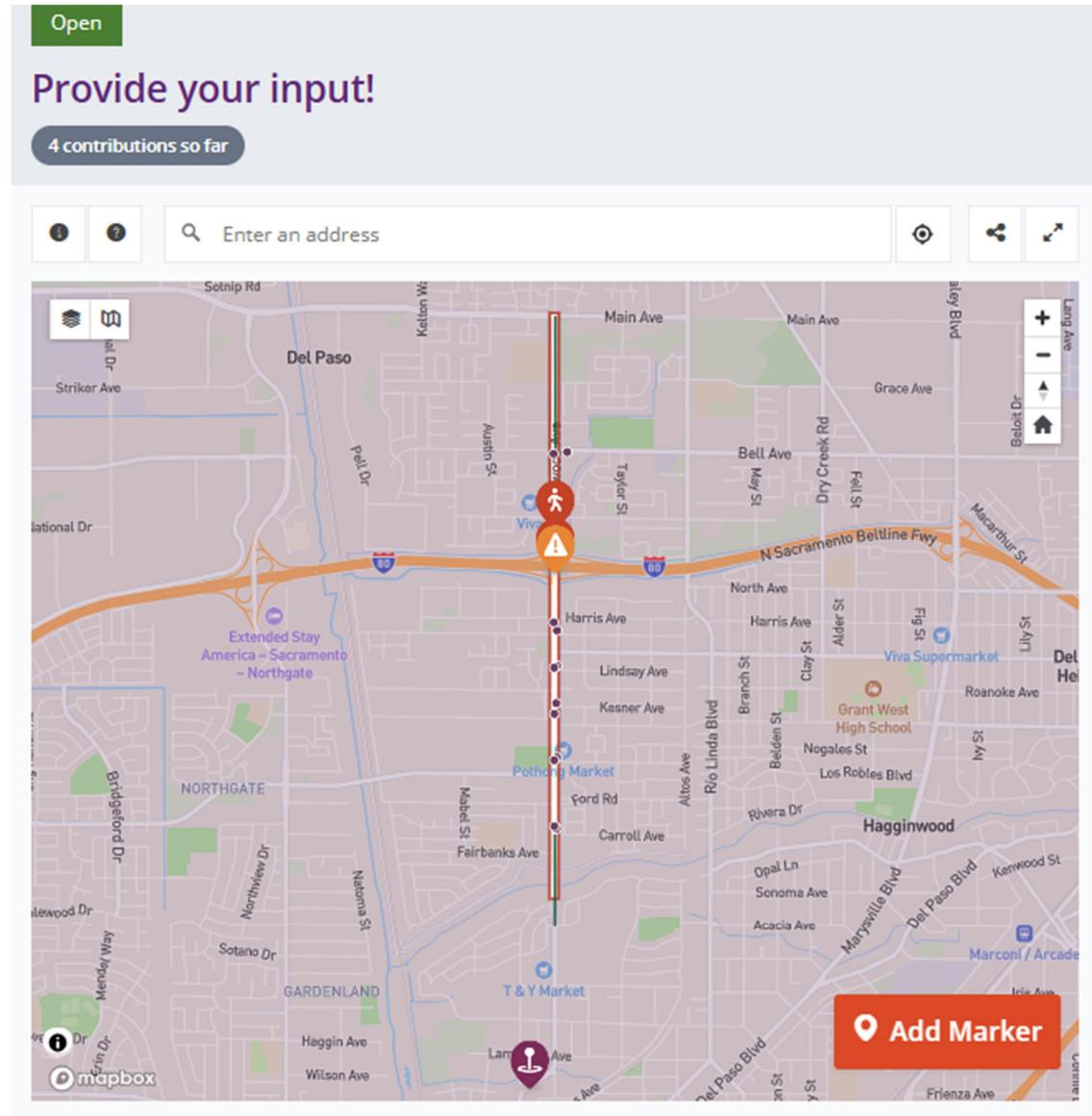


Figure 28. Norwood Avenue Interactive Comment Map

## Community Survey

Please take the following brief survey. Your input is extremely valuable, and it will help the project team select the preferred future options and potential physical changes to Norwood Avenue.

What is your zip code?

How often do you typically travel on Norwood Avenue?

- Daily
- Some Days (e.g., work commute, shopping, and errands)
- Weekly
- Every Couple of Weeks
- Monthly
- Rarely

How do you typically travel on Norwood Avenue? Select all that apply.

- Driving in a Personal Vehicle
- Riding in a Personal Vehicle
- Public Transit
- Paratransit
- Walking/Rolling
- Bicycling (including using e-bikes)
- Scooting
- Ride-Sharing (Uber, Lyft), Taxi
- Other (please specify)

For the next questions, please rate your interest in each potential change to Norwood Avenue on a scale from 1 (least interested) to 5 (most interested).

Improved public transit stop conditions and access

1 = least interested, 5 = most interested

- 1
- 2
- 3
- 4
- 5

### Figure 29. Norwood Avenue Community Survey

## Event Flyers

To promote awareness of the public workshop and virtual meeting, a flyer was circulated on the City of Sacramento website, pop-up events, and social media outlets to promote the upcoming events. As shown in **Figure 30**, the event flyer consisted of meeting information, project background, links, and a QR code to route views to the project website, survey, and comment map.



## Help us develop a plan to improve safety and access on Norwood Avenue whether you are walking, biking, driving, or taking the bus!

*¡Ayúdenos a desarrollar un plan para mejorar la seguridad y el acceso en Norwood Avenue ya sea que esté caminando, en bicicleta, conduciendo o tomando el autobús!*

### Join us for a workshop to share your ideas!

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Via Zoom Meeting | *Vía reunión de Zoom*

Register at | *Regístrate en:* [bit.ly/norwood-register](https://bit.ly/norwood-register)

Meeting ID | *ID de reunión:* 899 0189 8092

Passcode | *Código de acceso:* Norwood

Registration is required to attend

*Es necesario registrarse para asistir*

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Figure 30. Norwood Avenue Event Flyer

## Public Engagement Results

Since the project webpage launch in September up to December 2024, the Norwood Mobility Project received several comments through various outlets such as the interactive map, public survey, and engagement events.

The community survey results are based on 75 respondents, 49 of the survey responses are from in-person events. Survey results indicated that around 76% of survey respondents travel on Norwood Avenue daily; about 75% typically drive in their personal vehicle, approximately 29% walk/roll, and about 16% take public transit on Norwood Avenue.

Survey respondents were mostly interested in improving crossing opportunities for those walking and bicycling on Norwood Avenue, reduced driver speed, improved driver safety, and improved walking conditions such as wider sidewalks and street trees.

Based on 54 comments received via the online interactive map and in-person events, 26 comments were specific to Bell Avenue, Jessie Avenue, and I-80 eastbound and westbound on/off ramps and generated the most concern from those who provided input (**Figure 31**). Walking access, driving operations, and safety were the most prominent concerns for respondents at Bell Avenue, Jessie Avenue and I-80 ramps. Jessie Avenue is one of the primary community focal points along with the Robertson Community Center and Pothong Market. The Jessie Avenue intersection provides key access to the Viva Supermarket, Rite Aid, Arco, and fast-food restaurants. Additionally, I-80 westbound on-off ramps are directly accessed by Jessie Avenue. Bell Avenue is a key intersection for people living in adjacent multi-family housing to access Norwood Avenue.

**Figure 32** illustrates the comments stratified by transportation mode on Norwood Avenue. Approximately 43% revolve around walking concerns, such as areas where people walking feel unsafe. As noted, community members would support improved safety for people walking, including high-visibility crosswalks and lighting. The complete list of survey results and comments received are included in *Appendix E*.

Norwood Mobility Project Engagement Comment Cartogram

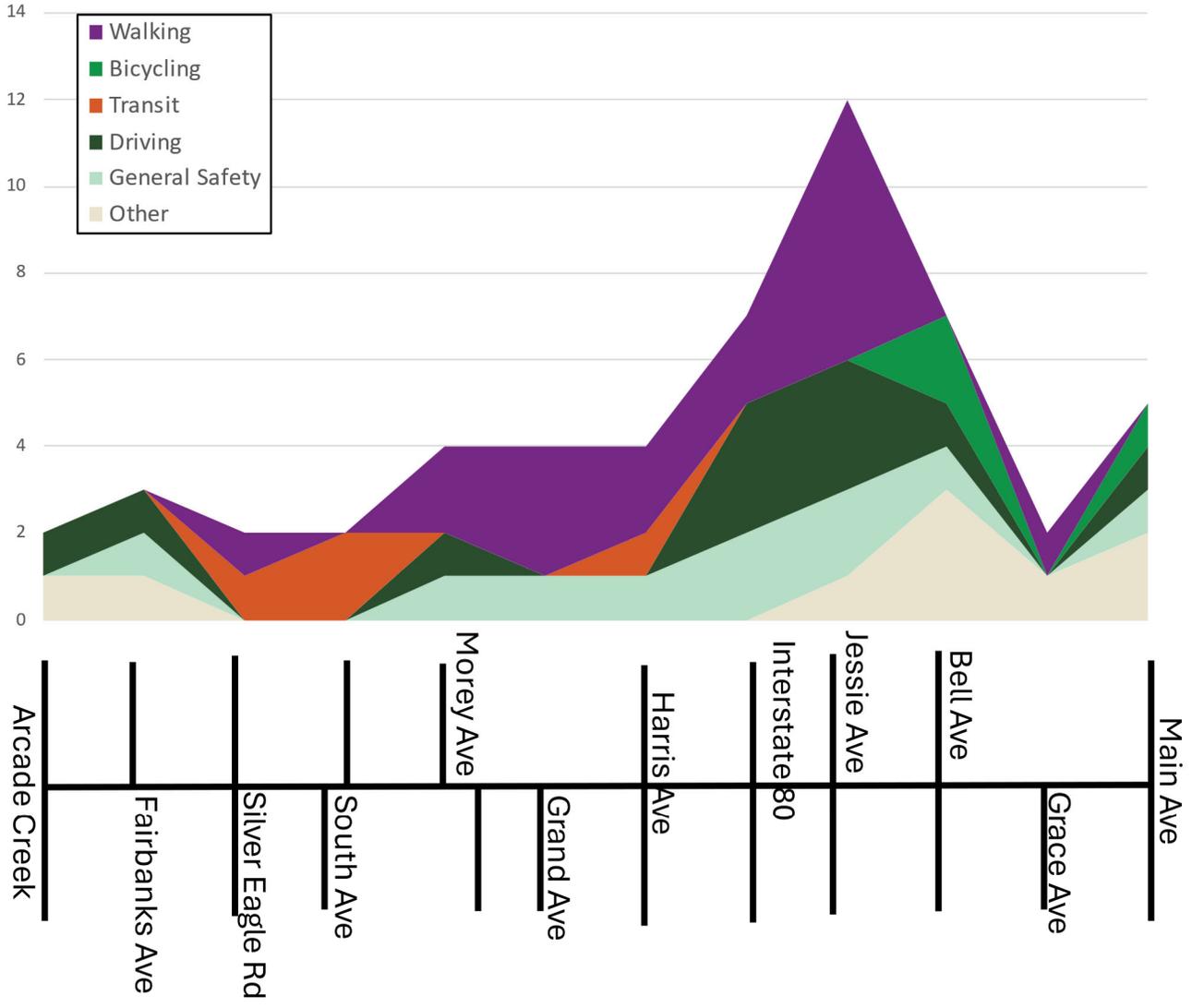
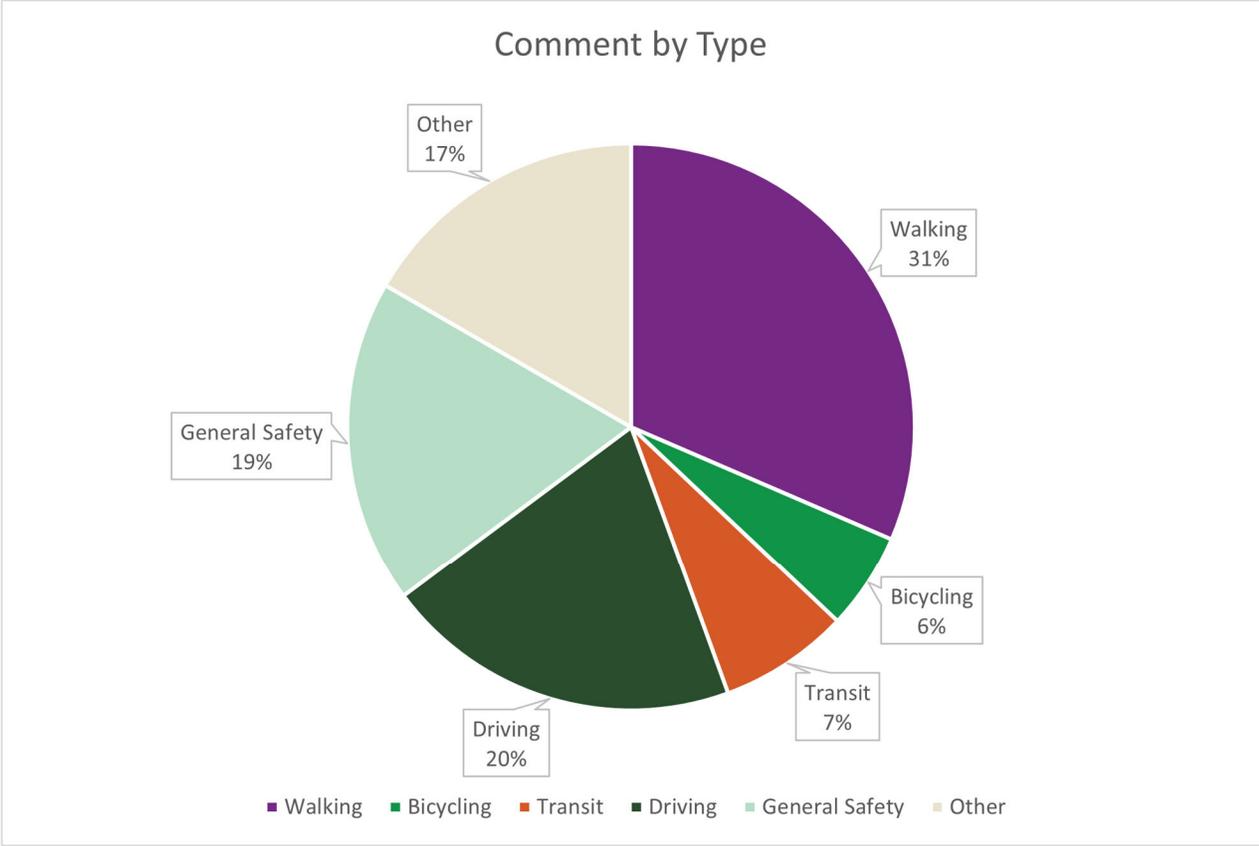


Figure 31. Engagement comments by Major Intersection



**Figure 32. Comments by Type**

## Existing Transportation Challenges and Constraints

To gain a greater understanding of the challenges presented by this corridor, the primary concerns are outlined below. **Figure 33** illustrates the existing infrastructure along Norwood Avenue and identifies bicycle lanes and sidewalk gaps.



**Figure 33. Infrastructure Gaps and Constraints**

## Walking Infrastructure

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Sidewalks exist throughout the study corridor except along the northbound travel lanes from Grace Avenue to Main Avenue and along the southbound travel lanes from Grace Avenue to Berthoud Street. The existing sidewalks along Norwood Avenue do not show significant deterioration but contain some cracks and chipped concrete. In addition to sidewalk conditions, throughout the corridor the sidewalk width is five feet but are obstructed by utility poles placed within the sidewalk, reducing the available sidewalk width.

The sidewalk along the northbound lanes from Grace Avenue to Berthoud Street do not contain significant shade for people walking. Increased shade cover from street trees is prevalent from Berthoud Street to Jessie Avenue, the remainder of the corridor from Jessie Avenue to Arcade Creek consists of substantial tree cover to protect people walking from extreme temperatures.

There are 11 intersections that have controlled marked crosswalks, five are north of I-80 and six are south of I-80. The distance between marked controlled crosswalks can vary between 650 to over 1,500 feet. South of I-80, Morey Avenue is an offset controlled intersection with three marked crosswalks. At uncontrolled intersections south of I-80, there are no Norwood Avenue crossing opportunities which can present non-intuitive crossing needs for people walking, promoting crossing activity at uncontrolled locations.

Additionally, the I-80 freeway ramps can create another barrier to people walking. The lack of control and visibility enhancements at the freeway ramps create a high-stress environment for people walking as vehicles increase speeds to enter the freeway and there is no traffic control for vehicles exiting the freeway and merging onto Norwood Avenue.

Future potential design alternatives will seek to address increasing visibility and improving walking comfortability.

## Bicycling Infrastructure

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Bicycling infrastructure along Norwood Avenue is inconsistent and disconnected throughout the study corridor. Bike lane widths at the following locations are five feet and do not provide green paint to highlight conflict areas between modes or physical barriers to separate people biking from vehicle traffic. Bike lanes are present at the following locations:

- Northbound and southbound from Arcade Creek to Carroll Avenue
- Northbound Bell Avenue 200 feet south of the intersection approach
- Northbound from Bell Avenue to Grace Avenue.
- Southbound from Main Avenue to Grace Avenue

Having bike parking at locations could increase interest in biking as a form of transportation, allowing people biking to park their bike at commercial and recreational centers. Within the study corridor, there are five locations with bike parking ranging between three to seven spaces listed below:

- Robertson Community Center
- Nuevo Park
- Dollar General
- Department of Human Assistance
- Norwood Center

Future potential design alternatives will seek to address bicycle lane gaps, provide connection to the adjacent Sacramento Northern Bike Trail and Walter S. Ueda Bikeway, and improve access and comfortability for all ages and abilities of people biking.

## **Transit Infrastructure**

---

Norwood Avenue is served by SacRT Route 19 and Route 86. Route 19 has 60-minute all day headways on weekdays and weekends. Route 86 has 30-minute weekday headways and between 45 and 60-minute headways on weekends.

Norwood Avenue has 14 bus stops with only one providing a bus shelter. The existing shelter is at the Norwood Avenue and Bell Avenue southbound bus stop and includes a bench for seating but does not have a trash bin. Bus stop locations vary along the corridor as being nearside or far-side of signalized intersections. All of the bus stops are located in-lane and, though the lanes are wider than City standards, a bus loading passengers would still block traffic.

Bus stops are heavily concentrated from Silver Eagle Road to Arcade Creek and there are no bus stops north of Bell Avenue. All bus stops along the corridor are identified by a transit sign. None of the bus stops are accessible via a low-stress walking or biking network.

## **Crashes**

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The study corridor experienced 137 injury crashes from 2018 to 2022. Of the 137 crashes, 21% were bicycle and pedestrian crashes (29 crashes). Fatal and severe injury crashes accounted for 34% of the 29 bicycle and pedestrian crashes. The highest density of crashes for all modes from 2018 to 2022 occurred between Bell Avenue and I-80, with 43% of all crashes occurring in Segment 2 of the corridor, making it a priority location for safety improvements.

This segment includes a mix of residential and commercial land use, on-street parking, and a high density of driveways. Of the 29 crashes involving people walking and biking, 16 occurred on this same segment between Bell Avenue and I-80.

The issues the design alternatives will seek to address are reducing uncontrolled conflicts between different modes of travel along the corridor, improving visibility and awareness of

potential conflict zones, reducing speeds along the corridor, and creating additional controlled crossing opportunities at high demand locations along the corridor.

## OPERATIONS

---

Much of the corridor experiences unreliable travel times and congestion. Although corridor intersections operate acceptably, many of them experience weekday AM/PM peak hour queue conditions that exceed available storage. The corridor design alternatives will seek to address consistent cross-sections throughout the corridor, efficient signal timing for all users of the corridor including buses, providing sufficient storage for queuing, and operational modifications that improve safety for all roadway users.

## Right of Way

---

Right of way (ROW) along the corridor varies throughout Norwood Avenue. From curb to curb, the ROW varies from 48 to 70 feet wide involving the following components:

- Inside travel lanes are 11 feet.
- Outside travel lane widths vary from 12 to 14 feet.
- Two-way center left turn lane is 10 feet.
- Sidewalks along the study corridor are 5 feet but are the responsibility of the fronting property owner<sup>18</sup>. Utility poles are located within the sidewalk width.
- Along the few segments where on-street parking is allowed, the parking lane is 8 feet.

Additional consideration for ROW will need to be given to the I-80 overpass and Arcade Creek bridge due to reduced roadway width and the structure providing a constrained roadway width. Where the corridor is two lanes per direction with a two-way center left turn lane, design alternatives will seek to use existing roadway space to improve infrastructure for people walking or biking such as widening sidewalks or implementing marked bike lanes or buffered bike lanes.

---

<sup>18</sup> [Sacramento City Code, Section 12.32.020](#)

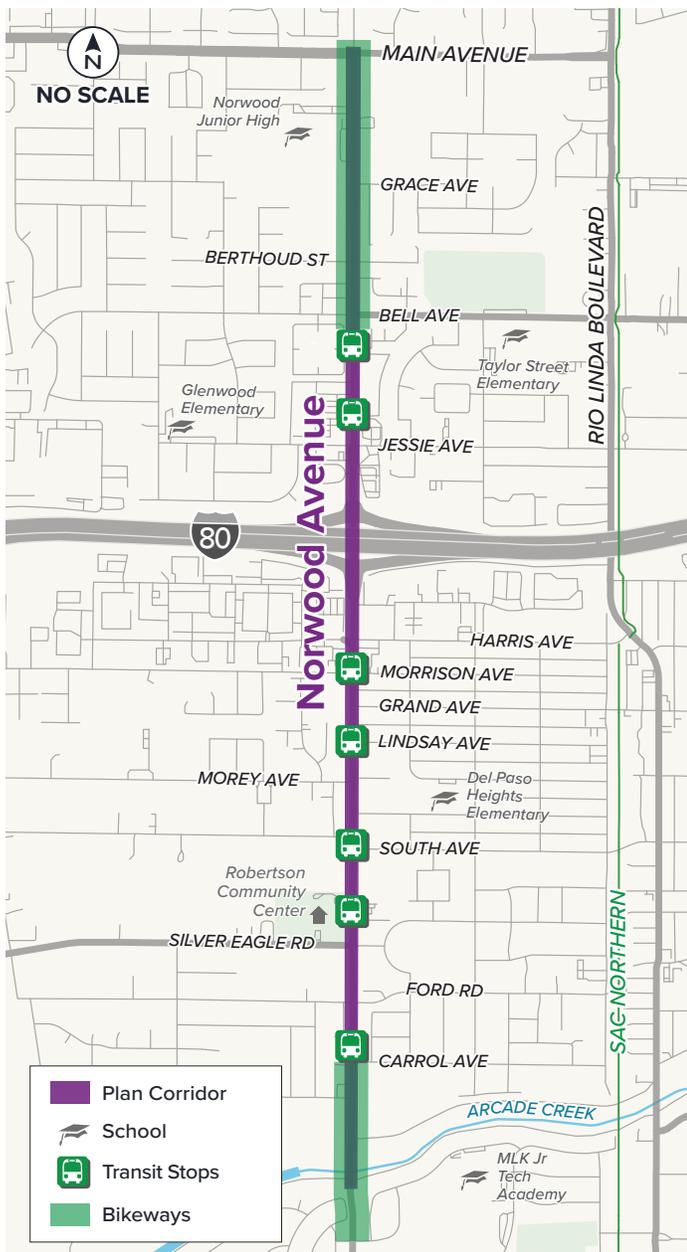


The Norwood  
**Mobility Project**

# Phase 2 Engagement Materials

**You shared ideas for changes to Norwood Avenue and we heard you. We developed concepts based on your input and we want your feedback!**

*Ustedes compartieron ideas para cambios en Norwood Avenue, y los escuchamos. Desarrollamos conceptos basados en sus aportes, ¡y ahora queremos saber qué opinan!*



**Share your input** on proposed solutions at the next **community workshop!**

*¡Comparta su opinión sobre las soluciones propuestas en el próximo taller comunitario!*

**IN-PERSON**  
*EN PERSONA*

**June 7, 2025 | 7 de junio de 2025**

**10:00 AM - 11:30 AM**

**Robertson Community Center**  
3525 Norwood Ave, Sacramento

**VIRTUAL**  
*VIRTUAL*

**June 9, 2025 | 9 de junio de 2025**

**6:30 PM - 7:30 PM**

**Via Zoom Meeting | Vía reunión de Zoom**

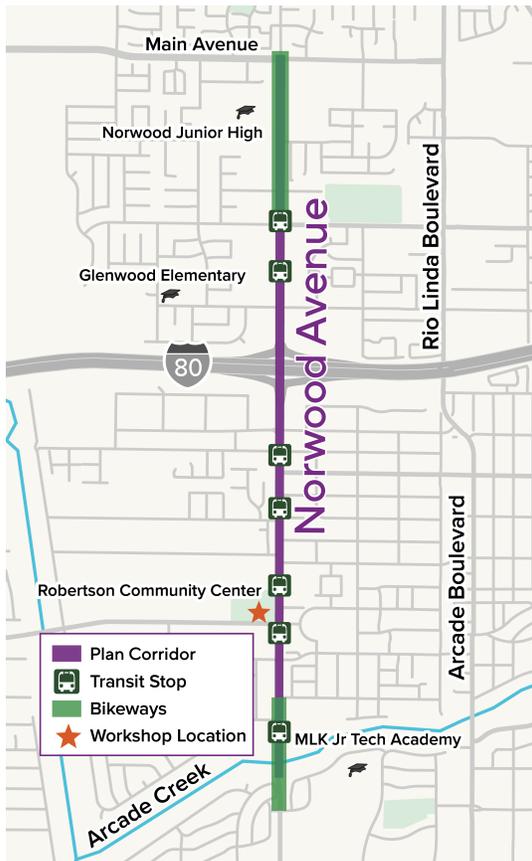
Register on project website:  
*Regístrese en el sitio web del proyecto:*  
[www.NorwoodMobility.org](http://www.NorwoodMobility.org)

Meeting ID | *ID de reunión:*  
841 8286 4546

Registration is required to attend.  
*Es necesario registrarse para asistir.*

**SCAN HERE TO REGISTER:**  
*ESCANEE EL CÓDIGO PARA REGISTRARSE:*





**You shared ideas for changes to Norwood Avenue and we heard you. We developed concepts based on your input and we want your feedback!**

**Share your input** on proposed solutions at the next **community workshop!**

**IN-PERSON**

**June 7, 2025**

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**Robertson Community Center**

3525 Norwood Ave, Sacramento

**VIRTUAL**

**June 9, 2025**

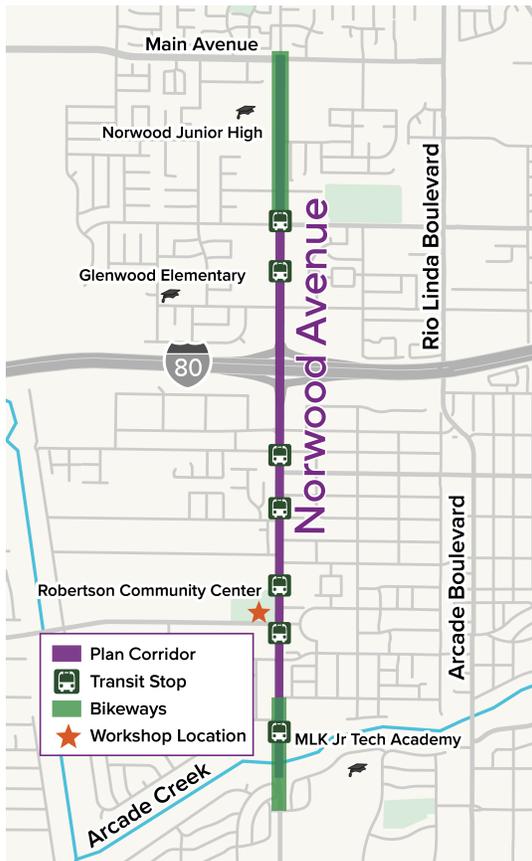
**6:30 PM - 7:30 PM**

**Via Zoom Meeting**

Register on the project website:  
[www.NorwoodMobility.org](http://www.NorwoodMobility.org)

Meeting ID: 841 8286 4546

*Registration is required to attend*



**Ustedes compartieron ideas para cambios en Norwood Avenue, y los escuchamos. Desarrollamos conceptos basados en sus aportes, ¡y ahora queremos saber qué opinan!**

**¡Comparte tus comentarios** sobre las soluciones propuestas en el próximo taller comunitario!

**EVENTO EN PERSONA**

**7 de junio de 2025**

**10:00 a. m. a 11:30 a. m.**

**Robertson Community Center**

3525 Norwood Ave, Sacramento

**EVENTO VIRTUAL**

**9 de junio de 2025**

**6:30 p. m. a 7:30 p. m.**

**A través de Zoom**

Regístrese en el sitio web del proyecto:

[www.NorwoodMobility.org](http://www.NorwoodMobility.org)

ID de reunión: 841 8286 4546

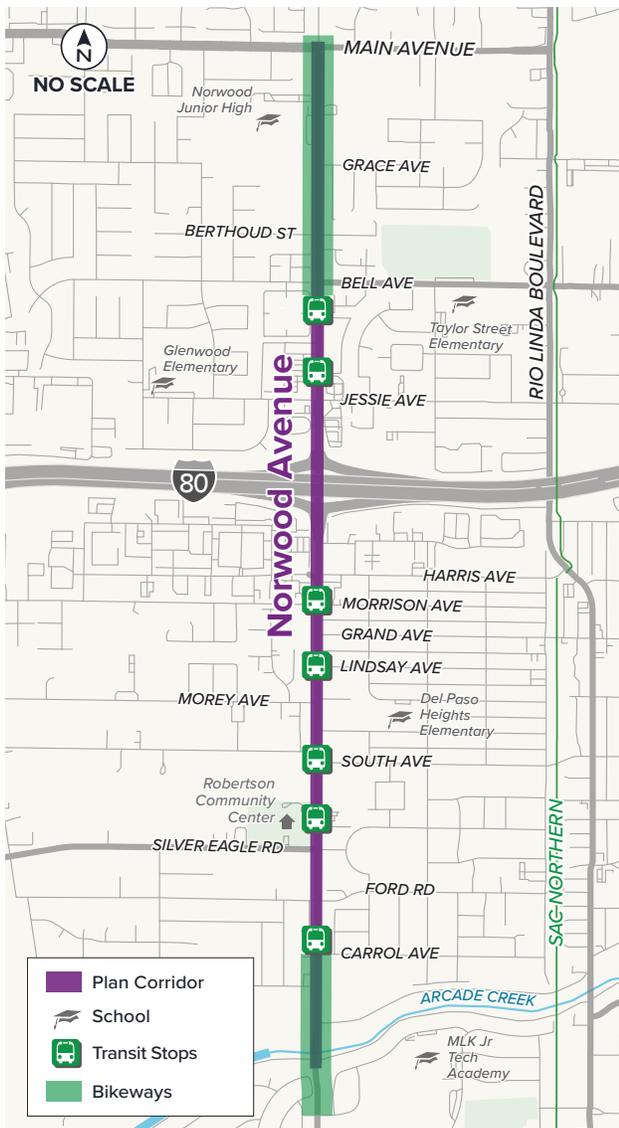
*Es necesario registrarse para asistir*



The Norwood  
Mobility Project

**You shared ideas for changes to Norwood Avenue and we heard you. We developed concepts based on your input and we want your feedback!**

*Ustedes compartieron ideas para cambios en Norwood Avenue, y los escuchamos. Desarrollamos conceptos basados en sus aportes, ¡y ahora queremos saber qué opinan!*



**Share your input on proposed solutions at the next community workshop!**

*¡Comparta su opinión sobre las soluciones propuestas en el próximo taller comunitario!*

**VIRTUAL  
VIRTUAL**

**June 17, 2025 | 17 de junio de 2025**

**NEW DATE!  
¡NUEVA FECHA!**

**6:30 PM - 7:30 PM**

**Via Zoom Meeting | Vía reunión de Zoom**

Register on project website:

*Regístrese en el sitio web del proyecto:*

[www.NorwoodMobility.org](http://www.NorwoodMobility.org)

Meeting ID | ID de reunión:

854 6961 1459

Registration is required to attend.

*Es necesario registrarse para asistir.*

**SCAN HERE TO REGISTER:**

*ESCANEE EL CÓDIGO PARA REGISTRARSE:*





The Norwood  
Mobility Project

City of  
SACRAMENTO

**You shared ideas for changes to Norwood Avenue and we heard you. We developed concepts based on your input and we want your feedback!**

**Share your input** on proposed solutions at the next **community workshop!**

**June 17, 2025**

**6:30 PM - 7:30 PM**

**Via Zoom Meeting**

Register on the project website: [www.NorwoodMobility.org](http://www.NorwoodMobility.org)

Meeting ID: 854 6961 1459

**Registration is required to attend**



Español | 中文 | Tagalog | Tiếng Việt | Hmoob | Русский



**Ustedes compartieron ideas para cambios en Norwood Avenue, y los escuchamos. Desarrollamos conceptos basados en sus aportes, ¡y ahora queremos saber qué opinan!**

**¡Comparte tus comentarios** sobre las soluciones propuestas en el próximo taller comunitario!

**17 de junio de 2025**

**6:30 p.m. a 7:30 p.m.**

**A través de Zoom**

Regístrese en el sitio web del proyecto: [www.NorwoodMobility.org](http://www.NorwoodMobility.org)

ID de reunión: 854 6961 1459

*Es necesario registrarse para asistir*

**311** Español | 中文 | Tagalog | Tiếng Việt | Hmoob | Русский

# Please provide your feedback on Alternative 1!

The Norwood Mobility Project / Alternative 1

## Alternative 1

- Add sidewalks north of Berthoud St
- Add signalized crosswalks at high demand locations and at I-80 ramp crossings
- Lower speed limits
- Add additional transit shelters and benches
- Remove on-street parking south of Bell Ave
- Widen sidewalks on the west side



**Community Input:**

"Sidewalks are too narrow,"  
"Increase lighting,"  
"More TREES!"  
"Ramp lanes narrow and only one lane in each direction,"  
"Bikeway on entire corridor,"  
"Use roundabouts."

"Needs bicycle lane and sidewalk,"  
"Improved child safety to/from around schools,"  
"Use protected bike/pedestrian paths,"  
"Need more safety/more and wider sidewalks/more trees."

**Benefits:**

- Wider sidewalks for people walking
- Additional marked and controlled crossings provide increased safety

**Challenges:**

- No bikeways
- No traffic calming infrastructure
- No new lighting
- No available space for trees

**Cost:** \$

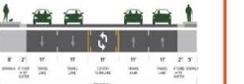


NORWOOD AVENUE ROADWAY CONFIGURATION

**BEFORE:**



**AFTER:**



IMPROVEMENT STRATEGY

**SIGNALIZED CROSSING**



[Click here to view the image above larger.](#)

Open

Embed

## Alternative 1 Survey

After reviewing the proposed alternative (above), please provide your feedback below.

### How well does Alternative 1 meet community priorities?

Improve corridor safety, particularly between Jessie Avenue and Bell Avenue and between Silver Eagle Road and Harris Avenue.

- Meets expectations
- Somewhat meets expectations
- Neutral
- Somewhat does not meet expectations
- Does not meet expectations

Improve walking infrastructure, including the addition of signal-protected crossing opportunities where feasible.

- Meets expectations
- Somewhat meets expectations
- Neutral
- Somewhat does not meet expectations
- Does not meet expectations

Create low-stress facilities that improve safety and comfort for people walking, rolling, and bicycling to reach transit.

- Meets expectations
- Somewhat meets expectations
- Neutral
- Somewhat does not meet expectations
- Does not meet expectations

Create low-stress facilities that improve safety and comfort for people biking.

- Meets expectations
- Somewhat meets expectations
- Neutral
- Somewhat does not meet expectations
- Does not meet expectations

Please provide any additional feedback on this alternative.

Submit

[Project Home](#) [Alternative 1](#) [Alternative 2](#) [Alternative 3](#) [Overall Feedback](#)

# Alternative 2

The Norwood Mobility Project / Alternative 2

## Alternative 2

**Benefits:**

- Provides a dedicated and separated space for people biking
- Provides additional buffer between people walking and people driving
- Roundabouts slow traffic and reduce the severity of crashes if they happen
- Landscape buffer and lighting provide separation from traffic and improved comfort

**Challenges:**

- The existing traffic volumes and overpass width don't provide room to expand the bicycle lanes over the freeway
- Utility relocation would need to be coordinated with SMUD

- Add sidewalks north of Berthoud St
- Add signalized crosswalks at high demand locations and at I-50 ramp crossings
- Lower speed limits
- Add additional transit shelters and benches
- Remove on-street parking south of Bell Ave
- Remove a travel lane in each direction
- Add a separated bikeway in each direction
- Add a landscaping buffer and lighting
- Add roundabouts for traffic calming

**Community Input**

"Sidewalks are too narrow."

"Increase lighting."

"More TREES!"

"Keep lanes narrow and only one lane in each direction."

"Bikeway on entire corridor."

"Use roundabouts."

"Needs bicycle lane and sidewalk."

"Improved child safety to/from around schools."

"Use protected bike/pedestrian paths."

"Need more safety/more and wider sidewalks/more trees."

**NORWOOD AVENUE ROADWAY CONFIGURATION**

**BEFORE:**

**AFTER:**

**SAMPLE INTERSECTION: NORWOOD & MOREY**

**BEFORE:**

**AFTER:**

**Cost:** \$ \$

[Click here to view the image above larger.](#)

Open

Embed

## Alternative 2 Survey

After reviewing the proposed alternative (above), please provide your feedback below.

### How well does Alternative 2 meet community priorities?

**Improve corridor safety, particularly between Jessie Avenue and Bell Avenue and between Silver Eagle Road and Harris Avenue.**

- Meets expectations
- Somewhat meets expectations
- Neutral
- Somewhat does not meet expectations
- Does not meet expectations

**Improve walking infrastructure, including the addition of signal-protected crossing opportunities where feasible.**

- Meets expectations
- Somewhat meets expectations
- Neutral
- Somewhat does not meet expectations
- Does not meet expectations

**Create low-stress facilities that improve safety and comfort for people walking, rolling, and bicycling to reach transit.**

- Meets expectations
- Somewhat meets expectations
- Neutral
- Somewhat does not meet expectations
- Does not meet expectations

**Create low-stress facilities that improve safety and comfort for people biking.**

- Meets expectations
- Somewhat meets expectations
- Neutral
- Somewhat does not meet expectations
- Does not meet expectations

Please provide any additional feedback on this alternative.

Submit

# Alternative 3

The Norwood Mobility Project / Alternative 3

## Alternative 3

- Add sidewalks north of Berthoud St
- Add signalized crosswalks at high demand locations and at I-80 ramp crossings
- Lower speed limits
- Add additional transit shelters and benches
- Remove on-street parking south of Bell Ave
- Remove a travel lane in each direction
- Add a shared use path on the west side of Norwood Ave
- Add a landscaping buffer and lighting
- Add roundabouts for traffic calming



**Community Input:**

"Sidewalks are too narrow."  
"Increase lighting."  
"More TREES!"  
"Keep lanes narrow and only one lane in each direction."  
"Bikeway on entire corridor."  
"Use roundabouts."

"Needs bicycle lane and sidewalks."  
"Improved child safety to/from schools."  
"Use protected bike/pedestrian paths."  
"Need more safety/more and wider sidewalks/more trees."

**Benefits:**

- Roundabouts slow traffic and reduce the severity of crashes if they happen
- Provides a dedicated space for people bicycling
- Landscaping buffer and lighting provide separation from traffic and improved comfort

**Challenges:**

- Right of way acquisition will be needed
- Utility relocation would need to be coordinated with SMUD
- The cantilevered bike path over the freeway would require coordination with Caltrans

**Cost:** \$ \$ \$



NORWOOD AVENUE ROADWAY CONFIGURATION

**BEFORE:**



**AFTER:**



IMPROVEMENT STRATEGY

LANDSCAPE BUFFER & LIGHTING



CANTILEVERED SHARED USE PATH



[Click here to view the image above larger.](#)

Open

Embed

## Alternative 3 Survey

After reviewing the proposed alternative (above), please provide your feedback below.

### How well does Alternative 3 meet community priorities?

**Improve corridor safety, particularly between Jessie Avenue and Bell Avenue and between Silver Eagle Road and Harris Avenue.**

- Meets expectations
- Somewhat meets expectations
- Neutral
- Somewhat does not meet expectations
- Does not meet expectations

**Improve walking infrastructure, including the addition of signal-protected crossing opportunities where feasible.**

- Meets expectations
- Somewhat meets expectations
- Neutral
- Somewhat does not meet expectations
- Does not meet expectations

**Create low-stress facilities that improve safety and comfort for people walking, rolling, and bicycling to reach transit.**

- Meets expectations
- Somewhat meets expectations
- Neutral
- Somewhat does not meet expectations
- Does not meet expectations

**Create low-stress facilities that improve safety and comfort for people biking.**

- Meets expectations
- Somewhat meets expectations
- Neutral
- Somewhat does not meet expectations
- Does not meet expectations

Please provide any additional feedback on this alternative.

Submit

[Project Home](#)
[Alternative 1](#)
[Alternative 2](#)
[Alternative 3](#)
[Overall Feedback](#)

# Provide your overall feedback!

The Norwood Mobility Project / Overall Feedback

## Alternative Components

Please review the elements in each alternative and then complete the survey to the right.

|                                 |   | Alt 1 | Alt 2a | Alt 2b | Alt 2c | Alt 3 |
|---------------------------------|---|-------|--------|--------|--------|-------|
| Widen & Complete Sidewalks      |    | ✓     | ✓      | ✓      | ✓      | ✓     |
| New Signalized Crosswalks       |    | ✓     | ✓      | ✓      | ✓      | ✓     |
| Removal of On-Street Parking    |    | ✓     | ✓      | ✓      | ✓      | ✓     |
| Transit Shelters/Benches        |   | ✓     | ✓      | ✓      | ✓      | ✓     |
| Sidewalk Scale Lighting         |  |       | ✓      | ✓      | ✓      | ✓     |
| Removal of Vehicle Travel Lanes |  | ✓     | ✓      | ✓      | ✓      | ✓     |

Open </> Embed

### What is your preferred alternative?

Choose one: Required

- Alternative 1
- Alternative 2a
- Alternative 2b
- Alternative 2c
- Alternative 3

### Please provide your thoughts on the following:

Widening and completing sidewalks

Adding signalized crosswalks

Removing on-street parking south of Bell Street

Adding bus shelters and benches

Adding sidewalk-scale lighting

Removing a travel lane in each direction

Adding roundabouts

Adding a landscaping buffer

Adding a separated bikeway in each direction

Adding shade trees where space permits

Adding a shared use path on the west side with a cantilever structure across the freeway

Submit

|                                     |   |          |          |          |          |
|-------------------------------------|---|----------|----------|----------|----------|
| <p>Roundabouts</p>                  |     | <p>✓</p> | <p>✓</p> | <p>✓</p> | <p>✓</p> |
| <p>Additional Landscaping</p>       |    | <p>✓</p> | <p>✓</p> | <p>✓</p> | <p>✓</p> |
| <p>Separated Bikeway</p>            |    | <p>✓</p> | <p>✓</p> | <p>✓</p> |          |
| <p>Street Trees</p>                 |   |          | <p>✓</p> | <p>✓</p> | <p>✓</p> |
| <p>Shared Use Path</p>              |  |          |          | <p>✓</p> |          |
| <p>Shared Use Path over Freeway</p> |  |          |          | <p>✓</p> |          |



The Norwood  
**Mobility Project**

# Phase 2 Engagement Summary



## PHASE 2 OUTREACH SUMMARY

DATE: July 11, 2025

TO: Charisse Padilla | City of Sacramento

FROM: Elise Brockett | DKS Associates  
Alice Chen | DKS Associates  
Jim Damkowitz | DKS Associates

SUBJECT: Norwood Mobility Project Project #24795

---

### INTRODUCTION

This memo provides an overview of the feedback received during Phase 2 of public outreach for the Norwood Mobility Project in June/July 2025.

The City of Sacramento and DKS Associates planned and completed the following outreach activities during the engagement period from June 2 – July 6, 2025:

- In-Person Workshop – June 7 from 10 – 11:30 a.m. at the Robertson Community Center
- Virtual Workshop – June 17 from 6:30 – 7:30 p.m. via Zoom
- Robla Park Community Association (RPCA) Mini Workshop #1 – June 25 from 7 – 8:30 p.m.
- Robla Park Community Association (RPCA) Action Committee Mini Workshop #2 – July 2 from 6:30 – 8:00 p.m.

PDFs of each alternative were also available on the project website where community members could submit their comments and feedback in an online form during the engagement period.

### SUMMARY OF FEEDBACK

Overall themes from the feedback received both online and in person are presented first, followed by detailed feedback on each alternative, and then feedback on specific proposed elements from the online form.

### OVERALL THEMES

---

Based on the feedback received both online and in person, Alternatives 2 and 3 were generally favored among respondents as opposed to Alternative 1. Alternative 3 received the most praise

and positive feedback, specifically for its ability to address pedestrian and bicycle safety, provide additional lighting and landscaping, and slow traffic to increase safety, despite the higher cost. Alternative 2 included three variations to the roadway configuration with varying locations and widths for elements such as landscaping, walking and biking facilities, and lighting. Respondents liked Alternative 2c the most, citing the inclusion of both street lighting and landscaping as a benefit due to the increased separation of pedestrians and bicyclists from vehicles.

While some respondents appreciate that Alternative 1 provides wider sidewalks and more bike and pedestrian crossings, almost all agreed that this option wouldn't be worth the time and funding to make minor improvements to an area that is plagued by unsafe travel conditions.

A link to the online response form (hosted on the platform Social Pinpoint) was available on the [project website](#).

Respondents were asked to rate each alternative for how well it meets the community priorities identified earlier in the project:

1. Improve corridor safety, particularly between Jessie Avenue and Bell Avenue and between Silver Eagle Road and Harris Avenue.
2. Improve walking infrastructure, including the addition of signal-protected crossing opportunities where feasible.
3. Create low-stress facilities that improve safety and comfort for people walking, rolling, and bicycling to reach transit.
4. Create low-stress facilities that improve safety and comfort for people biking.

A score of 5 means the alternative "Meets expectations", 4 "Somewhat meets expectations", 3 is "Neutral", 2 "Somewhat does not meet expectations", and 1 "Does not meet expectations". Figure 3 shows an overview of the responses to this question.

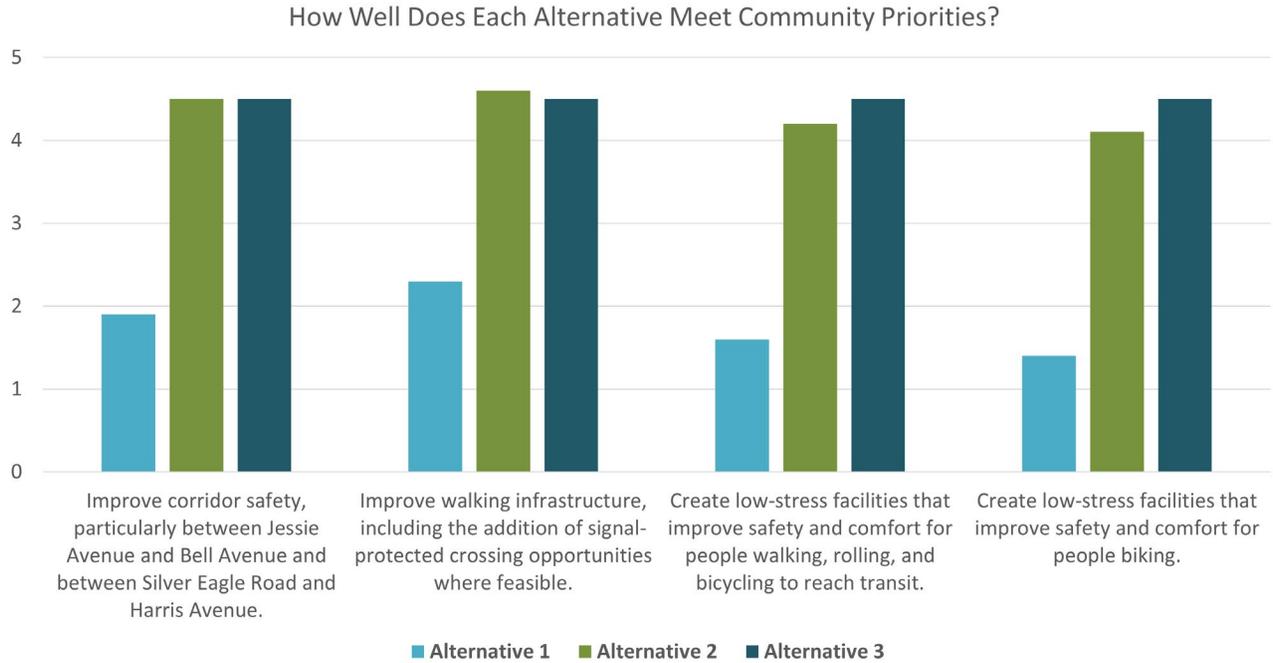


**FIGURE 1: ATTENDEES AT THE JUNE 7 WORKSHOP REVIEW THE ALTERNATIVES**



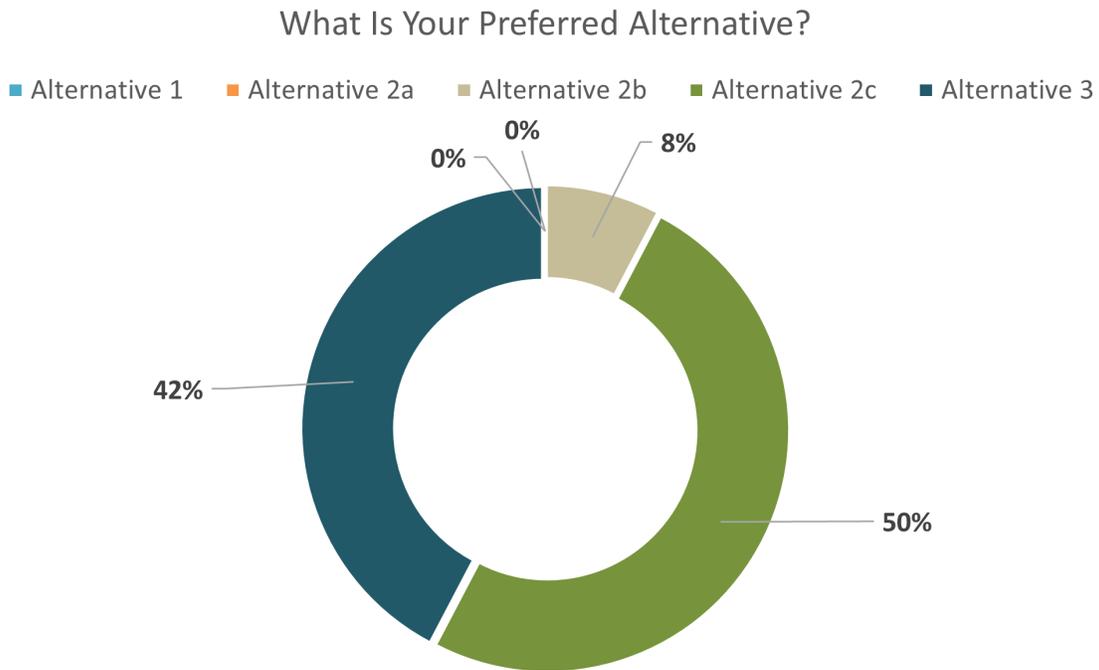
**FIGURE 2: CHARISSE PADILLA, PROJECT MANAGER WITH THE CITY OF SACRAMENTO, PRESENTS ON THE PROPOSED ALTERNATIVES**

**FIGURE 3: FEEDBACK ON COMMUNITY PRIORITIES**



Additionally, respondents were asked to select their preferred alternative. Figure 4 shows that 50% preferred Alternative 2c and 42% preferred Alternative 3.

**FIGURE 4: PREFERRED ALTERNATIVE – SOCIAL PINPOINT DATA**



The following sections include a more detailed summary and analysis of the feedback on each alternative received in the online written response forms and through in person outreach.

## **ALTERNATIVE 1**

---

Alternative 1 was generally received with mixed reviews, skewing towards negative responses overall. While a few participants acknowledged some positive elements, such as widening sidewalks or maintaining current vehicle capacity, many were critical of its lack of changes or improvements to the current roadway. Several comments stated that the option does not do enough to address corridor safety, comfort of people walking and biking, or biking infrastructure and needs. One respondent explicitly stated that it is "pretty much the same, dangerous road," reflecting a broader sentiment that Alternative 1 fails to offer a meaningful transformation of the corridor.

Those who liked Alternative 1 brought up their concerns around reducing vehicle lanes and how it would impact traffic congestion on Norwood Avenue, which is already a prominent concern among residents. Some attendees at the RPCA mini workshops expressed concerns about this issue, particularly with the increase in new developments in the area, questioning how much congestion would increase if Norwood Avenue were reduced to two lanes.

## **ALTERNATIVE 2**

---

Alternative 2 received more favorable responses, with many people saying it meets their expectations for addressing specific community priorities – mainly creating low stress facilities for those walking, biking, and rolling. Respondents showed appreciation for enhanced safety and improvements to walking and biking infrastructure, but expressed uncertainty about how well these ideas would be implemented, depending on configuration a, b, or c. Without a more distinct separation of vehicles from bikes and pedestrians, respondents had reservations about how effective this would be for improving safety. Option 2c was noted as the best long-term option for expanding green space, lighting, and comfortability along the corridor. Many respondents liked the inclusion of roundabouts for slowing traffic and reducing the potential for vehicle collisions, especially since Norwood Avenue is prone to motorists who travel at high speeds.

## **ALTERNATIVE 3**

---

Alternative 3 received the most discussion and feedback during all outreach activities. This option was viewed as the boldest and most transformative of the three. Residents liked specific elements such as roundabouts, improved landscaping, and separated bike and pedestrian facilities, all of which contributed to a perception of enhanced safety and increased comfort along the corridor. Concerns were raised about the tradeoffs of implementing a road diet and some of the other major changes proposed in Alternative 3. Specifically, some respondents wondered how reduced on-street parking and lane reductions would affect access to nearby neighborhoods and small businesses. Though some responded negatively due to the change in lane configuration, this did not outweigh the support shown for Alternative 3 due to the improvements to on-street facilities, safety, and comfortability of Norwood Avenue.

## FEEDBACK ON INDIVIDUAL PROJECT ELEMENTS

---

Respondents to the online form were asked to share feedback on various proposed elements of the project: widening and completing sidewalks, adding signalized crosswalks, removing on-street parking south of Bell Avenue, adding bus shelters and benches, adding sidewalk-scale lighting, removing a travel lane in each direction, adding roundabouts, adding a landscaping buffer, adding a separated bikeway in each direction, adding shade trees where space permits, and adding a shared use path on the west side with a cantilever structure across the freeway.

Feedback on these elements echoed many of the overarching themes in the previous section.

- Roundabouts were generally favored for traffic-calming and the safety benefits they would bring to users of the Norwood Avenue corridor. However, there were some concerns about the associated learning curve for motorists not used to traveling through roundabouts.
- Comments were supportive of removing on-street parking to use the space for protected bike lanes or wider sidewalks, if there is sufficient parking elsewhere to support visitors of local businesses.
- All improvements to walking, biking, and transit infrastructure and facilities were broadly supported in comments.
- Respondents generally supported the addition of signalized crosswalks and saw them as necessary, however, some questioned whether the high cost would be worth it since motorists don't always stop.
- Similarly, the proposed bike facilities, bus shelters, and sidewalk widening were seen as essential for improving safety and equity for active transportation users.
- Comments emphasized the need for clearly delineated routes that are separated from vehicles, reflecting the community's desire to make biking a more accessible travel option in the neighborhood. However, commenters were split on the idea of adding a shared use path with a cantilever across the freeway. Some saw it as an expensive and unnecessary addition, while others viewed it as a creative solution to create a low-stress option for crossing the freeway.
- As stated in previous sections, the reduction in travel lanes received positive feedback, while also acknowledging the potential for increasing traffic congestion. However, most respondents saw it as an important tradeoff in slowing traffic, increasing safety, and utilizing the extra space for landscaping, lighting, and comfortable walking and biking facilities.



The Norwood  
**Mobility Project**

# Phase 3 Engagement Materials



## The Norwood Mobility Public Draft Plan is Ready for Review!

Review and comment October 10 - November 2  
at [www.NorwoodMobility.org](http://www.NorwoodMobility.org)

Want to learn more? Attend a Community Workshop:

### IN-PERSON

**October 18, 2025**  
**1:00 - 2:00 PM**  
**Robertson Community Center**  
 3525 Norwood Ave,  
 Sacramento

### VIRTUAL

**October 20, 2025**  
**6:00 - 7:00 PM**  
**Zoom Meeting**  
 Register for the workshop:  
[www.NorwoodMobility.org](http://www.NorwoodMobility.org)





**There's Still Time to Review The  
Norwood Mobility Plan Public Draft!**

**Review and comment  
October 10 - November 2**



**[www.NorwoodMobility.org](http://www.NorwoodMobility.org)**

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City of  
SACRAMENTO



The Norwood  
**Mobility Project**

# Phase 3 Engagement Summary



## PHASE 3 ENGAGEMENT SUMMARY

DATE: November 26, 2025

TO: Charisse Padilla | City of Sacramento

FROM: Elise Brockett | DKS Associates

Alice Chen | DKS Associates

Josh Pilachowski | DKS Associates

SUBJECT: Norwood Mobility Project

Project #24795-000

### INTRODUCTION

This memo provides an overview of the feedback received during Phase 3 of public engagement for the Norwood Mobility Project in October/November 2025.

The City of Sacramento planned and/or attended the following events or activities during the public engagement period from October 10 – November 2, 2025:

- Hagginwood Community Meeting – October 1 at 6:00 p.m. at the Hagginwood Community Center
- District 2 Town Hall – October 15 at 6:00 p.m. at the Hagginwood Community Center
- Active Transportation Commission Meeting – October 16 at 5:30 p.m. at the City Hall Complex
- Community Workshop (in-person) – October 18 from 12:00 – 2:00 p.m. at the Robertson Community Center
- Virtual Workshop – October 20 from 6:00 – 7:00 p.m. via Zoom
- Hmong Youth and Parents United (HYPU) Trunk or Treat – October 24 from 6:00 – 9:00 p.m. at the HOPE Center
- Mutual Assistance Network (MAN) Harvest Festival – October 25 from 11 a.m. – 2:00 p.m. at the Robertson Community Center



**FIGURE 1: POP-IN AT THE HYPU TRUNK OR TREAT EVENT ON OCT. 24**

- Robla Park Community Association (RPCA) Community Meeting – October 29 from 7:00 – 8:30 p.m. at Glenwood Elementary School

A PDF of the draft plan was also available on the project website where community members could review and submit their feedback during the engagement period.

## SUMMARY OF FEEDBACK AND OVERALL THEMES

Several themes were noted in public feedback on the draft plan centering around safety, user access, and corridor design. Respondents shared their thoughts on proposed roundabouts, lane reductions, landscaping, and safety improvements for those walking and biking along Norwood Avenue.

### ROUNDBABOUTS

The following points were made regarding proposed roundabouts on Norwood Avenue:

- Roundabouts will be beneficial for the area if landscaping in the center does not obstruct driver view.
- Exploring a future roundabout at Morey Avenue would be beneficial.
- Proposed roundabout designs appear to require more space than necessary, with suggestions to explore smaller center circles to avoid right-of-way impacts.
- A two-lane roundabout may be unnecessary where only a right-turn slip lane exists today, as it could circumvent traffic calming goals.



**FIGURE 2: POP-IN AT THE MAN HARVEST FESTIVAL ON OCT. 25**

### LANE REDUCTION

The following points were made regarding the proposed lane reduction and parking reduction on Norwood Avenue:

- A reduction to one lane of traffic could impact traffic congestion on Norwood Avenue.
- There were concerns regarding the reduction of parking availability south of Bell Avenue on Norwood Avenue

### LANDSCAPING

The following points were made regarding the proposed landscaping improvements on Norwood Avenue:

- There is support for landscaping in roundabouts, with the caveat that plants should be low height to maintain visibility and safety for drivers.
- Green walkways with trees, flowers, and shrubs will make the corridor more inviting and offer some privacy for nearby residents.

- The landscaping should be sustainable in the long term.

## **OTHER COMMENTS**

---

- Some commenters showed concerns that the project limits don't extend further south along Norwood Avenue, which may exclude some communities and neighborhoods from safety and accessibility benefits.
- There were also suggestions for the following:
  - Adding multi-use lanes between Interstate 80 (I-80) north to Main Avenue and between I-80 south to Carrol Avenue
  - Adding a left-hand turning lane northbound at Jesse and Norwood and a left-hand turning lane southbound to prevent unsafe pedestrian crossings near the Chevron gas station.



The Norwood  
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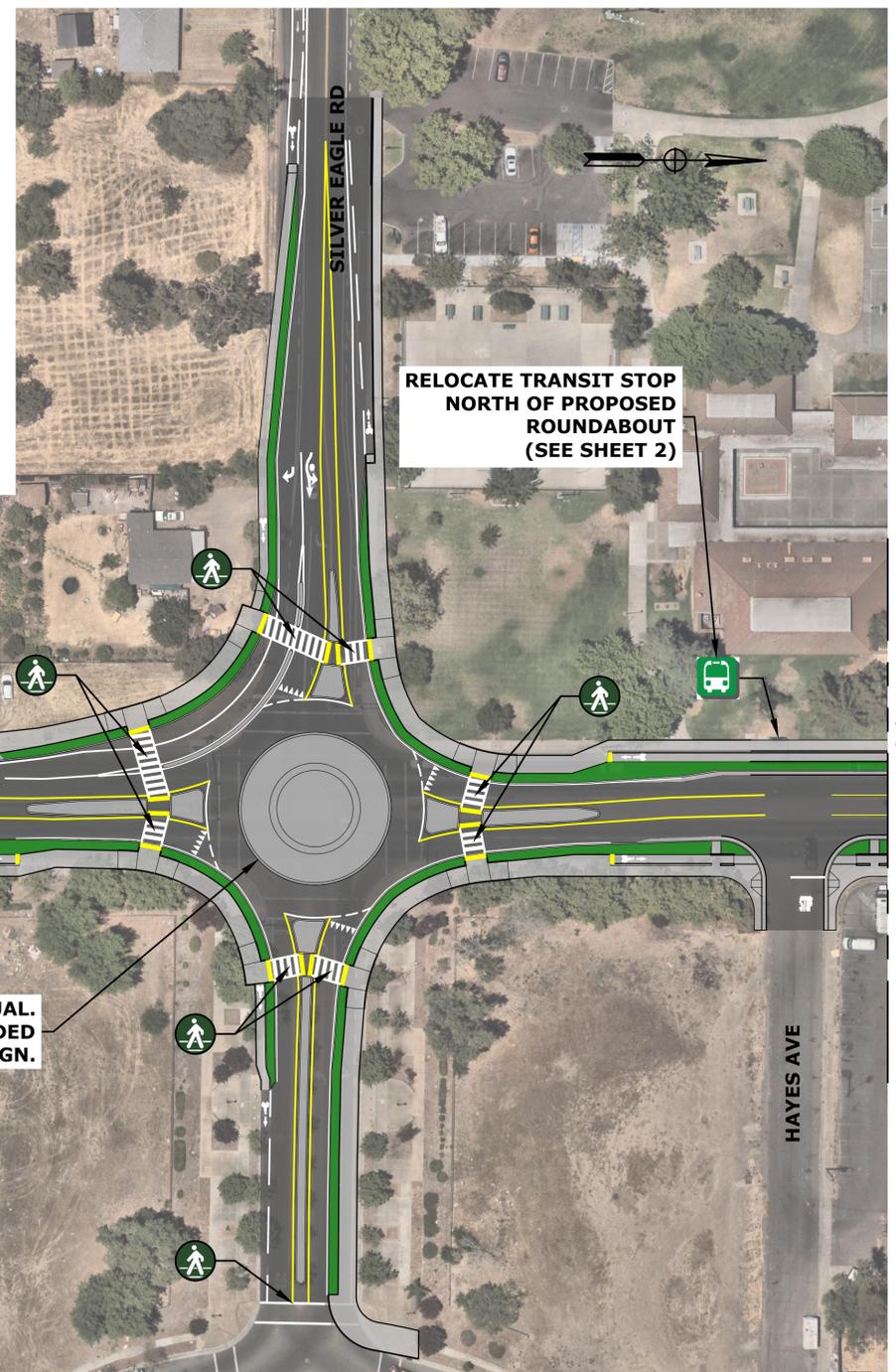
## **D – Concept Plan Set**

LEGEND:

-  Concrete Barrier
-  Crash Attenuator/Guardrail System
-  Retaining Wall
-  Modify Existing Traffic Signal
-  Pedestrian Signal
-  Roadway Pavement
-  Landscaping and/or Trees
-  Concrete Sidewalk/ Bike Lane/ Driveways
-  Existing SACRT Transit Stop
-  Crosswalk



MATCH LINE 'A'  
(SEE BELOW LEFT)

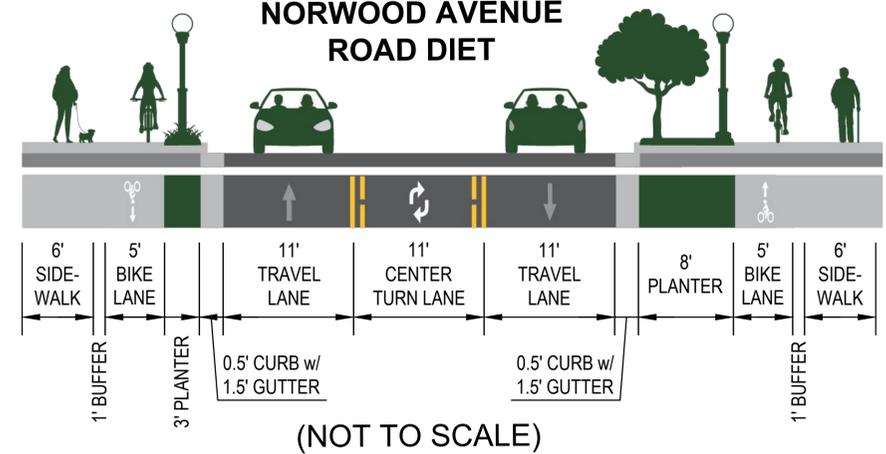


RELOCATE TRANSIT STOP  
NORTH OF PROPOSED  
ROUNDBOUT  
(SEE SHEET 2)

MATCH LINE 'B'  
(SEE SHEET 2)

TYPICAL CROSS SECTION

NORWOOD AVENUE  
ROAD DIET



MATCH LINE 'A'  
(SEE ABOVE RIGHT)

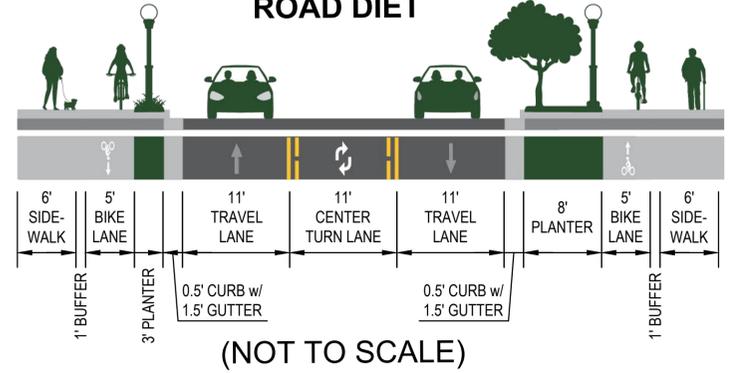
ROUNDBOUT IS CONCEPTUAL.  
ENGINEERING STUDY IS NEEDED  
TO DETERMINE SPECIFIC DESIGN.

LEGEND:

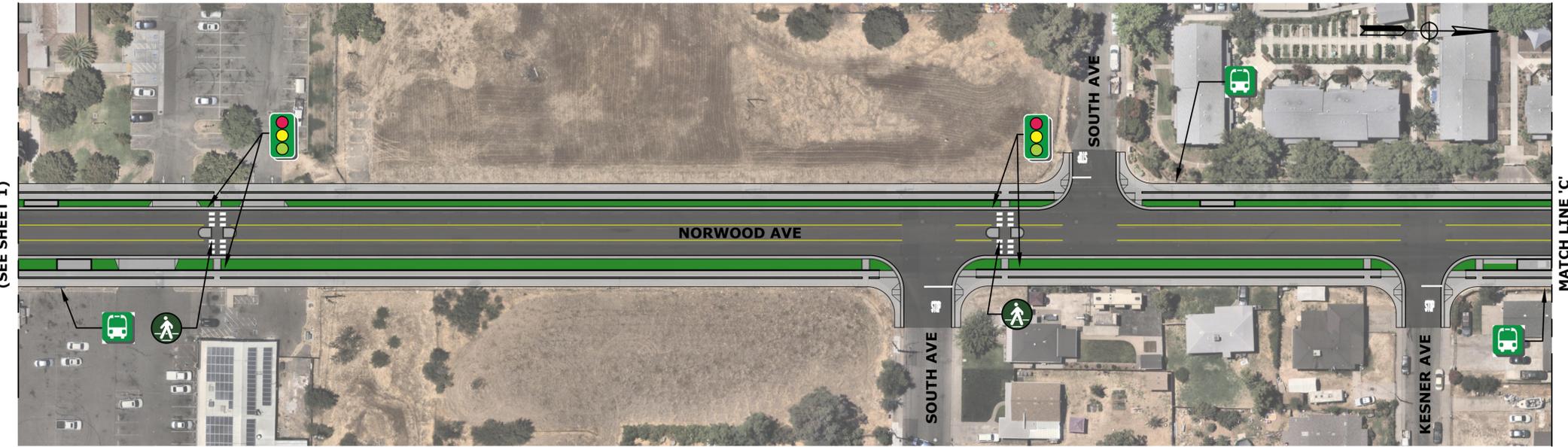
-  Concrete Barrier
-  Crash Attenuator/Guardrail System
-  Retaining Wall
-  Modify Existing Traffic Signal
-  Pedestrian Signal
-  Roadway Pavement
-  Landscaping and/or Trees
-  Concrete Sidewalk/ Bike Lane/ Driveways
-  Existing SACRT Transit Stop
-  Crosswalk

TYPICAL CROSS SECTION

NORWOOD AVENUE ROAD DIET

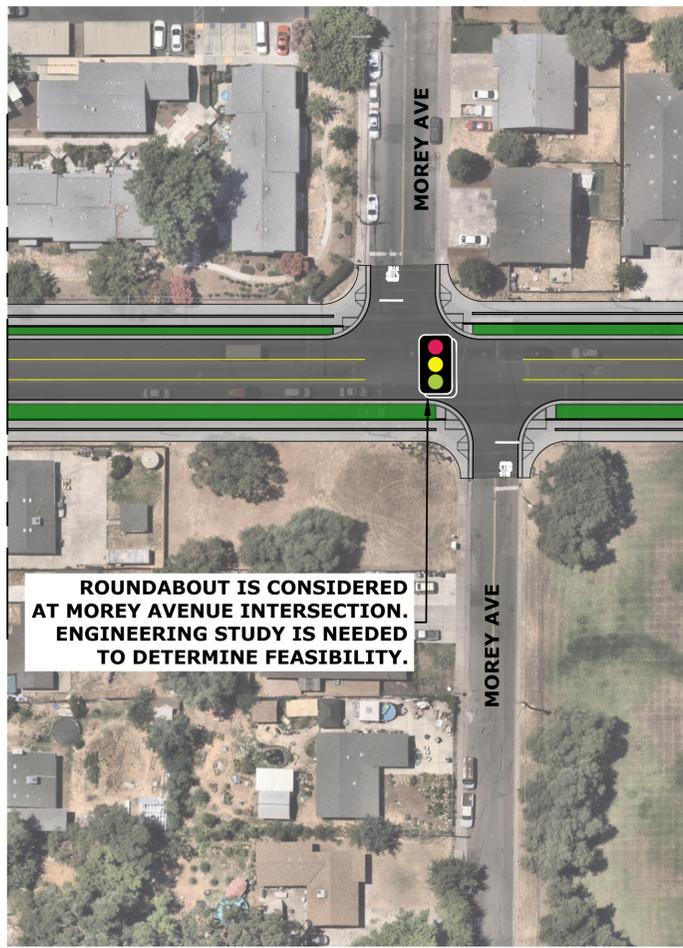


MATCH LINE 'B'  
(SEE SHEET 1)



MATCH LINE 'C'  
(SEE BELOW LEFT)

MATCH LINE 'C'  
(SEE ABOVE RIGHT)

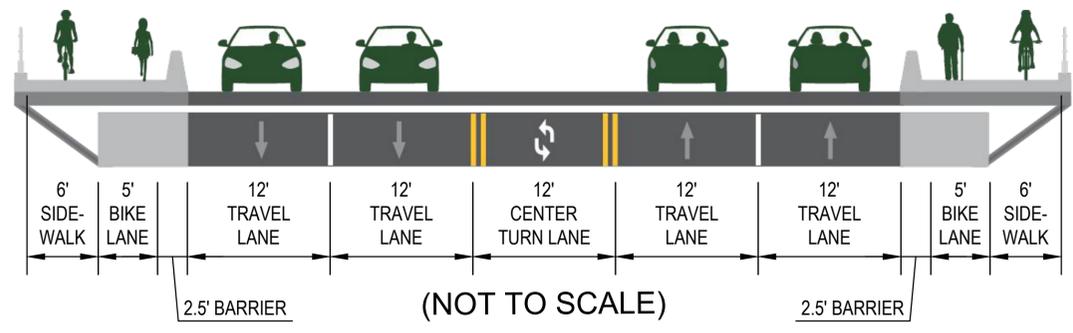


ROUNDABOUT IS CONSIDERED AT MOREY AVENUE INTERSECTION. ENGINEERING STUDY IS NEEDED TO DETERMINE FEASIBILITY.

MATCH LINE 'D'  
(SEE SHEET 3)

TYPICAL CROSS SECTION

NORWOOD AVENUE  
I-80 INTERCHANGE

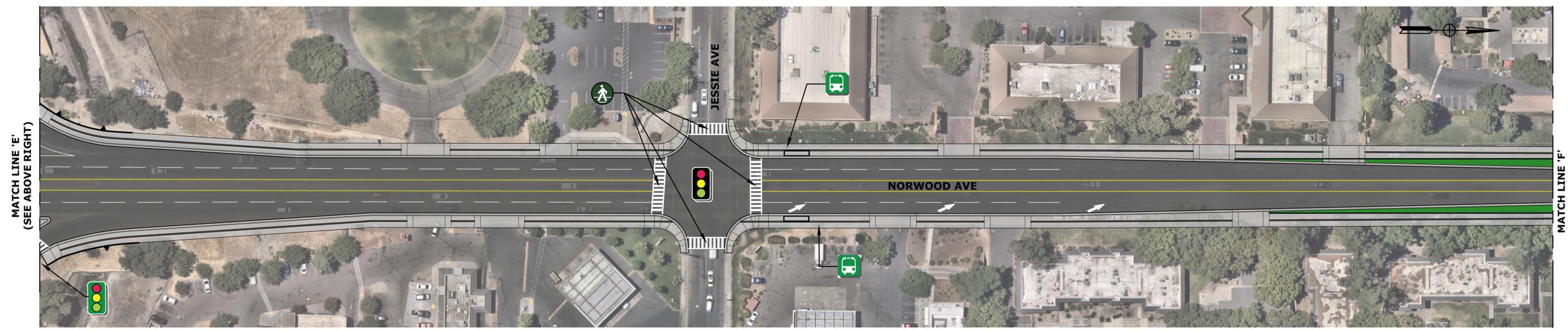
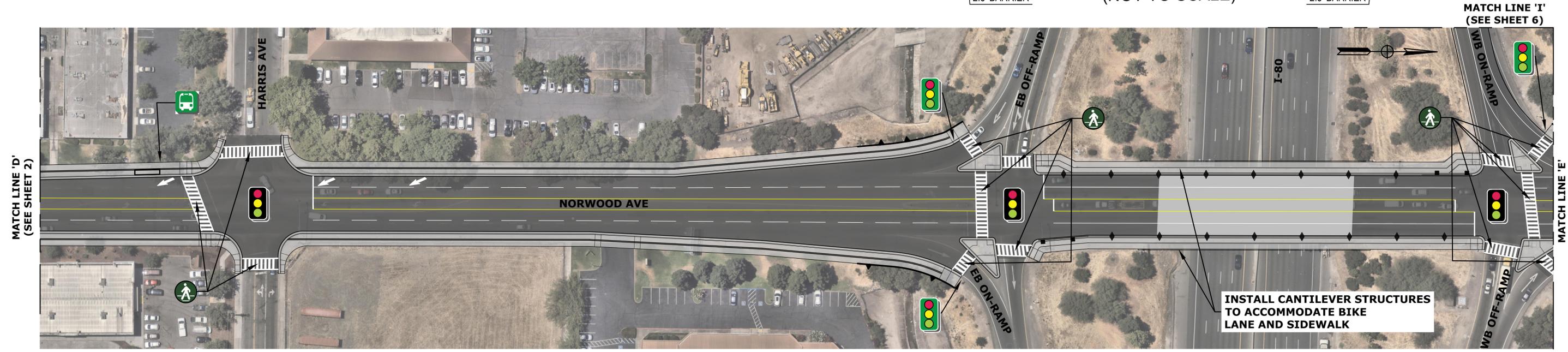


- LEGEND:**
- Concrete Barrier
  - Crash Attenuator/Guardrail System
  - Retaining Wall

- Modify Existing Traffic Signal
- Pedestrian Signal

- Roadway Pavement
- Landscaping and/or Trees
- Concrete Sidewalk/ Bike Lane/ Driveways

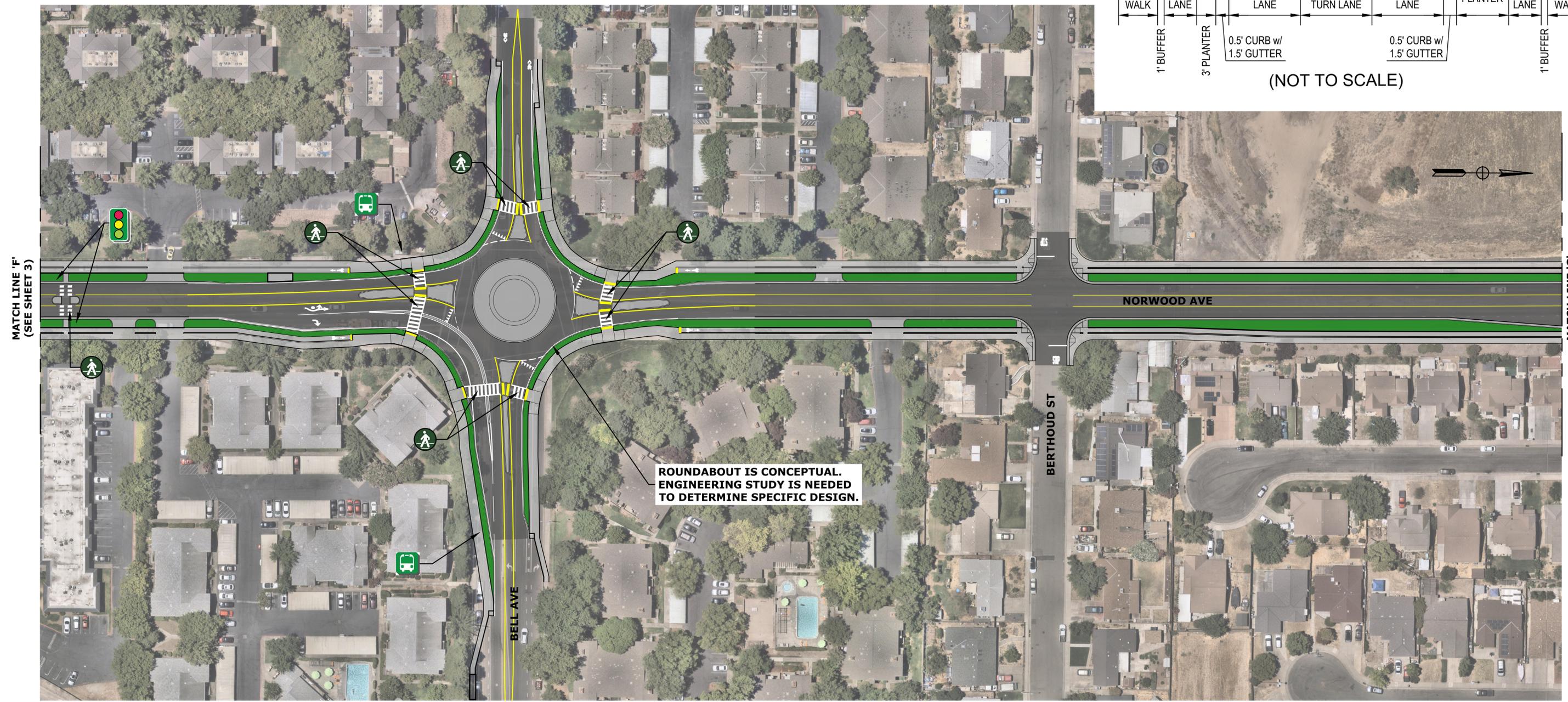
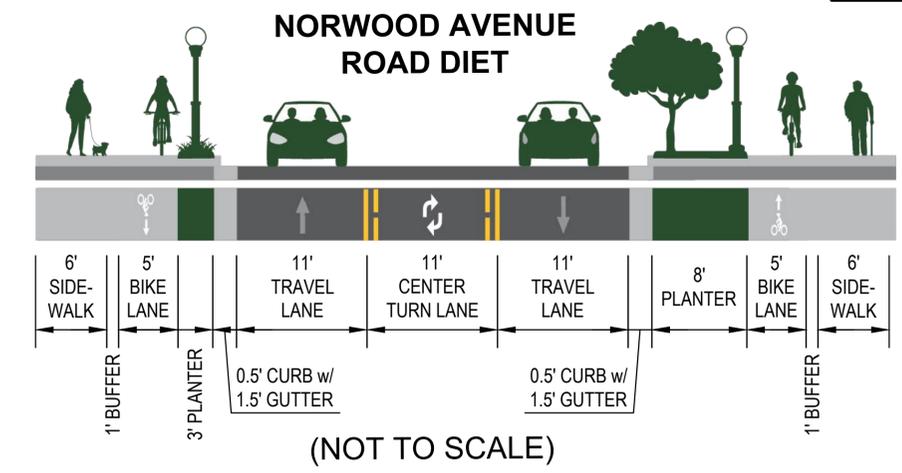
- Existing SACRT Transit Stop
- Crosswalk



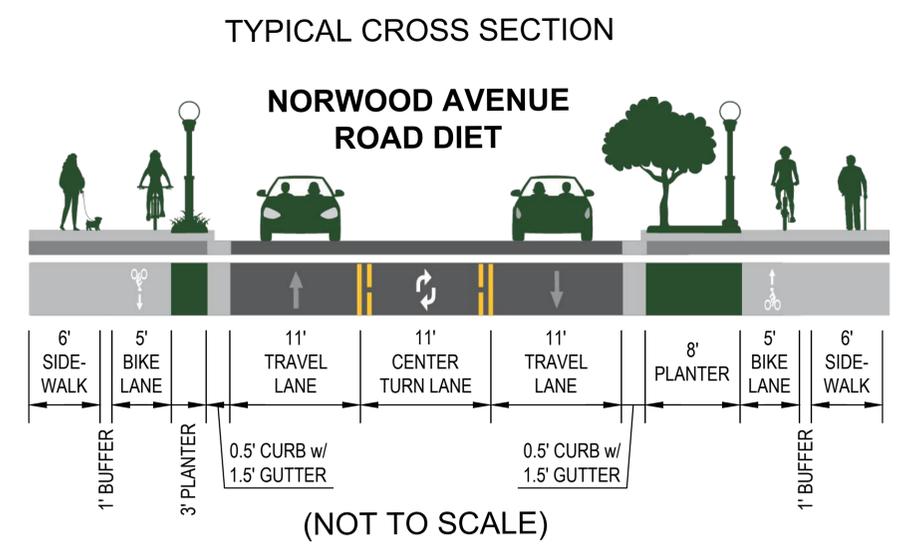
LEGEND:

-  Concrete Barrier
-  Crash Attenuator/Guardrail System
-  Retaining Wall
-  Modify Existing Traffic Signal
-  Pedestrian Signal
-  Roadway Pavement
-  Landscaping and/or Trees
-  Concrete Sidewalk/ Bike Lane/ Driveways
-  Existing SACRT Transit Stop
-  Crosswalk

TYPICAL CROSS SECTION



- LEGEND:**
-  Concrete Barrier
  -  Crash Attenuator/Guardrail System
  -  Retaining Wall
  -  Modify Existing Traffic Signal
  -  Pedestrian Signal
  -  Roadway Pavement
  -  Landscaping and/or Trees
  -  Concrete Sidewalk/ Bike Lane/ Driveways
  -  Existing SACRT Transit Stop
  -  Crosswalk



LEGEND:

Concrete Barrier

Crash Attenuator/Guardrail System

Retaining Wall

Modify Existing Traffic Signal

Pedestrian Signal

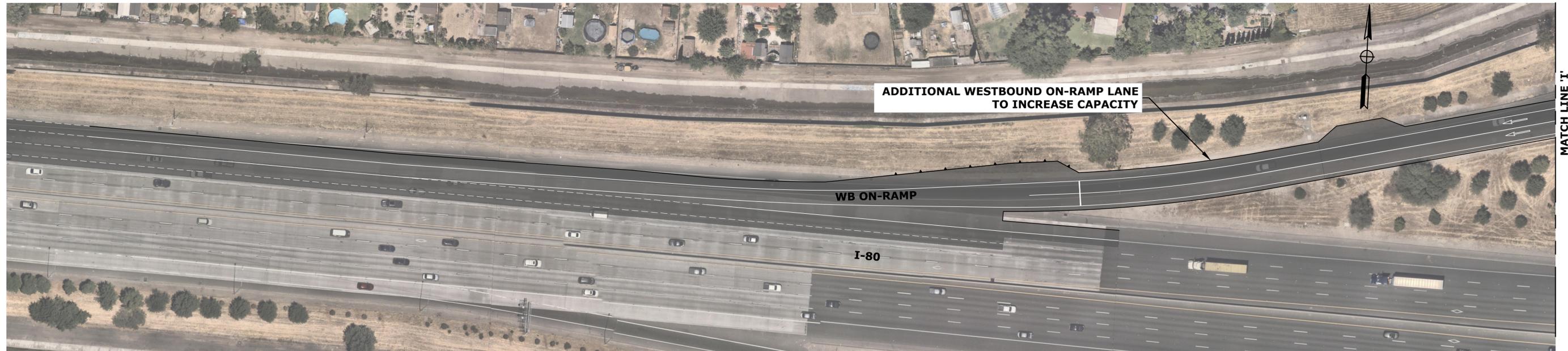
Roadway Pavement

Landscaping and/or Trees

Concrete Sidewalk/ Bike Lane/ Driveways

Existing SACRT Transit Stop

Crosswalk





The Norwood  
**Mobility Project**

## **E - Planning Level Cost Estimates**

**PRELIMINARY CONCEPT DESIGN - CONSTRUCTION COST ESTIMATE  
NORWOOD AVE COMPLETE STREETS - ALTERNATIVE 2C**

6DKS010700

9/29/2025

| ITEM NO. | ITEM DESCRIPTION                                    | UNIT | QUANTITY | UNIT PRICE  | AMOUNT      |
|----------|---|------|----------|-------------|-------------|
| 1        | Temporary Construction Easement                     | AC   | 0.60     | \$200,000   | \$120,000   |
| 2        | Right of Way Take                                   | AC   | 1.30     | \$653,400   | \$850,000   |
| 3        | Drainage System                                     | LS   | 1        | \$1,136,800 | \$1,140,000 |
| 4        | Remove Concrete Curb & Gutter                       | LF   | 19,900   | \$11        | \$220,000   |
| 5        | Remove Concrete Sidewalk                            | SF   | 99,500   | \$8         | \$800,000   |
| 6        | Roadway Excavation                                  | CY   | 26,400   | \$350       | \$9,240,000 |
| 7        | Base Repair   | TON  | 2,040    | \$300       | \$620,000   |
| 8        | Remove Striping                                     | LF   | 42,400   | \$3         | \$130,000   |
| 9        | Remove Pavement Markings                            | SF   | 5,400    | \$10        | \$60,000    |
| 10       | Hot Mix Asphalt (includes 3" overlay over existing) | TON  | 11,200   | \$250       | \$2,800,000 |
| 11       | Class 2 Aggregate Base                              | CY   | 30,400   | \$300       | \$9,120,000 |
| 12       | PCC (Stamped Concrete) to Construct                 | SF   | 16,300   | \$30        | \$490,000   |
| 13       | PCC (Curb)  | LF   | 5,600    | \$24        | \$140,000   |
| 14       | PCC (Curb & Gutter - Type 2) to Construct           | LF   | 22,800   | \$50        | \$1,140,000 |
| 15       | PCC (Sidewalk) to Construct                         | SF   | 221,900  | \$7         | \$1,560,000 |
| 16       | PCC (Curb Ramp) to Construct                        | SF   | 15,200   | \$20        | \$310,000   |
| 17       | PCC (Driveway) to Construct                         | SF   | 11,500   | \$15        | \$180,000   |
| 18       | Concrete Barrier (Type 60M)                         | LF   | 800      | \$300       | \$240,000   |
| 19       | Midwest Guardrail System                            | LF   | 50       | \$60        | \$3,000     |
| 20       | Alternative In-Line Terminal System                 | EA   | 2        | \$3,000     | \$6,000     |
| 21       | Retaining Wall                                      | SF   | 2,040    | \$200       | \$410,000   |
| 22       | Bridge Widening                                     | LS   | 1        | \$8,400,000 | \$8,400,000 |
| 23       | Striping  | LF   | 27,000   | \$6         | \$170,000   |
| 24       | Pavement Markings                                   | SF   | 13,900   | \$15        | \$210,000   |
| 25       | Roadside Signage                                    | LS   | 1        | \$40,000    | \$40,000    |
| 26       | Overhead Signage                                    | EA   | 4        | \$75,000    | \$300,000   |
| 27       | Street Lighting                                     | EA   | 67       | \$40,000    | \$2,680,000 |
| 28       | Traffic Signal Modifications                        | EA   | 9        | \$500,000   | \$4,500,000 |
| 29       | Utility Adjustments                                 | LS   | 1        | \$1,000,000 | \$1,000,000 |
| 30       | Landscaping   | LS   | 1        | \$800,000   | \$800,000   |

**SUBTOTAL** **\$54,500,000**

Contingency (25%) \$13,625,000

**TOTAL CONSTRUCTION COST ESTIMATE** **\$68,125,000**

Project Development Support Costs (35%) \$23,843,750

**TOTAL COST ESTIMATE** **\$91,968,750**

**10 Year Escalated Subtotal** **\$88,800,000**

**10 Year Escalated Contingency (25%)** **\$22,200,000**

**10 Year Escalated CONSTRUCTION COST ESTIMATE** **\$111,000,000**

**10 Year Escalated Project Development Support Costs (35%)** **\$38,900,000**

**10 Year Escalated TOTAL COST ESTIMATE** **\$149,900,000**

\* Escalation is 5% per year

# Final Draft Plan

*Active Transportation Commission*

January 15, 2026

## Project Team

City of Sacramento

**Charisse Padilla**, Project Manager, Associate Planner

**Jennifer Donlon Wyant**, Mobility and Sustainability Division  
Manager



## The Norwood **Mobility Project**

*City of*  
**SACRAMENTO**

# Agenda

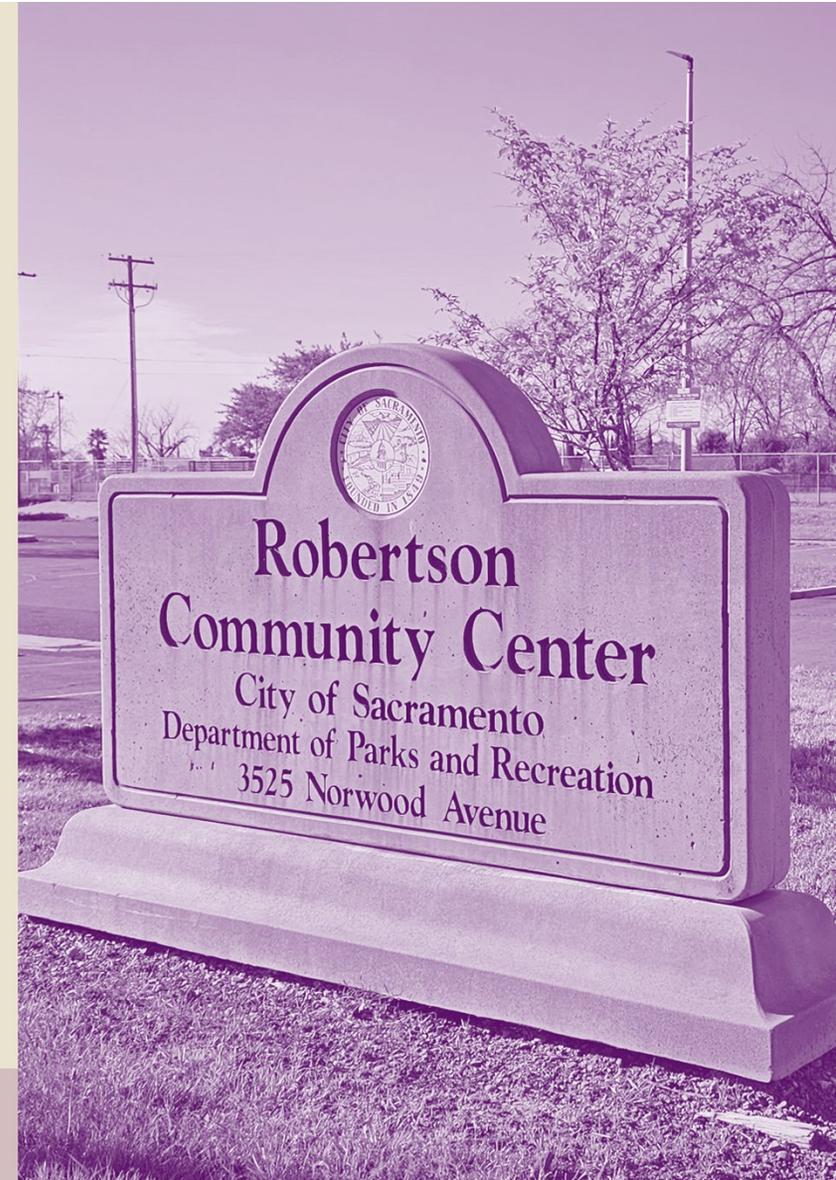
- Project Overview
- Review of Plan Features
- Next Steps



The Norwood  
**Mobility Project**



# Project Overview



# Project Overview

## Why Norwood Avenue?

1. High Priority (TPP)
2. Vision Zero High Injury Network
3. Critical corridor serving and connecting:
  - Communities
  - Residents
  - Students
  - Businesses



# Planning Goal

## Caltrans Sustainable Transportation Planning Grant funded Project

The goal of the plan is to identify a data-driven, community-supported plan for a future Norwood Avenue that will improve safety and mobility.



# Project Overview: Engagement & Plan Development

## PHASE 1 (Fall/ Winter 2024)

### Community Vision & Existing Conditions

- Interactive Web Map & Survey (Social Pinpoint)
- Mutual Assistance Network (MAN) Annual Harvest Festival
- City Hosted In-person and Virtual Workshops
- NDAT Community Workshop
- Transportation Planning Newsletter
- City Minute Blog
- ATC Presentation



## PHASE 2 (Spring/Summer 2025)

### Alternatives Analysis & Community Preferred Alternative

- Alternatives Review (Project Website-Social Pinpoint)
- Community Advisory Committee Meeting
- City Hosted In-person and Virtual Workshops
- Community Association Pop-ins/ Mini Workshops (Hagginwood CA, Robla Park CA, etc.)
- D1 Community Conversations
- Council District Newsletters
- Norwood Mailing List
- Transportation Planning Newsletter
- City Minute Blog
- ATC Presentation

## PHASE 3 (Summer/Fall 2025)

### Public Draft Plan & Public Review/ Comment

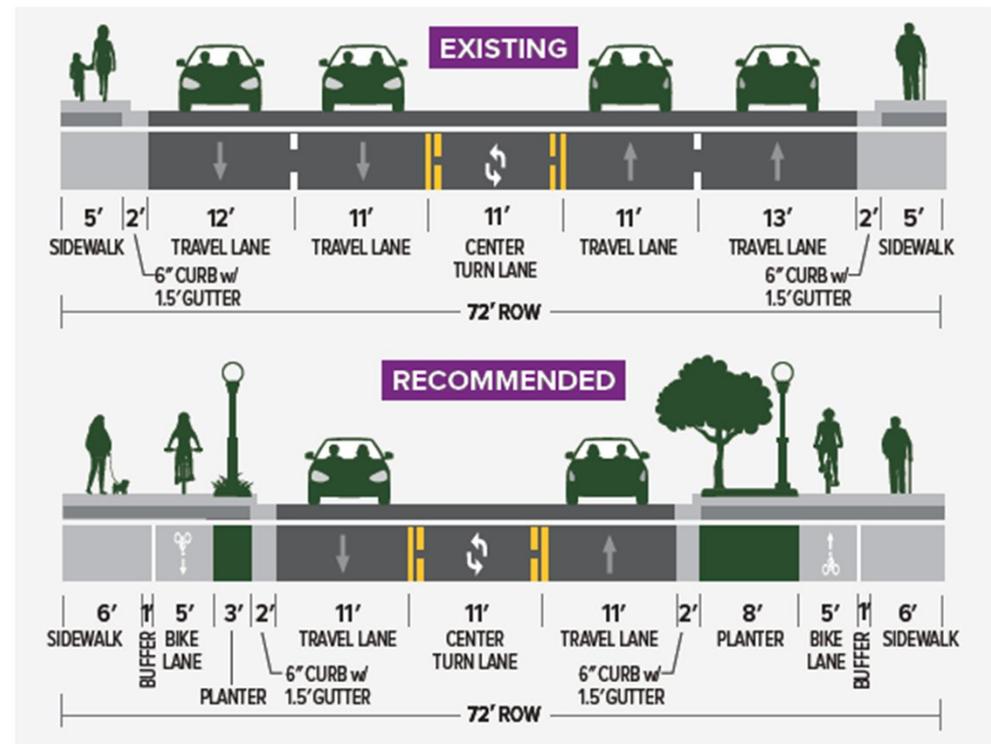
- Online Draft Plan Review & Comment (Konveio)
- City Hosted In-person and Virtual Workshops
- Community Association Pop-ins (Hagginwood CA, Robla Park CA, etc.)
- D2 Town Hall and Resource Fair
- HYPUP Trunk or Treat Event
- MAN Annual Harvest Festival
- Council District Newsletters
- Norwood Mailing List
- Transportation Planning Newsletter
- City Minute Blog
- ATC Presentation

# The Norwood Mobility Draft Plan Features



# The Norwood Mobility Draft Plan Includes:

- Removing a travel lane in each direction north of Jessie Avenue and south of Harris Avenue
- Adding sidewalks north of Berthoud Street
- Adding sidewalk lighting, a landscaping buffer, as well as shade trees on the east side of the street
- Removing on-street parking south of Bell Avenue
- Add a separated bikeway in each direction



# The Norwood Mobility Draft Plan continued...

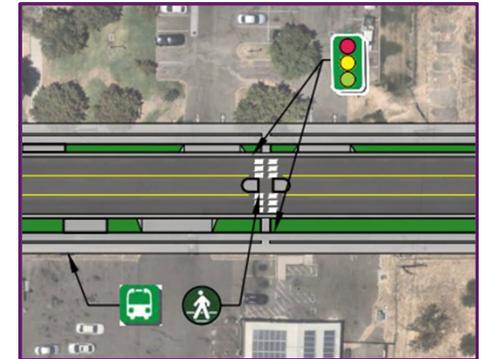
- Add roundabouts for traffic calming
- Adding signalized crosswalks at high demand locations and at I-80 ramp crossings
- Add a cantilever structure on both sides across the freeway



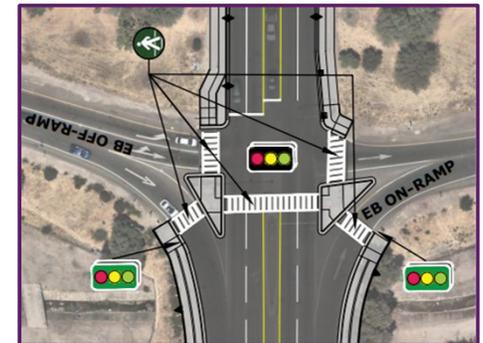
Cantilever on both sides of I-80 overpass



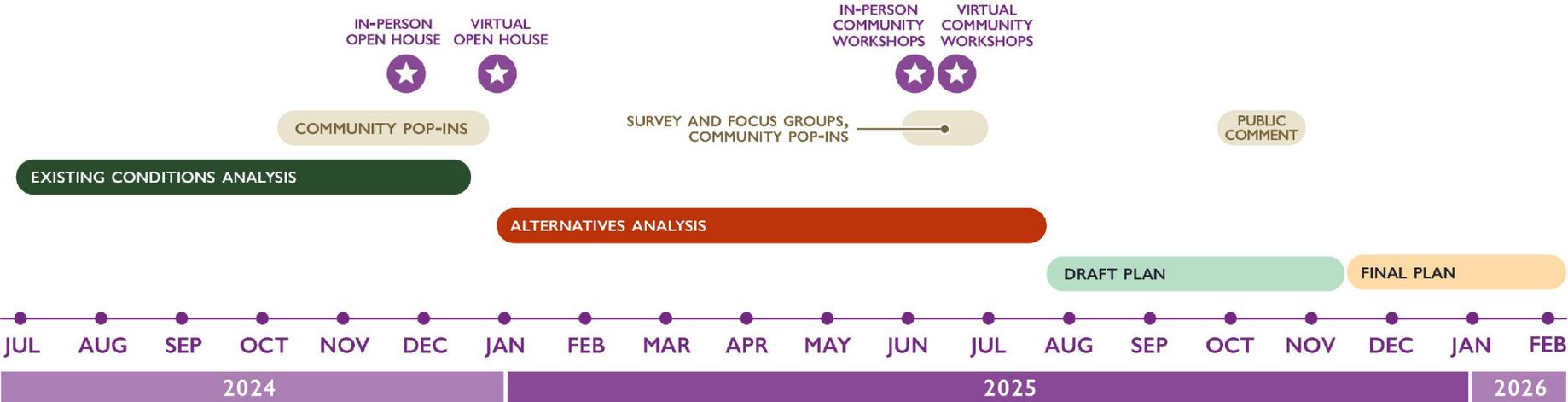
Roundabouts



Striped Crosswalks & Signalized Ped Crossings



# Next Steps



We are here

**February 2026:** Final Draft Plan for Council adoption

Staff requests ATC pass a Motion to recommend City Council approve and adopt the *Norwood Mobility Plan*

**Thank You**



The Norwood  
**Mobility Project**